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AD-A213 350



Final Report
for the Period
July 1988 to
March 1989

AL-TR-89-011

AD:

Gas Flows in Rocket Motors

Volume 3. Appendix D. Computer Code Listings

DTIC
ELECTED
OCT 13 1989
S B D

August 1989

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F04611-88-C-0014

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Prepared for the

Astronautics Laboratory (AFSC)

Air Force Space Technology Center
Space Systems Division
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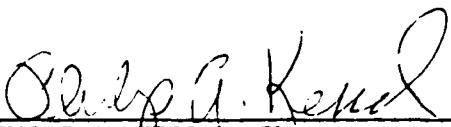
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FOREWORD

This is the final report for Task 1, Navier Stokes Analysis of Rocket Nozzles, for SETA contract F04611-88-C-0014 with the Astronautics Laboratory (AFSC), Edwards AFB CA. This work was performed by Pennsylvania State University as a subcontractor to Science Applications International Corporation (the SETA contractor). Dr Philip A. Kessel was the project manager for this analysis task.

This report has been reviewed and is approved for release and distribution in accordance with the distribution statement on the cover and on the DD Form 1473.



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REPORT DOCUMENTATION PAGE

1a. REPORT SECURITY CLASSIFICATION UNCLASSIFIED		1b. RESTRICTIVE MARKINGS										
2a. SECURITY CLASSIFICATION AUTHORITY		3. DISTRIBUTION/AVAILABILITY OF REPORT Approved for Public Release; Distribution is unlimited.										
2b. DECLASSIFICATION/DOWNGRADING SCHEDULE												
4. PERFORMING ORGANIZATION REPORT NUMBER(S)		5. MONITORING ORGANIZATION REPORT NUMBER(S) AL-TR-89-011										
6a. NAME OF PERFORMING ORGANIZATION Pennsylvania State University	6b. OFFICE SYMBOL (If applicable)	7a. NAME OF MONITORING ORGANIZATION Astronautics Laboratory (AFSC)										
6c. ADDRESS (City, State, and ZIP Code) Mechanical Engineering Department University Park PA 16802		7b. ADDRESS (City, State, and ZIP Code) AL/LSCF Edwards AFB CA 93523-5000										
8a. NAME OF FUNDING/SPONSORING ORGANIZATION	8b. OFFICE SYMBOL (If applicable)	9. PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER F04611-88-C-0014										
8c. ADDRESS (City, State, and ZIP Code)		10. SOURCE OF FUNDING NUMBERS <table border="1"> <tr> <th>PROGRAM ELEMENT NO.</th> <th>PROJECT NO.</th> <th>TASK NO</th> <th>WORK UNIT ACCESSION NO</th> </tr> <tr> <td>62302F</td> <td>3058</td> <td>00</td> <td>SD</td> </tr> </table>		PROGRAM ELEMENT NO.	PROJECT NO.	TASK NO	WORK UNIT ACCESSION NO	62302F	3058	00	SD	
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62302F	3058	00	SD									
11. TITLE (Include Security Classification) Gas Flows in Rocket Nozzles. Volume 3: Appendix D - Computer Code Listings												
12. PERSONAL AUTHOR(S) Kronzon, Yigal; Lyan-Chang, Chau; and Merkle, Charles L.												
13a. TYPE OF REPORT Final	13b. TIME COVERED FROM 88/07 TO 89/03	14. DATE OF REPORT (Year, Month, Day)	15. PAGE COUNT									
16. SUPPLEMENTARY NOTATION This is volume 3 of a 3 volume report												
17. COSATI CODES <table border="1"> <tr> <th>FIELD</th> <th>GROUP</th> <th>SUB-GROUP</th> </tr> <tr> <td>20</td> <td>04</td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> </tr> </table>		FIELD	GROUP	SUB-GROUP	20	04					18. SUBJECT TERMS (Continue on reverse if necessary and identify by block number) nozzle analysis, Navier-Stokes, turbulent flow, equilibrium chemistry	
FIELD	GROUP	SUB-GROUP										
20	04											
19. ABSTRACT (Continue on reverse if necessary and identify by block number) Detailed descriptions of the governing equations, the method of solution, and the computer code for calculating perfect gas or real gas flow in axisymmetric nozzles are given. The codes permit calculation of a perfect gas or a real gas for inviscid flow by solving the Euler equations, and for viscous flow by solving the thin layer Navier-Stokes equations. These equations are written in a conservative form and solved implicitly in body-fitted coordinates. The solution obtained by the conservative variables is expressed in terms of the density, ρ , the momentum parallel to the axis of symmetry (u), the momentum perpendicular to the axis (v), and the total internal energy, e_0 . These variables are then used to calculate the nonconservative primitive variables, the velocity components, u and v , the pressure, p , and the temperature, T . The nozzle performance including the rate of mass flow, \dot{m} , the thrust, T , and the specific impulse are also computed. The codes were written in FORTRAN V and ran on the CYBER 180/840, NOS/BE system which limited the number of grid points to 20 x 44 for solving the Euler equations and 60 x 40 for												
20. DISTRIBUTION/AVAILABILITY OF ABSTRACT <input checked="" type="checkbox"/> UNCLASSIFIED/UNLIMITED <input type="checkbox"/> SAME AS RPT. <input type="checkbox"/> DTIC USERS		21. ABSTRACT SECURITY CLASSIFICATION UNCLASSIFIED										
22a. NAME OF RESPONSIBLE INDIVIDUAL Dr Philip A. Kessel		22b. TELEPHONE (Include Area Code) (805) 275-5591	22c. OFFICE SYMBOL AL/LSCF									

Block 19.

the TLNS equations. The results obtained for the nozzle flowfield showed maximum global mass flux errors of less than $\pm 1\%$ for the Euler equations and less than $\pm 2\%$ for the TLNS equations. Solutions with more dense grids (typically 100×50 or higher) consistently showed global mass conservation of better than one percent.

VENKATESWARAN SANKA (V19)

AXI2DV FOR

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VENKATESWARAN SANKA (V19)

AXI2DV FOR

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  D DD VOL=REF=STU.I19500.MYH100.LIB,DISP=(OLD,DELETE),
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    DSN=STU.I19500.MYH100.HERMES.CONV.MASS.VIS
  EXEC FVCG,PARM,SOURCE='OPT(3)'
  SYSIN DD *
C*****+
C*      PROGRAM NAME: AXI2DV.FOR
C*      AXISYMMETRIC TRANSONIC NOZZLE FLOW
C*      IN GENERAL COORDINATE SYSTEM
C*      USING TIME ITERATIVE CD/CD SCHEME
C*      WITH THIN-LAYER APPROXIMATED NAVIER-STOKE'S EQ.
C*      MAIN PROGRAM
C*
C*****+
IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=100)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
  P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
  ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
  ,ZMUT(IZ,JZ)
  ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
  PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF,COND
COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
  (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****+
CALL ERRSET(208,256,-1,0,0,0)
CALL INITIA
DO 10 NADV=NBEG,NEND
  WRITE(6,*) NADV
  CALL SOLVE
  CALL CHECK
10  CONTINUE
  CALL MASS
  CALL OUTPUT
  STOP
  END
C*
C* SET UP INITIAL CONDITION
C*
SUBROUTINE INITIA
C*****+
IMPLICIT REAL*8(A-H,O-Z)

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```

PARAMETER (IZ=150,JZ=100)
COMMON/VECTOR/PQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
           P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
           ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELAU(IZ,JZ)
           ,ZMUT(IZ,JZ)
           ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
           PRNT,PB,RM1,SUM(4),ZMU0,REN,PRN,TWALL,TREF,COND
COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
COMMON/CPCOEF/ CPA1,CPA2,CPA3,CPA4,CPA5,CPA6,CPA7
           ,CPA8,CPA9,CPA10,ENE(101)
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
           ,(Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****+*****+*****+*****+*****+*****+*****+*****+*****+*****+*****+*****+*****+*****+
DIMENSION SS(3500,4)
NAMELIST/INPUT/IL,JL,NEND,PO,TO,CFL,OMEGAX,OMEGAY,RM1,AIN,EST,
           NITER,ATH,RL,THETA,CPO,GAMMAO,NBEG,ITIME,ISUP,IVISC,IWALL,RM2
           ,IREAD,PRN,REN,TREF,ZMU0,TWALL,FSTY,PB,PRNT,COND
C... ISUP = 0 FOR PURE SUBSONIC FLOW
C      1 FOR TRANSONIC FLOW
C      3 FOR PURE SUPERSONIC FLOW
C... NOT SUITABLE FOR PURE SUPERSONIC FLOW CALCULATION
C... PB = BACK PRESSURE FOR ISUP=0
C
C ** READ INPUT DATA
  READ(5,INPUT)
  WRITE(22,INPUT)
C ** SET UP GEOMETRY
  IL1=IL-1
  JL1=JL-1
C
  CALL CPCOEF
  WRITE(6,*) CPA1,CPA2,CPA3,CPA4,CPA5,CPA6,CPA7,CPA8,CPA9,CPA10
C
  PI=PI=DCOS(-1.D0)
  C1=(AIN-ATH)/2.
  C2=(AIN+ATH)/2.
  DO 10 I=1,IL
  IF(ISUP.EQ.3)THEN
    AREA(I)=AIN+(ATH-AIN)*DFLOAT(I-1)/DFLOAT(IL1)
  ELSE
    AREA(I)=(C1*DCOS(DFLOAT(I-1)*2.*PI/DFLOAT(IL1))+C2)*0.5
  ARR=ATH/AIN
  XX=DFLOAT(I-1)/DFLOAT(IL1)*RL
  AREA(I)=2.0*(ARR-1.)*XX**3+3.0*(ARR-1.)*XX**2+1.0
  AREA(I)=(ARR-1.)*(XX**2-4.*XX+4.)*XX**2+1.0
  END IF
10  CONTINUE
  IF(IREAD.EQ.2)THEN
    DO 18 I=1,IL
    READ(38,*) X(I,1),AREA(I)
    CONTINUE
18

```

```

ENDIF
DO 20 I=1, IL
DO 20 J=1, JL
IF(IREAD.EQ.2)THEN
  X(I,J)=X(I,1)
ELSE
  X(I,J)=DFLOAT(I-1)/DFLOAT(IL1)*RL
ENDIF
20 Y(I,J)=DFLOAT(J-1)/DFLOAT(JL1)*AREA(I)
IF(FST.NE.0.D0.AND.ISUP.EQ.3)THEN
DO=(FST-1.0)/(FST**IL1-1.)*RL
DO 15 I=1, IL
XL=DO*(FST**((I-1)-1.)/(FST-1.))
AREA(I)=AIN+XL/RL*(ATH-AIN)
DO 15 J=1, JL
X(I,J)=XL
Y(I,J)=DFLOAT(J-1)/DFLOAT(JL1)*AREA(I)
15 CONTINUE
ELSE
ENDIF
C* STRETCH THE GRID ALONG Y-DIRECETION IN VISCOUS CASE
IF(IVISC.EQ.1.AND.FSTY.NE.0.D0)THEN
  DO 17 I=1, IL
    Y(I,1)=0.
    DAO=(1.-FSTY)/(1.-FSTY**JL1)*AREA(I)
    DO 17 J=2, JL
      Y(I,J)=Y(I,J-1)+DAO*FSTY**((J-2))
17 CONTINUE
ELSE
ENDIF
C * READ GRID FROM DATA FILE
IF(IREAD.EQ.1)THEN
DO 25 I=1, IL
DO 25 J=1, JL
READ(38)II,JJ,X(I,J),Y(I,J)
25 CONTINUE
ELSE
ENDIF
ATH=Y(1,JL)
DO 125 I=2, IL
IF(Y(I,JL).LT.ATH)THEN
  ATH=Y(I,JL)
  XTH=X(I,JL)
ELSE
ENDIF
125 CONTINUE
C ** COORDINATE TRANSFORMATION
EXI=1.0
EYI=1.0
DO 30 I=1, IL
IP1=I+1
IM1=I-1
IF(I.EQ.1)IM1=1
IF(I.EQ.IL)IP1=IL
DSA1=2.*EXI

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IF(I.EQ.1.OR.I.EQ.IL)DSA1=EX1
DO 30 J=1,JL
  JP1=J+1
  JM1=J-1
  IF(J.EQ.1)JM1=1
  IF(J.EQ.JL)JP1=JL
  DETA=2.*EY1
  IF(J.EQ.1.OR.J.EQ.JL)DETA=EY1
  XSA1=(X(IP1,J)-X(IM1,J))/DSA1
  YSA1=(Y(IP1,J)-Y(IM1,J))/DSA1
  XETA=(X(I,JP1)-X(I,JM1))/DETA
  YETA=(Y(I,JP1)-Y(I,JM1))/DETA
  IF(J.EQ.1)THEN
    XETA=XETA-0.5*(X(I,J)-2.*X(I,J+1)+X(I,J+2))
    YETA=YETA-0.5*(Y(I,J)-2.*Y(I,J+1)+Y(I,J+2))
  ELSE
  ENDIF
  IF(J.EQ.JL) THEN
    XETA=(3.DO*X(I,JL)-4.DO*X(I,JL-1)+X(I,JL-2))*0.5DO
    YETA=(3.DO*Y(I,JL)-4.DO*Y(I,JL-1)+Y(I,JL-2))*0.5DO
  ELSE
  ENDIF
  RJP=XSA1*YETA-XETA*YSA1
  RJ(I,J)=1./RJP
  SAIX(I,J)=YETA/RJP
  SAIY(I,J)=-XETA/RJP
  ETAX(I,J)=-YSA1/RJP
  30  ETAY(I,J)=XSA1/RJP
C ** INITIALIZATION
RGAS=8314.3/20.405
R=RGAS
DO 991 I=1,IL
DO 991 J=1,JL
TTT=3061.1DO
CALL CPGAM(CP(I,J),CV(I,J),GAMMA(I,J),GM1(I,J),RGAS,I,J,
> RHO(I,J),RHOU(I,J),RHOV(I,J),E(I,J),TTT)
991 CONTINUE
C* GIVE THE INITIAL VALUE OF VISCOSTY
C  TIN=T0*(1.+0.5*GM10*RM1**2)
C  UIN=RM1*DSQRT(GAMMAO*R*TIN)
C  PIN=P0*(TIN/T0)**(GAMMAO/GM10)
C  RIN=PIN/(R*TIN)
C  ZMU0=(RIN*UIN*AREA(1)*2.)/REN
C* CALCULATE METRIC TERMS AT MID POINTS
C*
CALL MCONST
C ** SKIP TO RERUN THE CODE
  IF(NBEG.NE.1)GOTO 300
  RM=0.04
  DO 50 I=1,IL
C#  IF(ISUP.EQ.0)THEN
C#    RMTH=RM2
C#    RM=RM1+X(I,1)/RL*2.* (RMTH-RM1)
C#    IF(X(I,1).GT.(0.5*RL))RM=RMTH-(X(I,1)-0.5*RL)/RL*2.
C#    *(RMTH-RM1)

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C#      ELSE
C#          RM=RM1+DFLOAT(I-1)/DFLOAT(IL1)*(RM2-RM1)
C#      END IF
C#      CALL ISENMA(I,ATH,XTH,RM)
C#      TS=TO/(1.+0.5*GM1(I,1)*RM**2)
C#      UU=RM*DSQRT(GAMMA(I,1)*R*TS)
C#      DO 50 J=1,JL
C#      IF(I.EQ.1.OR.I.EQ.IL)THEN
C#          IF(I.EQ.1)SLOPE=(Y(I+1,J)-Y(I,J))/(X(I+1,J)-X(I,J))
C#          IF(I.EQ.IL)SLOPE=(Y(I,J)-Y(I-1,J))/(X(I,J)-X(I-1,J))
C#      ELSE
C#          SLOPE=(Y(I+1,J)-Y(I-1,J))/(X(I+1,J)-X(I-1,J))
C#      END IF
C#      DENOM=DSQRT(1.+SLOPE*SLOPE)
C#      U(I,J)=UU/DENOM
C#      V(I,J)=UU*SLOPE/DENOM
C#      VN(I,J)=ETAX(I,J)*U(I,J)+ETAY(I,J)*V(I,J)
C#      UN(I,J)=SAIX(I,J)*U(I,J)+SAIY(I,J)*V(I,J)
C#      IF(J.EQ.JL)THEN
C#          VN(I,J)=0.
C#          U(I,J)=UU/DENOM
C#          V(I,J)=-ETAX(I,J)/ETAY(I,J)*U(I,J)
C#          UN(I,J)=U(I,J)*SAIX(I,J)+V(I,J)*SAIY(I,J)
C#      ELSE
C#      END IF
50    CONTINUE
C#      NO SLIP INITIAL CONDITION
IF(IVISC.EQ.1)THEN
    DO 60 I=1,IL
    U(I,JL)=0.
    V(I,JL)=0.
    UN(I,JL)=0.
    VN(I,JL)=0.
60    CONTINUE
ELSE
ENDIF
EIGMAX=0.0
DO 80 I=1,IL
DO 80 J=1,JL
TS=TO-(U(I,J)**2+V(I,J)**2)/CP(I,J)*0.5
PS=FO/(TO/TS)**(GAMMA(I,J)/GM1(I,J))
IF(J.EQ.JL.AND.IVIS.CEQ.1)THEN
    IF(IWALL.EQ.1)TS=TWALL
    PS=P(I,J-1)
ELSE
ENDIF
RHOO=PS/R/TS
RHO(I,J)=RHOO
RHOU(I,J)=RHO(I,J)*U(I,J)
RHOV(I,J)=RHO(I,J)*V(I,J)
E(I,J)=RHO(I,J)*(CV(I,J)*TS+0.5*(U(I,J)**2+V(I,J)**2))
80    P(I,J)=PS
DO 90 I=1,IL
DO 90 J=1,JL
CO=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))

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ZM=DSQRT(U(I,J)**2+V(I,J)**2)/CO
IF(COND.GT.0.0.AND.ZM.LT.1.C) GOTO 210
CX=DSQRT(SAIX(I,J)**2+SAIY(I,J)**2)
CY=DSQRT(ETAX(I,J)**2+ETAY(I,J)**2)
CX=(UN(I,J)+CX*CO)/EXI
CY=(VN(I,J)+CY*CO)/EYI
C EIGNN=CX
C IF(DABS(CY).GT.EIGNN)EIGNN=DABS(CY)
EIGNN=DSQRT(CX**2+CY**2)
IF(ITIME.EQ.1)GO TO 85
IF(CX.GE.EIGMAX)EIGMAX=CX
IF(CY.GT.EIGMAX)EIGMAX=CY
85 DELTAU(I,J)=CFL/EIGNN
GOTO 90
210 CONTINUE
C ZM=DSQRT((U(I,J)**2+V(I,J)**2)/C(I,J)**2)
SX=UN(I,J)**2*(1.DO-ZM**2)**2+4.DO*(U(I,J)**2+V(I,J)**2)
` *(SAIX(I,J)**2+SAIY(I,J)**2)
SY=VN(I,J)**2*(1.DO-ZM**2)**2+4.DO*(U(I,J)**2+V(I,J)**2)
` *(ETAX(I,J)**2+ETAY(I,J)**2)
EIGVX=0.5DO*(UN(I,J)*(1.DO+ZM**2)+DSQRT(SX))
EIGVY=0.5DO*(VN(I,J)*(1.DO+ZM**2)+DSQRT(SY))
DELTAU(I,J)=CFL/DSQRT(EIGVX**2+EIGVY**2)
90 CONTINUE
IF(ITIME.EQ.1)RETURN
DO 100 I=1,IL
DO 100 J=1,JL
100 DELTAU(I,J)=CFL/EIGMAX
RETURN
300 CONTINUE
310 READ(19,720,END=1000)NDUM,(SS(NDUM,K),K=1,4)
GOTO 310
1000 CONTINUE
REWIND 19
NBEG=NDUM+1
NEND=NBEG+NITER-1
DO 320 N=1,NDUM
320 WRITE(19,720)N,(SS(N,K),K=1,4)
720 FORMAT(I5,3X,4(1X,E14.7))
DO 330 I=1,IL
DO 330 J=1,JL
READ(66)(Q(I,J,K),K=1,4),DELTAU(I,J)
TCP=0.DO
CALL CPGAM(CP(I,J),CV(I,J),GAMMA(I,J),GM1(I,J),RGAS,I,J,
` RHO(I,J),RHOU(I,J),RHOV(I,J),E(I,J),TCP)
U(I,J)=RHOU(I,J)/RHO(I,J)
V(I,J)=RHOV(I,J)/RHO(I,J)
UN(I,J)=U(I,J)*SAIX(I,J)+V(I,J)*SAIY(I,J)
VN(I,J)=U(I,J)*ETAX(I,J)+V(I,J)*ETAY(I,J)
P(I,J)=GM1(I,J)*(E(I,J)-0.5*RHO(I,J)*(U(I,J)**2+V(I,J)**2))
330 CONTINUE
REWIND 66
RETURN
END
C*****
```

FILE: AXI.DV FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STA

SUBROUTINE ISENMA(I,ATH,XTH,RM)

C*****

IMPLICIT REAL*8(A-H,O-Z)

PARAMETER (IZ=150,JZ=100)

COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)

,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)

,ZMUT(IZ,JZ)

,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)

COMMON/INTEG/IL,JL,IL1,JL1,NEND,NNEG,NADV,ITIME,ISUP,IVISC,IWALL

COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS

ARR=(Y(I,JL)/ATH)**2

RM1=RM*1.05

RM2=RM*0.95

IF(X(I,JL).GT.XTH)THEN

 RM1=RM*1.05

 RM2=RM*1.01

ELSE

ENDIF

GP1=GAMMA(I,JL)+1.0

GEXP=GP1/(2.0-2.0*GAMMA(I,JL))

GSQRT=DSQRT(GAMMA(I,JL))

CNUM=GSQRT*(GP1/2.0)**GEXP

ZM=RM1

F01=ZM*GSQRT*(1.0+0.5*GM1(I,JL)*ZM*ZM)**GEXP

F1=CNUM/F01

ZM=RM2

F01=ZM*GSQRT*(1.0+0.5*GM1(I,JL)*ZM*ZM)**GEXP

F2=CNUM/F01

10 RM3=FM1+(RM2-RM1)*(ARR-F1)/(F2-F1)

ZM=FM3

F01=ZM*GSQRT*(1.0+0.5*GM1(I,JL)*ZM*ZM)**GEXP

F3=CNUM/F01

ERR=DABS(ARR-F3)

IF(ERR.LT.1.0D-4) GO TO 20

RM1=RM2

F1=F2

RM2=RM3

F2=F3

GO TO 10

20 RM=RM3

WRITE(6,*) I,ARR,RM

RETURN

END

C-----

SUBROUTINE SOLVE

C*

C* SOLVE SUBROUTINE

C*

C*****

IMPLICIT REAL*8(A-H,O-Z)

PARAMETER (IZ=150,JZ=100)

COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),

P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)

COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)

```

      , RJ(IZ,JZ), X(IZ,JZ), Y(IZ,JZ), DELTAU(IZ,JZ)
      , ZMUT(IZ,JZ)
      , AREA(IZ), ZMU(IZ,JZ), A1(IZ,JZ), A2(IZ,JZ), A3(IZ,JZ), A4(IZ,JZ)
COMMON /CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,FO,TO,
      FRNT,PB,RM1,SUM(4),ZMUE,REN,PRN,TWALL,TREF,COND
COMMON /CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
COMMON /INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
      (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
*****+
C* RHS CALCULATION
    IF(IVISC.EQ.1)CALL MULAM
    IF(FRNT.NF.O.DO) CALL MUTUR
    CALL RHS
    IF(IVISC.EQ.1)CALL VPHS
C* CALCULATE RESIDUAL
    DO 40 I=1,IL
    DO 40 J=1,JL
    DO 40 K=1,4
40   DQ(I,J,K)=-DELTAU(I,J)*DQ(I,J,K)
C* AVE SAI-DIRECTION 4TH ORDER ARTIFICIAL VISCOSITY
    IF(OMEGAX.NE.O.ODO)CALL ADDX
C* AVE ETA-DIRECTION 4TH ORDER ARTIFICIAL VISCOSITY
    IF(OMEGAY.NE.O.ODO)CALL ADDY
C* SOLVE LSAI-OPERATOR
    JEND=JL
    IF(IVISC.EQ.1)JEND=JL1
    DO 50 J=2,JEND
50   CALL COEFX(J)
C* SOLVE LETA-OPERATOR
    IEND=IL1
    IF(ISUP.EQ.1.OR.ISUP.EQ.3)IEND=IL
    DO 55 I=2,IEND
55   CALL COEFY(I)
C* UPDATING VARIABLES
    EIGMAX=0.
    IREG=1
    IF(ISUP.EQ.3)IBEG=2
    DO 70 I=IBEG,IL
    DO 70 J=2,JEND
    RJJ=RJ(I,J)/Y(I,J)
    DO 60 K=1,4
60   Q(I,J,K)=Q(I,J,K)+DQ(I,J,K)*RJJ
    TCP=O.DO

```

```

CALL CPGAM(CP(I,J),CV(I,J),GAMMA(I,J),GM1(I,J),RGAS,I,J,
> RHO(I,J),RHOU(I,J),RHOV(I,J),E(I,J),TCP)
U(I,J)=RHOU(I,J)/RHO(I,J)
V(I,J)=RHOV(I,J)/RHO(I,J)
UN(I,J)=U(I,J)*SAIX(I,J)+V(I,J)*SAIY(I,J)
VN(I,J)=U(I,J)*ETAX(I,J)+V(I,J)*ETAY(I,J)
P(I,J)=GM1(I,J)*(E(I,J)-0.5*RHO(I,J)*(U(I,J)**2+V(I,J)**2))
CO=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
ZM=DSQRT(U(I,J)**2+V(I,J)**2)/CO
IF(COND.GT.0.0.AND.ZM.LT.1.0) GOTO 210
CX=DSQRT(SAIX(I,J)*SAIX(I,J)+SAIY(I,J)*SAIY(I,J))
CY=DSQRT(ETAX(I,J)*ETAX(I,J)+ETAY(I,J)*ETAY(I,J))
CX=(UN(I,J)+CX*CO)/EXI
CY=(VN(I,J)+CY*CO)/EYI
C EIGNN=DABS(CX)
C IF(DABS(CY).GT.EIGNN) EIGNN=DABS(CY)
EIGNN=DSQRT(CX**2+CY**2)
IF(EIGNN.GT.EIGMAX)EIGMAX=EIGNN
DELTAU(I,J)=ITIME*CFL/EIGNN+(1-ITIME)*DELTAU(I,J)
GOTO 70
210 CONTINUE
SX=UN(I,J)**2*(1.DO-ZM**2)**2+4.DO*(U(I,J)**2+V(I,J)**2)
> *(SAIX(I,J)**2+SAIY(I,J)**2)
SY=VN(I,J)**2*(1.DO-ZM**2)**2+4.DO*(U(I,J)**2+V(I,J)**2)
> *(ETAX(I,J)**2+ETAY(I,J)**2)
EIGVX=0.5DO*(UN(I,J)*(1.DO+ZM**2)+DSQRT(SX))
EIGVY=0.5DO*(VN(I,J)*(1.DO+ZM**2)+DSQRT(SY))
DELTAU(I,J)=CFL/DSQRT(EIGVX**2+EIGVY**2)
70 CONTINUE
C *
C * CENTERLINE BOUNDARY CONDITIONS
CALL CLBC
IF(IVISC.EQ.1)CALL WALLBC
RETURN
END
C*
C* SUBROUTINE FOR CALCULATING METRIC TERMS
C* AT THE MIDPOINT
SUBROUTINE MCONST
***** IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=100)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
> P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
> ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
> ,ZMUT(IZ,JZ)
> ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
> PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF,COND
COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))

```

```

C*****+
      DATA FD3,OD3/1.333333333333,0.333333333333/
      DO 20 I=2,IL
      DO 20 J=1,JL1
      IF(I.EQ.IL)THEN
      XSAI=0.5*(X(I,J)+X(I,J+1)-X(I-1,J)-X(I-1,J+1))
      YSAI=0.5*(Y(I,J)+Y(I,J+1)-Y(I-1,J)-Y(I-1,J+1))
      ELSE
      YSAI=0.25*(Y(I+1,J+1)+Y(I+1,J)-Y(I-1,J+1)-Y(I-1,J))
      XSAI=0.25*(X(I+1,J+1)+X(I+1,J)-X(I-1,J+1)-X(I-1,J))
      END IF
      YETA=Y(I,I+1)-Y(I,J)
      XETA=X(I,J+1)-X(I,J)
      RJJ=1./(XSAI*YETA-XETA*YSAI)
      A1(I,J)=RJJ*(FD3*YSAI**2+XSAI**2)
      A2(I,J)=-RJJ*OD3*XSAI*YSAI
      A3(I,J)=RJJ*(YSAI**2+FD3*XSAI**2)
      A4(I,J)=RJJ*(XSAI**2+YSAI**2)
20    CONTINUE
      RETURN
      END
C-----+
C*          SUBROUTINE SMOOTH
C*
C*  ADD ARTIFICIAL DISSIPATIONAL TERM FOR SAI,ETA-DIRECTION
C*
C*****+
      IMPLICIT REAL*8(A-H,O-Z)
      PARAMETER (IZ=150,JZ=100)
      COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
      >           P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
      COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
      >           ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
      >           ,ZMUT(IZ,JZ)
      >           ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
      COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
      >           PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF,COND
      COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
      COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
      DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
      EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
      >           (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****+
      DIMENSION ADD(4)
      DIMENSION PRE(4,4),PADD(4)
C ** SAI-DIRECTION
      ENTRY ADDX
      COFF=0.125DO*OMEGAX
      DO 70 J=1,JL
      DO 70 I=1,IL
      IF(I.EQ.1) GO TO 10
      IF(I.EQ.2) GO TO 20
      IF(I.EQ.IL1) GO TO 30
      IF(I.EQ.IL) GO TO 40
      DO 5 K=1,4

```

```

5   ADD(K)=COEF*(Q(I+2,J,K)-4.*Q(I+1,J,K)
>      +6.*Q(I,J,K)-4.*Q(I-1,J,K)
>      +Q(I-2,J,K))
GO TO 50
10  DO 15 K=1,4
QM=2.*Q(1,J,K)-Q(2,J,K)
QMM=2.*QM-Q(1,J,K)
15  ADD(K)=COEF*(Q(I+2,J,K)-4.*Q(I+1,J,K)
>      +6.*Q(I,J,K)-4.*QM+QMM)
GO TO 50
20  DO 25 K=1,4
QMM=2.*Q(1,J,K)-Q(2,J,K)
25  ADD(K)=COEF*(Q(I+2,J,K)-4.*Q(I+1,J,K)
>      +6.*Q(I,J,K)-4.*Q(I-1,J,K)
>      +QMM)
GO TO 50
30  DO 35 K=1,4
QFP=2.*Q(I+1,J,K)-Q(I,J,K)
35  ADD(K)=COEF*(QPP-4.*Q(I+1,J,K)+6.*Q(I,J,K)
>      -4.*Q(I-1,J,K)+Q(I-2,J,K)
>      )
GO TO 50
40  DO 45 K=1,4
QP=2.*Q(I,J,K)-Q(I-1,J,K)
QPP=2.*QP-Q(I,J,K)
45  ADD(K)=COEF*(QPP-4.*QP+6.*Q(I,J,K)-4.*Q(I-1,J,K)+Q(I-2,J,K))
50  CONTINUE
CALL PRECON(I,J,PRE)
CALL MMV(4,PRE,ADD,PADD)
DO 60 K=1,4
60  DQ(I,J,K)=DQ(I,J,K)-PADD(K)/RJ(I,J)*Y(I,J)
70  CONTINUE
RETURN
C ***
C   ADD Eta-DIRECTLON 4TH ORDER ARTFLCLAL VLSCOSLTY
C ***
ENTRY ADDY
COEF=0.125DO*OMEGAY
DO 170 I=1,IL
DO 170 J=1,JL
IF(J.EQ.1) GO TO 110
IF(J.EQ.2) GO TO 120
IF(J.EQ.JL1) GO TO 130
IF(J.EQ.JL) GO TO 140
DO 95 K=1,4
95  ADD(K)=COEF*(Q(I,J+2,K)-4.*Q(I,J+1,K)
>      +6.*Q(I,J,K)-4.*Q(I,J-1,K)
>      +Q(I,J-2,K))
GO TO 150
110 DO 115 K=1,4
QM=2.*Q(I,1,K)-Q(I,2,K)
QMM=2.*QM-Q(I,1,K)
115 ADD(K)=COEF*(Q(I,J+2,K)-4.*Q(I,J+1,K)
>      +6.*Q(I,J,K)-4.*QM+QMM)

```

```

      GO TO 150
120  DO 125 K=1,4
      QMM=2.*Q(I,1,K)-Q(I,2,K)
125  ADD(K)=COEF*(Q(I,J+2,K)-4.*Q(I,J+1,K)
      > +6.*Q(I,J,K)-4.*Q(I,J-1,K)
      > +QMM)
      GO TO 150
130  DO 135 K=1,4
      QPP=2.*Q(I,J+1,K)-Q(I,J,K)
135  ADD(K)=COEF*(QPP-4.*Q(I,J+1,K)+6.*Q(I,J,K)
      > -4.*Q(I,J-1,K)+Q(I,J-2,K)
      > )
      GO TO 150
140  DO 145 K=1,4
      QP=2.*Q(I,J,K)-Q(I,J-1,K)
      QPP=2.*QP-Q(I,J,K)
145  ADD(K)=COEF*(QPP-4.*QP+6.*Q(I,J,K)-4.*Q(I,J-1,K)+Q(I,J-2,K))
150  CONTINUE
      CALL PRECON(I,J,PRE)
      CALL MMV(4,PRE,ADD,PADD)
      DO 160 K=1,4
160  DQ(I,J,K)=DQ(I,J,K)-PADD(K)/RJ(I,J)*Y(I,J)
170  CONTINUE
      RETURN
      END

```

```

C
C ** SUBROUTINE FOR CENTER LINE BOUNDARY CONDITIONS
C-----SUBROUTINE BC
C-----IMPLICIT REAL*8(A-H,O-Z)
C-----PARAMETER (IZ=150,JZ=100)
C-----COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
C-----> P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
C-----COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
C-----> ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
C-----> ,ZMUT(IZ,JZ)
C-----> ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
C-----COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
C-----> PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF,COND
C-----COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
C-----COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
C-----DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
C-----EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
C-----> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****DIMENSION AM(IZ),BM(IZ),CM(IZ),DM(IZ),PTEMP(IZ)
C-----DATA SCONST/110./
C-----ENTRY CLBC

```

C * THE QUANTITIES EXTRAPOLATED ARE U,P,T AND LET V=0

```

C
      IF(ISUP.EQ.3)THEN
      I1=2
      ELSE
      I1=1

```

```

END IF
DO 20 I=11,IL
SY=SAIY(I,1)
EY=ETAY(I,1)
DENOM=SY-1.5*EY
IF(I.EQ.1)THEN
UIM1=0.
PIM1=0.
RIM1=1.0
ELSE
UIM1=U(I-1,1)
PIM1=P(I-1,1)
RIM1=RHO(I-1,1)
END IF
V(I,1)=0.
U(I,1)=(SY*UIM1-0.5*EY*(4.*U(I,2)-U(I,3)))/DENOM
UN(I,1)=SAIX(I,1)*U(I,1)
VN(I,1)=ETAX(I,1)*U(I,1)
P(I,1)=(SY*PIM1-0.5*EY*(4.*P(I,2)-P(I,3)))/DENOM
RIV=1./RGAS
TIM1=PIM1/RIM1*RIV
T2=P(I,2)/RHO(I,2)*RIV
T3=P(I,3)/RHO(I,3)*RIV
T1=(SY*TIM1-0.5*EY*(4.*T2-T3))/DENOM
CALL CPGAM(CP(I,1),CV(I,1),GAMMA(I,1),GM1(I,1),RGAS,I,1,
> RHO(I,1),RHOU(I,1),RHOV(I,1),E(I,1),T1)
RHO(I,1)=P(I,1)/T1*RIV
RHOU(I,1)=RHO(I,1)*U(I,1)
RHOV(I,1)=RHO(I,1)*V(I,1)
E(I,1)=P(I,1)/GM1(I,1)+0.5*RHO(I,1)*(U(I,1)**2+V(I,1)**2)
20 CONTINUE
RETURN
C*
ENTRY WALLBC
J=JL
IBEG=1
IF(ISUP.EQ.3)IBEG=2
C* SOLVE THE PRESSURE EQUATION
IF(ISUP.NE.3)THEN
AM(1)=0.
BM(1)=1.5*(ETAX(1,J)**2+ETAY(1,J)**2)-(SAIX(1,J)*
> ETAX(1,J)+SAIY(1,J)*ETAY(1,J))
CM(1)=SAIX(1,J)*ETAX(1,J)+SAIY(1,J)*ETAY(1,J)
DM(1)=(ETAX(1,J)**2+ETAY(1,J)**2)*(2.*P(1,J-1)-0.5*P(1,J-2))
ELSE
AM(1)=0.
BM(1)=1.
CM(1)=0.
DM(1)=P(1,J)
ENDIF
DO 30 I=2,IL1
CC1=SAIX(I,J)*ETAX(I,J)+SAIY(I,J)*ETAY(I,J)
CC2=ETAX(I,J)**2+ETAY(I,J)**2
AM(I)=-0.5*CC1
BM(I)=1.5*CC2

```

```

CM(I)=0.5*CC1
DM(I)=CC2*(2.*P(I,J-1)-0.5*P(I,J-2))
30  CONTINUE
    CC1=SAIX(IL,J)*ETAX(IL,J)+SAIY(IL,J)*ETAY(IL,J)
    CC2=ETAX(IL,J)**2+ETAY(IL,J)**2
    AM(IL)=-CC1
    BM(IL)=CC1+1.5*CC2
    CM(IL)=0.
    DM(IL)=CC2*(2.*P(IL,J-1)-0.5*P(IL,J-2))
    CALL SYH(1,IL,AM,BM,CM,DM)
    DO 32 I=1,IL
32  PTEMP(I)=DM(I)
    RIV=1./RGAS
    IF(IWALL.EQ.0)THEN
        IF(ISUP.EQ.3)THEN
            DM(I)=P(I,J)*RIV/RHO(I,J)
        ELSE
            T1=P(I,J-1)*RIV/RHO(I,J-1)
            T2=P(I,J-2)*RIV/RHO(I,J-2)
            CC2=ETAX(I,J)**2+ETAY(I,J)**2
            DM(I)=CC2*(2.*T1-0.5*T2)
        END IF
    DO 34 I=2,IL
        CC2=ETAX(I,J)**2+ETAY(I,J)**2
        T1=P(I,J-1)*RIV/RHO(I,J-1)
        T2=P(I,J-2)*RIV/RHO(I,J-2)
34  DM(I)=CC2*(2.*T1-0.5*T2)
    CALL SYH(1,IL,AM,BM,CM,DM)
    ELSE
    ENDIF
    DO 40 I=IBEG,IL
    IF(IWALL.EQ.0)THEN
        TT=DM(I)
    ELSE
        TT=TWALL
    ENDIF
    PP=PTEMP(I)
    U(I,JL)=0.
    V(I,JL)=0.
    RHOU(I,JL)=0.
    RHOV(I,JL)=0.
    RHOO=PP*RIV/TT
    RHO(I,JL)=RHOO
    CALL CPCAM(CP(I,JL),CV(I,JL),GAMMA(I,JL),GM1(I,JL),RGAS,I,JL,
> RHO(I,JL),RHOU(I,JL),RHOV(I,JL),E(I,JL),TT)
    E(I,JL)=PP/GM1(I,JL)
    P(I,JL)=PP
    UN(I,JL)=0.
    VN(I,JL)=0.
40  CONTINUE
    RETURN
C*
C* LAMINAR VISCOSITY CALCULATION
C+
C   ENTRY MULAM

```

```

C* USE SUTHERLAND LAW
C   DO 60 I=1,IL
C   DO 60 J=1,JL
C   TOS=TREF+SCONST
C   TT=(E(I,J)/RHO(I,J)-0.5*(U(I,J)**2+V(I,J)**2))/CV(I,J)
C   TTS=TT+SCONST
C   ZMU(I,J)=ZMUO*TOS/TTS*(TT/TREF)**1.5
C   ZMU(I,J)=ZMUO
C   ZMU(I,J)=ZMUO*(TT/TREF)**0.67
C 60  CONTINUE
C   RETURN
C   END
C*****SUBROUTINE MULAM*****
C*****IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=100)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
>           P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
>           ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
>           ,ZMUT(IZ,JZ)
>           ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
>           PRNT,PB,RM1,SUM(4),ZMUC,REN,PRN,TWALL,TREF,COND
COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
>           (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****B1=4.3222557667160623D-06
B2=3.8885996244952953D-08
B3=-3.7263546610032919D-12
DO 50 NN=1,IL
DO 50 MM=1,JL
TT=(E(NN,MM)/RHO(NN,MM)-0.5*(U(NN,MM)**2+V(NN,MM)**2))/CV(NN,MM)
ZMU(NN,MM)=B1+B2*TT+B3*TT*TT
50  CONTINUE
      RETURN
      END
C
C   BOLDWIN & LOMAX TURBULENCE MODEL
C
C*****SUBROUTINE MUTUR*****
C*****IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=100)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
>           P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
>           ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
>           ,ZMUT(IZ,JZ)
>           ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,

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      PRNT, PB, RM1, SUM(4), ZMUO, REN, PRN, TWALL, TREF, COND
COMMON/CONST1/CP(IZ,JZ), CV(IZ,JZ), GAMMA(IZ,JZ), GM1(IZ,JZ), RGAS
COMMON/INTEG/IL, JL, IL1, JL1, NEND, NBEG, NADV, ITIME, ISUP, IVISC, IWALL
DIMENSION RHO(IZ,JZ), RHOU(IZ,JZ), RHOV(IZ,JZ), E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
           (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****+
DIMENSION YVERT(JZ), ZMUI(JZ)
DATA AP, CCP, CKLEB, CWK, VKCON, XK/26., 1.6, .3, .25, .4, .0168/
DATA ZMUI/JZ*0.0/
DO 991 II=1, IL
  I=II
  FYMAX = 0.0
  YMAX = 0.0
  UDIF=0.
  YVERT(JL) = 0.0
  TAUW = ZMU(I, JL)*DABS(ETAY(I, JL)*(U(I, JL)-U(I, JL-1))-
                           ETAX(I, JL)*(V(I, JL)-V(I, JL-1)))
  CYP = DSQRT(RHO(I, JL)*TAUW)/ZMU(I, JL)
C
  DO 10 KK = 2, JL1
    K = JL+1-KK
    YVER = YVERT(K+1) + 1.0/DSQRT(ETAX(I, K)**2 + ETAY(I, K)**2)
    OMG = DABS( ETAY(I, K)*(U(I, K+1)-U(I, K-1)).5
               +SAIY(I, K)*(U(I, K) -U(I-1, K))
               -ETAX(I, K)*(V(I, K+1)-V(I, K-1)).5
               -SAIX(I, K)*(V(I, K) -V(I-1, K)) )
    YPLUS = CYP*YVER
    TURLEN = VKCON*YVER*(1.0D0 -DEXP(-YPLUS/AP))
    ZMUI(K) = RHO(I, K)*OMG*TURLEN**2
    FY = TURLEN/VKCON*OMG
    UTOTAL= DSQRT(U(I, K)**2+V(I, K)**2)
    IF(UTOTAL.GE.UDIF) UDIF=UTOTAL
    IF(FY .LT. FYMAX) GO TO 10
    FYMAX = FY
    YMAX = YVER
  10  YVERT(K) = YVER
C
  VXDIF = UDIF
C
  WRITE(6,*) II, K, TURLEN, YVER, OMG, FY, FYMAX
  FWAKE1=YMAX*FYMAX
  FWAKE2=CWK*YMAX*VXDIF**2/FYMAX
  FWAKE =DMIN1(FWAKE1, FWAKE2)
C
  DO 20 KK = 2, JL1
    K = JL+1-KK
    FKLEB = (CKLEB*YVERT(K)/YMAX)**6
    FKLEB = 1./(1.0 + 5.5*FKLEB)
    ZMUO = XK*CCP*RHO(I, K)*FWAKE*FKLEB
    IF(ZMUI(K).GT.ZMUO) THEN
      ZMUTUR = ZMUO
    ELSE
      ZMUTUR = ZMUI(K)
    END IF
    ZMUT(I, K)= ZMUTUR

```

FILE: AXI2DV FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STA

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ZMU(I,K) = ZMU(I,K) + ZMUTUR
C      WRITE(77,119)K,Y(I,K),YVERT(K),U(I,K),ZMUI(K),ZMUO,ZMU(I,K)
C114  FORMAT(2X,I3,6(2X,D13.6))
20    CONTINUE
C
ZMUT(I,1)=0.
ZMUT(I,JL)=0.
991 CONTINUE
RETURN
END
C* SOURCE TERM JACOBIAN MATRIX
SUBROUTINE DHDQ(D,I,J)
C-----+
IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=100)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
> ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
> ,ZMUT(IZ,JZ)
> ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF,COND
COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****+
DIMENSION D(4,4)
CALL SZERO(4,D)
IF(IVISC.EQ.0)THEN
R2MY=0.
ELSE
R2MY=4./3.*ZMU(I,J)/(Y(I,J)*Y(I,J)*RHO(I,J))
END IF
D(3,1)=.5*GM1(I,J)*(U(I,J)**2+V(I,J)**2)/Y(I,J)+IVISC*V(I,J)*R2MY
D(3,2)=-GM1(I,J)*U(I,J)/Y(I,J)
D(3,3)=-GM1(I,J)*V(I,J)/Y(I,J)-IVISC*R2MY
D(3,4)=GM1(I,J)/Y(I,J)
RETURN
END
SUBROUTINE JACCAL
C*
C* SUBROUTINE FOR JACOBIAN METRIX
C* IF IA=1, ACAP MATRIX
C* IF IA=2, BCAP MATRIX
C*
C*****+
IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=100)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
> ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
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```

` ,ZMUT(IZ,JZ)
` ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
` PRNT,PB,RM1,SUM(4),ZM0,REN,PRN,TWALL,TREF,COND
COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
` (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****+
DIMENSION A(4,4),B(4,4),C(4,4)
C*****
ENTRY JACCB(IA,A,I,J)
IF(IA.EQ.2)GO TO 10
CX=SAIX(I,J)
CY=SAIY(I,J)
CONTRA=UN(I,J)
GO TO 20
10 CX=ETAX(I,J)
CY=ETAY(I,J)
CONTRA=VN(I,J)
20 CONTINUE
PHI2=0.5D0*GM1(I,J)*(U(I,J)**2+V(I,J)**2)
A(1,1)=0.0D0
A(1,2)=CX
A(1,3)=CY
A(1,4)=0.D0
A(2,1)=CX*PHI2-U(I,J)*CONTRA
A(2,2)=CONTRA-(GAMMA(I,J)-2.)*CX*U(I,J)
A(2,3)=CY*U(I,J)-GM1(I,J)*CX*V(I,J)
A(2,4)=GM1(I,J)*CX
A(3,1)=CY*PHI2-V(I,J)*CONTRA
A(3,2)=CX*V(I,J)-GM1(I,J)*CY*U(I,J)
A(3,3)=CONTRA-CY*V(I,J)*(GAMMA(I,J)-2.)
A(3,4)=GM1(I,J)*CY
A(4,1)=CONTRA*(2.D0*PHI2-GAMMA(I,J)*E(I,J)/RHO(I,J))
A(4,2)=CX*(GAMMA(I,J)*E(I,J)/RHO(I,J)-PHI2)-GM1(I,J)*CONTRA*U(I,J)
A(4,3)=CY*(GAMMA(I,J)*E(I,J)/RHO(I,J)-PHI2)-GM1(I,J)*CONTRA*V(I,J)
A(4,4)=GAMMA(I,J)*CONTRA
RETURN
C* VISCOS TERM JACOBIAN MATRIX
C*
ENTRY VJACOB(A,B,C,I,J)
JP1=J+1
JM1=J-1
ZMUP=0.5*(ZMU(I,J)+ZMU(I,JP1))
ZMUM=0.5*(ZMU(I,J)+ZMU(I,JM1))
YYP =0.5*(Y(I,J)+Y(I,JP1))
YYM =0.5*(Y(I,J)+Y(I,JM1))
YJP =RJ(I,JP1)/Y(I,JP1)
IF(JM1.EQ.1)THEN
YJM=0.
ELSE
YJM =RJ(I,JM1)/Y(I,JM1)
ENDIF

```

```
IF(PRNT.EQ.0.DO) THEN
GAMP=0.5*(GAMMA(I,J)+GAMMA(I,J+1))
GAMM=0.5*(GAMMA(I,J)+GAMMA(I,J-1))
GKCPP=ZMUP*GAMP/PRN
GKCPM=ZMUM*GAMM/PRN
ELSE
ZMUTP = 0.5*(ZMUT(I,JP1)+ZMUT(I,J))
ZMUTM = 0.5*(ZMUT(I,JM1)+ZMUT(I,J))
ZMULP = ZMUP - ZMUTP
ZMULM = ZMUM - ZMUTM
GAMP=0.5*(GAMMA(I,J)+GAMMA(I,J+1))
GAMM=0.5*(GAMMA(I,J)+GAMMA(I,J-1))
GKCPP = GAMP*(ZMULP/PRN+ZMUTP/PRNT)
GKCPM = GAMM*(ZMULM/PRN+ZMUTM/PRNT)
ENDIF
EXJ=ETAX(I,J)/RJ(I,J)
EYJ=ETAY(I,J)/RJ(I,J)
ZMUU=ZMU(I,J)
OR=1./RHO(I,J)
ORP=1./RHO(I,JP1)
ORM=1./RHO(I,JM1)
ZMURP=ZMU(I,JP1)*ORP
ZMURM=ZMU(I,JM1)*ORM
UR =U(I,J)*OR
URP=U(I,JP1)*ORP
URM=U(I,JM1)*ORM
VR =V(I,J)*OR
VRM=V(I,JM1)*ORM
VRP=V(I,JP1)*ORP
UMRP=URP*ZMU(I,JP1)
UMRM=URM*ZMU(I,JM1)
VMRP=VRP*ZMU(I,JP1)
VMRM=VRM*ZMU(I,JM1)
U2R =UR*U(I,J)
U2RP=URP*U(I,JP1)
U2RM=URM*U(I,JM1)
V2R =VR*V(I,J)
V2RP=VRP*V(I,JP1)
V2RM=VRM*V(I,JM1)
UVR =UR*V(I,J)
UVRP=URP*V(I,JP1)
UVRM=URM*V(I,JM1)
ER2 =E(I,J)*OR**2
ER2P=E(I,JP1)*ORP**2
ER2M=E(I,JM1)*ORM**2
ZRYJP=ZMURP*YJP
ZRYJM=ZMURM*YJM
ORYJP=ORP*YJP
ORYJM=ORM*YJM
VMRP=-ZMURP*V(I,JP1)*YJP
VMRM=-ZMURM*V(I,JM1)*YJM
URYJP=-URP*YJP
URYJM=-URM*YJM
VYJP=2.*ZMU(I,JP1)*VRP*YJP
VYJM=2.*ZMU(I,JM1)*VRM*YJM
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```

V2YJP=-V2RP*2.*ZMU(I,JP1)*YJP
V2YJM=-V2RM*2.*ZMU(I,JM1)*YJM
UVYJP=-2.*ZMU(I,JP1)*UVRP*YJP
UVYJM=-2.*ZMU(I,JM1)*URM*YJM
VYJP2=VYJP*0.5
VYJM2=0.5*VYJM
UYJP=ZMU(I,JP1)*URP*YJP
UYJM=ZMU(I,JM1)*URM*YJM
AAP1= ZMUP*A1(I,J)*YYP
AAP2= ZMUP*A2(I,J)*YYP
AAP3= ZMUP*A3(I,J)*YYP
AAP4= GKCPP*A4(I,J)*YYP
AAM1= ZMUM*A1(I,JM1)*YYM
AAM2= ZMUM*A2(I,JM1)*YYM
AAM3 =ZMUM*A3(I,JM1)*YYM
AAM4 =GKCPM*A4(I,JM1)*YYM
IF(JM1.EQ.1)THEN
CALL SZERO(‡,A)
ELSE
A(1,1) =0.
A(1,2) =0.
A(1,3) =0.
A(1,4) =0.
A21=(AAM1*URM+AAM2*VRM)*RJ(I,JM1)/Y(I,JM1)
A(2,1) =A21-1./3.*EXJ*VMRM
A(2,2) =-AAM1*ORM*RJ(I,JM1)/Y(I,JM1)
A(2,3) =-AAM2*ORM*RJ(I,JM1)/Y(I,JM1)-1./3.*EXJ*ZRYJM
A(2,4) =0.
A31=(AAM2*URM+AAM3*VRM)*RJ(I,JM1)/Y(I,JM1)
A(3,1) =A31+1./3.*ZMU(I,J)
*          *EXJ*URYJM
A(3,2) =-AAM2*ORM*RJ(I,JM1)/Y(I,JM1)+1./3.*ZMU(I,J)*EXJ*ORYJM
A(3,3) =-AAM3*ORM*RJ(I,JM1)/Y(I,JM1)
A(3,4) =0.
A(4,1) =(-AAM4*(-ER2M+U2RM+V2RM)+AAM1*U2RM+AAM3*V2RM+
+          2.*AAM2*VRM)*RJ(I,JM1)/Y(I,JM1)-
+          1./3.*EYJ*V2YJM-1./3.*EXJ*UVYJM
A(4,2) =AAM4*URM*RJ(I,JM1)/Y(I,JM1)-A21-1./3.*EXJ*VYJM2
A(4,3) =AAM4*VRM*RJ(I,JM1)/Y(I,JM1)-A31-1./3.*EYJ*VYJM-
*          1./3.*EXJ*UYJM
A(4,4) =-AAM4*ORM*RJ(I,JM1)/Y(I,JM1)
ENDIF
C(1,1) =0.
C(1,2) =0.
C(1,3) =0.
C(1,4) =0.
C21=(AAP1*URP+AAP2*VRP)*RJ(I,JP1)/Y(I,JP1)
C(2,1) =C21+1./3.*EXJ*VMRP
C(2,2) =-AAP1*ORP*RJ(I,JP1)/Y(I,JP1)
C(2,3) =-AAP2*ORP*RJ(I,JP1)/Y(I,JP1)+1./3.*EXJ*ZRYJP
C(2,4) =0.
C31=(AAP2*URP+AAP3*VRP)*RJ(I,JP1)/Y(I,JP1)
C(3,1) =C31-1./3.*ZMU(I,J)
*          *EXJ*URYJP
C(3,2) =-AAP2*ORP*RJ(I,JP1)/Y(I,JP1)-1./3.*ZMU(I,J)*EXJ*ORYJP

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C(3,3) =-AAP3*ORP*RJ(I,JP1)/Y(I,JP1)
C(3,4) =0.
C(4,1) =(-AAP4*(-ER2P+U2RP+V2RP)+AAP1*U2RP+AAP3*V2RP+
2.*AAP2*UVRP)*RJ(I,JP1)/Y(I,JP1) +
1./3.*EYJ*V2YJP+1./3.*EXJ*UVYJP
C(4,2) =AAP4*URP*RJ(I,JP1)/Y(I,JP1)-C21+1./3.*EXJ*VYJP2
C(4,3) =AAP4*VRP*RJ(I,JP1)/Y(I,JP1)-C31+1./3.*EYJ*VYJP+
1./3.*EXJ*UYJP
C(4,4) =-AAP4*ORP*RJ(I,JP1)/Y(I,JP1)
AAM=AAP1+AAM1
AAP=AAP2+AAM2
AAB=AAP3+AAM3
AAC=AAP4+AAM4
P(1,1)=0.
S(1,2)=0.
R(1,3)=0.
B(1,4)=0.
B(1,1)=(-AA1*UR-AA2*VR)*RJ(I,J)/Y(I,J)
B(1,2)=AA1*OR*RJ(I,J)/Y(I,J)
B(1,3)=AA2*OR*RJ(I,J)/Y(I,J)
B(1,4)=0.
B(2,1)=(-AA2*UR-AA3*VR)*RJ(I,J)/Y(I,J)
B(2,2)=AA2*OR*RJ(I,J)/Y(I,J)
B(2,3)=AA3*OR*RJ(I,J)/Y(I,J)
B(2,4)=0.
B(3,1)=(AA4*(-ER2+U2R+V2R)-AA1*U2R-AA3*V2R-
2.*AA2*UVR)*RJ(I,J)/Y(I,J)
B(3,2)=-AA4*UR*RJ(I,J)/Y(I,J)-B(2,1)
B(3,3)=-AA4*VR*RJ(I,J)/Y(I,J)-B(3,1)
B(3,4)=AA4*OR*RJ(I,J)/Y(I,J)
RETURN
END
*****
```

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*** SUBROUTINE FOR COMPUTING PRECONDITIONER
***
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SUBROUTINE PRECON(I,J,A)
*****
```

 $\text{IMPLICIT REAL*8(A-H,O-Z)}$
 $\text{PARAMETER (IZ=150,JZ=100)}$
 $\text{COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),}$
 $\text{P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)}$
 $\text{COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ),}$
 $\text{RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)}$
 ,ZMUT(IZ,JZ)
 $\text{,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)}$
 $\text{COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,}$
 $\text{PRNT,PB,RM1,SUM(4),ZMU0,REN,PRN,TWALL,TREF,COND}$
 $\text{COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS}$
 $\text{COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL}$
 $\text{DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)}$
 $\text{EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),}$
 $\text{(Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))}$
 DIMENSION A(4,4)

```

CALL SZERO(4,A)
```

```

CO=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
ZM=DSQRT(U(I,J)**2+V(I,J)**2)/CO
IF(COND.GT.0.0.AND.ZM.LT.1.0) GO TO 100
DO 1 MM=1,4
1 A(MM,MM)=1.0D0
RETURN
100 CONTINUE
ALPHA=U(I,J)*U(I,J)+V(I,J)*V(I,J)
CON=CO*CO/ALPHA
CONM1=CON-1.0D0
A(1,1)=1.0D0
A(2,2)=1.0D0
A(3,3)=1.0D0
A(4,1)=0.5D0*ALPHA*CONM1
A(4,2)=-U(I,J)*CONM1
A(4,3)=-V(I,J)*CONM1
A(4,4)=CON
RETURN
END
C-----
      SUBROUTINE EIGEN(IA,A,I,J)
C*
C*   SUBROUTINE FOR EIGENVECTOR MATRIX CALCULATION
C*   IF IA=1  L FOR ACAP
C*   IF IA=2  L FOR BCAP
C*
C*****+
IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=100)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
     P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
     ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
     ,ZMUT(IZ,JZ)
     ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
     PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF,COND
COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
     (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****+
DIMENSION A(4,4),C(IZ,JZ)
C*****+
CO=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
C(I,J)=CO
ZM=DSQRT(U(I,J)**2+V(I,J)**2)/CO
C*
IF(COND.GT.0.0.AND.ZM.LT.1.0) GO TO 500
C*
C*   EIGENVECTOR FOR ORIGINAL EULER EQN
C*
IF(IA.EQ.2)GO TO 10
CX=SAIX(I,J)

```

FILE: AXI2DV FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STA

```
CY=SAIY(I,J)
GO TO 20
10 CX=ETAX(I,J)
CY=ETAY(I,J)
20 CONTINUE
SQ2=DSQRT(2.D0)
C C=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
C1=CX/DSQRT(CX**2+CY**2)
C2=CY/DSQRT(CX**2+CY**2)
A(1,1)=1.-0.5*GM1(I,J)*(U(I,J)**2+V(I,J)**2)/CO**2
A(1,2)=GM1(I,J)*U(I,J)/CO**2
A(1,3)=GM1(I,J)*V(I,J)/CO**2
A(1,4)=-GM1(I,J)/CO**2
A(2,1)=(-C2*U(I,J)+C1*V(I,J))/RHO(I,J)
A(2,2)=C2/RHO(I,J)
A(2,3)=-C1/RHO(I,J)
A(2,4)=0.
A(3,1)=-(C1*U(I,J)+C2*V(I,J))/SQ2/RHO(I,J) +
> 0.5/SQ2*GM1(I,J)*(U(I,J)**2+V(I,J)**2)/RHO(I,J)/CO
A(3,2)=C1/SQ2/RHO(I,J)-GM1(I,J)/SQ2*U(I,J)/RHO(I,J)/CO
A(3,3)=C2/SQ2/RHO(I,J)-GM1(I,J)/SQ2*V(I,J)/RHO(I,J)/CO
A(3,4)=GM1(I,J)/SQ2/RHO(I,J)/CO
A(4,1)=(C1*U(I,J)+C2*V(I,J))/SQ2/RHO(I,J)+0.5/SQ2*GM1(I,J)*
> (U(I,J)**2+V(I,J)**2)/RHO(I,J)/CO
A(4,2)=-C1/SQ2/RHO(I,J)-GM1(I,J)/SQ2*U(I,J)/RHO(I,J)/CO
A(4,3)=-C2/SQ2/RHO(I,J)-GM1(I,J)/SQ2*V(I,J)/RHO(I,J)/CO
A(4,4)=GM1(I,J)/SQ2/RHO(I,J)/CO
GOTO 600
C
C
500 CONTINUE
C*
C* EIGENVECTOR FOR PRECONDITIONED EULER EQN
C*
IF(IA.EQ.2) GO TO 50
IF(IA.NE.1) STOP 999
CX=SAIX(I,J)
CY=SAIY(I,J)
CONTRA=UN(I,J)
GO TO 60
50 CX=ETAX(I,J)
CY=ETAY(I,J)
CONTRA=VN(I,J)
60 CONTINUE
UU=U(I,J)**2+V(I,J)**2
XM=DSQRT(UU/C(I,J)**2)
QM=1.D0-XM**2
XMM=QM**2
AC=DSQRT(CONTRA**2*XMM+4.D0*C(I,J)**2*XM**2
> *(CX**2+CY**2))
A(1,1)=0.5D0+0.5D0*(V(I,J)*CX-U(I,J)*CY)/(RHO(I,J)*
> (CX**2+CY**2))-2.D0*QM*CONTRA**2/(XMM*CONTRA**2-AC**2)
> +GM1(I,J)*UU*(CX**2+CY**2)/(XMM*CONTRA**2-AC**2)
A(1,2)=0.5D0*CY/(RHO(I,J)*(CX**2+CY**2))+2.D0*
> CX*QM*CONTRA/(XMM*CONTRA**2-AC**2)
```

```

> -GM1(I,J)*U(I,J)*2.DO*(CX**2+CY**2)/(XMM*CONTRA**2-AC**2)
A(1,3)=-0.5DO*CX/(RHO(I,J)*(CX**2+CY**2))+2.DO*CY*QM*CONTRA
> /(XMM*CONTRA**2-AC**2)
> -GM1(I,J)*V(I,J)*2.DO*(CX**2+CY**2)/(XMM*CONTRA**2-AC**2)
A(1,4)=2.DO*GM1(I,J)*(CX**2+CY**2)/(XMM*CONTRA**2-AC**2)
A(2,1)=0.5DO+0.5DO*(U(I,J)*CY-V(I,J)*CX)/(RHO(I,J)
> *(CX**2+CY**2))
> -2.DO*QM*CONTRA**2/(XMM*CONTRA**2-AC**2)
> +GM1(I,J)*UU*(CX**2+CY**2)/(XMM*CONTRA**2-AC**2)
A(2,2)=-0.5DO*CY/(RHO(I,J)*(CX**2+CY**2))+2.DO*CX*QM*CONTRA/
> (XMM*CONTRA**2-AC**2)
> -GM1(I,J)*U(I,J)*2.DO*(CX**2+CY**2)/(XMM*CONTRA**2-AC**2)
A(2,3)=0.5DO*CX/(RHO(I,J)*(CX**2+CY**2))+2.DO*CY*QM*CONTRA/
> (XMM*CONTRA**2-AC**2)
> -GM1(I,J)*V(I,J)*2.DO*(CX**2+CY**2)/(XMM*CONTRA**2-AC**2)
A(2,4)=2.DO*GM1(I,J)*(CX**2+CY**2)/(XMM*CONTRA**2-AC**2)
A(3,1)=((QM*CONTRA+AC)*CONTRA-GM1(I,J)*UU*(CX**2+CY**2))
> /(AC*(QM*CONTRA-AC))
A(3,2)=(-CX*(QM*CONTRA+AC)+2.DO*GM1(I,J)*U(I,J)*(CX**2+CY**2))
> /(AC*(QM*CONTRA-AC))
A(3,3)=(-CY*(QM*CONTRA+AC)+2.DO*GM1(I,J)*V(I,J)*(CX**2+CY**2))
> /(AC*(QM*CONTRA-AC))
A(3,4)=-2.DO*GM1(I,J)*(CX**2+CY**2)/(AC*(QM*CONTRA-AC))
A(4,1)=(CONTRA*(QM*CONTRA-AC)-GM1(I,J)*UU*(CX**2+CY**2))
> /(AC*(QM*CONTRA+AC))
A(4,2)=(-CX*(QM*CONTRA-AC)+2.DO*GM1(I,J)*U(I,J)*(CX**2+CY**2))
> /(AC*(QM*CONTRA+AC))
A(4,3)=(-(QM*CONTRA-AC)*CY+2.DO*GM1(I,J)*V(I,J)*(CX**2+CY**2))
> /(AC*(QM*CONTRA+AC))
A(4,4)=-2.DO*GM1(I,J)*(CX**2+CY**2)/(AC*(QM*CONTRA+AC))

```

600 CONTINUE

```

RETURN
END

```

C-----

SUBROUTINE COEFX(J)

C*

C* SETTING COEFFICIENTS FOR LX-OPERATOR

C*

C*****

```

IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=100)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
> P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
> ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
> ,ZMUT(IZ,JZ)
> ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
> PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF,COND
COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****

```

```
DIMENSION IN(4),EE(4,4,IZ),EL(4,IZ),W(4,IZ)
DIMENSION AM(4,4),BM(4,4),CM(4,4),DM(4)
DIMENSION AL(4,4),BE(4)
DIMENSION A(4,4),AL1(4,4),D(4,4)
```

C

```
DIMENSION PA(4,4),PPD(4,4),PINV(4,4),PRE(4,4),AL2(4,4)
DIMENSION AM1(4,4),BM1(4,4),CM1(4,4),DM1(4),PIA(4,4)
DIMENSION EL(4,4),EINV(4,4),AA(4,4),GA(4,4),GA1(4,4),EG(4,4)
> ,AINV(4,4)
```

C*****

C*

C* UPSTREAM BOUNDARY CONDITION AT I=1

C*

```
I=1
TAUD=DELTAU(I,J)*THETA/EXI
IF (ISUP.EQ.3) GOTO 45
CALL SZERO(4,AM)
CALL JACOB(1,A,I,J)
CALL DHDQ(D,I,J)
CALL PRECON(I,J,PRE)
CALL EIGEN(1,AL1,I,J)
DO 951 M=1,3
DO 951 N=1,4
```

```
951 AL1(M,N)=0.D0
DO 901 MM=1,4
DO 901 NN=1,4
PPD(MM,NN)=PRE(MM,NN)-TAUD*D(MM,NN)
```

```
901 CONTINUE
CALL INVER(4,PPD,PINV)
CALL MMM(4,PINV,A,PA)
CALL MMM(4,AL1,PA,PIA)
CALL SZERO(4,BM)
```

```
DO 10 M=1,4
DO 10 N=1,4
BM(M,N)=AL1(M,N)-TAUD*PIA(M,N)
```

```
10 CONTINUE
RJYY=RJ(I,J)/Y(I,J)
RCV=RHO(I,J)*CV(I,J)
RJRCV=RJYY/RCV
BM(1,1)=(-E(I,J)/RHO(I,J)+GM1(I,J)/GAMMA(I,J)*(U(I,J)**2
> +V(I,J)**2))*RJRCV
BM(1,2)=-GM1(I,J)/GAMMA(I,J)*U(I,J)*RJRCV
BM(1,3)=-GM1(I,J)/GAMMA(I,J)*V(I,J)*RJRCV
BM(1,4)=RJRCV
```

C

```
BM(2,1)=-GAMMA(I,J)*E(I,J)/RHO(I,J)+(GAMMA(I,J)+1.)*AAA
BM(2,2)=-U(I,J)
BM(2,3)=-V(I,J)
BM(2,4)=1.D0
```

```
C1=(RHO(I,J)*E(I,J)-0.5*RHO(I,J)**2*(U(I,J)**2+V(I,J)**2))
C2=(RHO(I,J)*E(I,J)-0.5*GM1(I,J)/GAMMA(I,J)*RHO(I,J)**2*(U(I,J)**2
> +V(I,J)**2))
```

```
C3=(C2/C1)**(GAMMA(I,J)/GM1(I,J))
```

```
C4=GAMMA(I,J)/GM1(I,J)/C1*(C2/C1)**(1.D0/GM1(I,J))
```

```
BM(2,1)=(0.5*(U(I,J)**2+V(I,J)**2)*C3+C4*E(I,J)*(C1-C2)/RHO(I,J)
> )*GM1(I,J)*RJYY
```

```

BM(2,2)=(-U(I,J)*C3+C4*U(I,J)*(C2-GM1(I,J)/GAMMA(I,J)*C1))
> *GM1(I,J)*RJYY
BM(2,3)=(-V(I,J)*C3+C4*V(I,J)*(C2-GM1(I,J)/GAMMA(I,J)*C1))
> *GM1(I,J)*RJYY
BM(2,4)=(C3+C4*(C1-C2))*GM1(I,J)*RJYY
EM(3,1)=-VN(I,J)*RJYY/RHO(I,J)
BM(3,2)=ETAX(I,J)*RJYY/RHO(I,J)
BM(3,3)=ETAY(I,J)*RJYY/RHO(I,J)
BM(3,4)=0.
CALL SZERO(4,CM)
CALL JACOB(1,A,I+1,J)
CALL MMM(4,PINV,A,PA)
CALL MMM(4,AL1,PA,PIA)
DO 20 M=1,4
DO 20 N=1,4
CM(M,N)=-TAUD*PIA(M,N)
20 CONTINUE
DO 971 M=1,3
DO 971 N=1,4
971 CM(M,N)=0.DO
C*
      CALL MMM(4,AL1,PINV,AL2)
      DO 952 M=1,4
952 DM1(M)=DQ(I,J,M)
      CALL MMV(4,AL2,DM1,DM)
C*
      TON=(E(I,J)/RHO(I,J)-0.5*GM1(I,J)/GAMMA(I,J)*(U(I,J)**2
> +V(I,J)**2))/CV(I,J)
      TT =(E(I,J)/RHO(I,J)-0.5*(U(I,J)**2+V(I,J)**2))/CV(I,J)
      PON=P(I,J)*(TON/TT)**(GAMMA(I,J)/GM1(I,J))
      DM(1)=(TO-TON)
      DM(2)=(PO-PON)
      DM(3)=-VN(I,J)
      GOTO 49
45 CONTINUE
      CALL SZERO(4,AM)
      CALL SZERO(4,BM)
      CALL SZERO(4,CM)
      DO 46 M=1,4
      DM(M)=0.
      BM(M,M)=1.0
46 CONTINUE
49 CONTINUE
      CALL EEL(I,4,IL,EE,EL,AM,BM,CM,DM,IN,AL,BE)
C*
C* INTERIOR NODES
C*
      DO 70 I=2,IL1
      TAUD=0.5D0*DELTAU(I,J)*THETA/EXI
      TAUD2=2.*TAUD
      IM1=I-1
      IP1=I+1
      CALL PRECON(I,J,PRE)
      CALL JACOB(1,A,IM1,J)
      CALL DHDQ(D,I,J)

```

```

DO 902 MM=1,4
DO 902 NN=1,4
PPD(MM,NN)=PRE(MM,NN)-TAUD2*D(MM,NN)
902 CONTINUE
CALL INVER(4,PPD,PINV)
CALL MMM(4,PINV,A,PA)
CALL SMM(4,TAUD,PA,AM)
CALL SZERO(4,BM)
DO 50 M=1,4
50 BM(M,M)=BM(M,M)+1.
CALL JACOB(1,A,IP1,J)
CALL MMM(4,PINV,A,PA)
CALL SMM(4,-TAUD,PA,CM)
DO 961 M=1,4
961 DM1(M)=DQ(I,J,M)
CALL MMV(4,PINV,DM1,DM)

C
C
    CALL EEL(I,4,IL,EE,EL,AM,BM,CM,DM,IN,AL,BE)
70 CONTINUE
C*
C* DOWNSTREAM BOUDARY CONDITION AT I=IL
C*
    I=IL
    TAUD=DELTAU(I,J)*THETA/EXI
    CALL JACOB(1,A,I-1,J)
    CALL DHDQ(D,I,J)
    CALL PRECON(I,J,PRE)
    DO 903 MM=1,4
    DO 903 NN=1,4
    PPD(MM,NN)=PRE(MM,NN)-TAUD*D(MM,NN)
903 CONTINUE
    CALL INVER(4,PPD,PINV)
    IF(ISUP.EQ.1.OR.ISUP.EQ.3) GO TO 75
    CALL EIGEN(1,AL1,I,J)
    DO 71 N=1,4
71 AL1(4,N)=0.0D0
    CALL MMM(4,AL1,PA,AM1)
    CALL SMM(4,TAUD,AM1,AM)
    CALL JACOB(1,A,I,J)
    CALL MMM(4,PINV,A,PA)
C    DO 78 M=1,4
C    DO 78 N=1,4
C 78 A(M,N)=A(M,N)-D(M,N)
    CALL MMM(4,AL1,PA,BM)
    DO 72 M=1,4
    DO 72 N=1,4
72 BM(M,N)=BM(M,N)*TAUD+AL1(M,N)
    BM(4,1)=0.5*(U(I,J)*U(I,J)+V(I,J)*V(I,J))
    BM(4,2)=-U(I,J)
    BM(4,3)=-V(I,J)
    BM(4,4)=1.
    CALL SZERO(4,CM)
    CALL MMM(4,AL1,PINV,AL2)
    DO 73 M=1,4

```

```

DM(M)=0.
DO 73 K=1,4
73 DM(M)=DM(M)+AL2(M,K)*DQ(I,J,K)
IF(PB.NE.0.DO)THEN
DM(4)= (PB-P(IL,J))/GM1(IL,J)*Y(IL,J)/RJ(IL,J)
ENDIF
GO TO 95
75 CONTINUE
CALL MMM(4,PINV,A,PA)
CALL SMM(4,TAUD,PA,AM)
CALL JACOB(1,A,I,J)
CALL MMM(4,PINV,A,PA)
CALL SMM(4,TAUD,PA,BM)
DO 80 M=1,4
80 BM(M,M)=BM(M,M)+1.
CALL SZERO(4,CM)
DO 90 K=1,4
90 DM1(K)=DQ(I,J,K)
CALL MMV(4,PINV,DM1,DM)
95 CONTINUE
CALL EEL(I,4,IL,EE,EL,AM,BM,CM,DM,IN,AL,BE)

C*
C* SOLVE 4*4 BLOCK TRIDIAGONAL SYSTEM
C*
CALL SOLU(W,IL,4,EE,EL)
DO 100 I=1,IL
DO 100 K=1,4
DQ(I,J,K)=W(K,I)
100 CONTINUE
C* MULTIPY DQ BY I-DT*D
C   I2=IL
C   IF(ISUP.EQ.0)I2=IL1
C   DO 200 I=2,I2
C   CALL SZERO(4,BM)
C   CALL DHDQ(D,I,J)
C   DO 120 M=1,4
C   BM(M,M)=BM(M,M)+1.0
C   DO 120 N=1,4
C   BM(M,N)=BM(M,N)-DELTAU(I,J)*D(M,N)
C 120 CONTINUE
C   DO 140 K=1,4
C   DM(K)=0.
C   DO 140 N=1,4
C   DM(K)=DM(K)+BM(K,N)*W(N,I)
C 140 CONTINUE
C   DO 160 K=1,4
C 160 DQ(I,J,K)=DM(K)
C 200 CONTINUE
      RETURN
      END

C-----  

C*          SUBROUTINE COEFY(I)
C*
C*  SETTING COEFFICIENTS FOR LY-OPERATOR
C*

```

```

C*****+
      IMPLICIT REAL*8(A-H,O-Z)
      PARAMETER (IZ=150,JZ=100)
      COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
      >          P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
      COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
      >          ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
      >          ,ZMUT(IZ,JZ)
      >          ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
      COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
      >          PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF,COND
      COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
      COMMON/INTEG/IL,JL,IL1,JL1,NEND,NEEG,NADV,ITIME,ISUP,IVISC,IWALL
      DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
      EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
      >          (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****+
      DIMENSION IN(4),EE(4,4,JZ),EL(4,JZ),W(4,JZ)
      DIMENSION AM(4,4),BM(4,4),CM(4,4),DM(4)
      DIMENSION AL(4,4),BE(4)
      DIMENSION B(4,4),BL1(4,4),D(4,4),A(4,4)

C*CH01
      DIMENSION AMJL(4,4),BMJL(4,4),CMJL(4,4),DMJL(4)
      DIMENSION PINV(4,4),PPD(4,4),PRE(4,4),PINV1(4,4),PPDJL1(4,4)
      >          ,PID(4,4),PIA(4,4),PIB(4,4),DM1(4),DM2(4),DM10(4),DM20(4)
C*****+
C*
C* ON THE CENTER LINE OF THE NOZZLE AT J=1
C*
      J=1
      CALL SZERO(4,AM)
      CALL SZERO(4,BM)
      DO 20 M=1,4
      DM(M)=0.
      BM(M,M)=BM(M,M)+1.0
20    CONTINUE
      CALL SZERO(4,CM)
      CALL EEL(J,4,JL,EE,EL,AM,BM,CM,DM,IN,AL,BE)

C*
C* INTERIOR NODS
C*
      DO 80 J=2,JL1
      TAUD=0.5DO*DELTAU(I,J)*THETA/EYI
      TAUD2=2.*TAUD
      JM1=J-1
      JP1=J+1
      CALL JACOB(2,B,I,JM1)
      CALL PRECON(I,J,PRE)
      CALL DHDQ(D,I,J)
      DO 904 MM=1,4
      DO 904 NN=1,4
      PPD(MM,NN)=PRE(MM,NN)-TAUD2*D(MM,NN)
904   CONTINUE
      CALL INVER(4,PPD,PINV)
      CALL MMM(4,PINV,B,PIB)

```

```

CALL SMM(4,TAUD,PIB,AM)
CALL SZERO(4,BM)
DO 60 M=1,4
60 BM(M,M)=BM(M,M)+1.
CALL JACOB(2,B,I,JP1)
CALL MMM(4,PINV,B,PIB)
CALL SMM(4,-TAUD,PIB,CM)

C*
C* INSERT VISCOUS JACOBIAN LHS HERE
C*
IF(IVISC.EQ.1)THEN
  CALL VJACOB(A,B,D,I,J)
  CALL MMM(4,PINV,A,PIA)
  CALL MMM(4,PINV,B,PIB)
  CALL MMM(4,PINV,D,PID)
  DO 68 M=1,4
  DO 68 N=1,4
    AM(M,N)=AM(M,N)-DELTAU(I,J)*PIA(M,N)
    BM(M,N)=BM(M,N)+DELTAU(I,J)*PIB(M,N)
68 CM(M,N)=CM(M,N)-DELTAU(I,J)*PID(M,N)
ELSE
END IF
DO 70 K=1,4
70 DM(K)=DQ(I,J,K)
CALL EEL(J,4,JL,EE,EL,AM,BM,CM,DM,IN,AL,BE)
80 CONTINUE

C*
C* WALL BOUNDARY CONDITION
C*
CHOI      J=JL
CHOI      TAUD=THETA*DELTAU(I,J)/EYI
CHOI      IF(IVISC.EQ.1)GOTO 111
CHOI      CALL SZERO(4,AM)
CHOI      CALL JACOB(2,B,I,J-1)
CHOI      CALL EIGEN(2,BL1,I,J)
CHOI      DO 90 M=1,3
CHOI      DO 90 N=1,4
CHOI      DO 90 K=1,4
CHOI 90 AM(M,N)=AM(M,N)+TAUD*BL1(M,K)*B(K,N)
CHOI      CALL SZERO(4,BM)
CHOI      CALL JACOB(2,B,I,J)
CHOI      CALL DHDQ(D,I,J)
CHOI      DO 100 M=1,3
CHOI      DO 100 N=1,4
CHOI      BM(M,N)=BM(M,N)+BL1(M,N)
CHOI      DO 100 K=1,4
CHOI      BM(M,N)=BM(M,N)+TAUD*BL1(M,K)*(B(K,N)-D(K,N))
CHOI 100 CONTINUE
CHOI
CHOI      J=JL
TAUJL=DELTAU(I,JL)
TAUJM=DELTAU(I,JL1)
CALL PRECON(I,JL1,PRE)
CALL DHDQ(D,I,JL1)

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FILE: AXI2DV FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STAT

```
DO 905 MM=1,4
DO 905 NN=1,4
PPDJL1(MM,NN)=PRE(MM,NN)-TAUJM*D(MM,NN)
905 CONTINUE
CALL PRECON(I,JL,PRE)
CALL DHDQ(D,I,JL)
DO 906 MM=1,4
DO 906 NN=1,4
PPD(MM,NN)=PRE(MM,NN)-TAUJL*D(MM,NN)
906 CONTINUE
IF(.VISC.EQ.1) GOTO 111
CALL SZERO(4,AMJL)
CALL JACOB(2,B,I,J-1)
CALL EIGEN(2,BL1,I,J)
DO 1105 N=1,4
BL1(4,N)=0.DO
1105 CONTINUE
DO 1101 M=1,4
DO 1101 N=1,4
AMJL(M,N)=-TAUJL*(PPDJL1(M,N)-2.DO*TAUJM*B(M,N))
1101 CONTINUE
CALL MMM(4,BL1,AMJL,AM)
CALL SZERO(4,BMJL)
CALL JACOB(2,B,I,J)
DO 1201 M=1,4
DO 1201 N=1,4
BMJL(M,N)=TAUJM*(PPD(M,N)+2.DO*TAUJL*B(M,N))
1201 CONTINUE
CALL MMM(4,BL1,BMJL,BM)
CALL SZERO(4,CM)
DO 1501 MM=1,4
DM1(MM)=DQ(I,JL,MM)
1501 CONTINUE
DO 1502 MM=1,4
DM2(MM)=DQ(I,JL1,MM)
1502 CONTINUE
CALL MMV(4,PPD,DM1,DM10)
CALL MMV(4,PPDJL1,DM2,DM20)
DO 1300 M=1,4
DMJL(M)=TAUJM*DM10(M)+TAUJL*DM20(M)
1300 CONTINUE
CALL MMV(4,BL1,DMJL,DM)
CHOI
CHOI
BM(4,1)=-VN(I,J)
BM(4,2)=ETAX(I,J)
BM(4,3)=ETAY(I,J)
BM(4,4)=0.
CALL SZERO(4,CM)
CHOI      DO 110 M=1,3
CHOI      DM(M)=0.
CHOI      DO 110 K=1,4
CHOI      DM(M)=DM(M)+BL1(M,K)*DQ(I,J,K)
CHOI 110 CONTINUE
DM(4)=0.
```

```

      GOTO 119
111  CONTINUE
      CALL SZERO(4,AM)
      CALL SZERO(4,BM)
      CALL SZERO(4,CM)
      DO 113 M=1,4
      DM(M)=0.
113  BM(M,M)=1.0
119  CONTINUE
      CALL EEL(J,4,JL,EE,EL,AM,BM,CM,DM,IN,AL,BE)

C*
C*   SOLVE 4*4 BLOCK TRIDIAGONAL MATRICES
C*
      CALL SOLU(W,JL,4,EE,EL)
      DO 120 J=1,JL
      DO 120 K=1,4
      DQ(I,J,K)=W(K,J)
120  CONTINUE
      RETURN
      END

C-----SUBROUTINE FLUXCL
C*
C*   SUBROUTINE FOR FLUX VECTOR CALCULATION
C*
C*****IMPLICIT REAL*8(A-H,O-Z)
      IMPLICIT REAL*8(A-H,O-Z)
      PARAMETER (IZ=150,JZ=100)
      COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
>          P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
      COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
>          ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
>          ,ZMUT(IZ,JZ)
>          ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
      COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
>          PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF,COND
      COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
      COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
      DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
      EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
>          (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****ENTRY FLUX
C*
C*   COMPUTE CONVECTIVE TERMS
C*
      DO 10 I=1,IL
      DO 10 J=1,JL
      F(I,J,1)=RHO(I,J)*UN(I,J)/RJ(I,J)*Y(I,J)
      F(I,J,2)=(RHOU(I,J)*UN(I,J)+SAIX(I,J)*P(I,J))/RJ(I,J)*Y(I,J)
      F(I,J,3)=(RHOV(I,J)*UN(I,J)+SAIY(I,J)*P(I,J))/RJ(I,J)*Y(I,J)
      F(I,J,4)=(E(I,J)+P(I,J))*UN(I,J)/RJ(I,J)*Y(I,J)
      G(I,J,1)=RHO(I,J)*VN(I,J)/RJ(I,J)*Y(I,J)
      G(I,J,2)=(RHOU(I,J)*VN(I,J)+ETAX(I,J)*P(I,J))/RJ(I,J)*Y(I,J)
      G(I,J,3)=(RHOV(I,J)*VN(I,J)+ETAY(I,J)*P(I,J))/RJ(I,J)*Y(I,J)

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FILE: AXIZDV FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STA

```
G(I,J,4)=(E(I,J)+P(I,J))*VN(I,J)/RJ(I,J)*Y(I,J)
10 CONTINUE
RETURN
C* VISCOSITY FLUX VECTOR
C*
FNTRY VFLUX
DO 30 I=2,IL
DO 30 J=2,JL1
JP1=J+1
JM1=J-1
ZMUP=0.5*(ZMU(I,J)+ZMU(I,JP1))
ZMUM=0.5*(ZMU(I,J)+ZMU(I,JM1))
IF(PRNT.EQ.0.0) THEN
GAMP=0.5*(GAMMA(I,J)+GAMMA(I,JP1))
GAMM=0.5*(GAMMA(I,J)+GAMMA(I,JM1))
GKCPP=ZMUP*GAMP/PRN
GKCPM=ZMUM*GAMM/PRN
ELSE
ZMUTP = 0.5*(ZMUT(I,JP1)+ZMUT(I,J))
ZMUTM = 0.5*(ZMUT(I,JM1)+ZMUT(I,J))
ZMULP = ZMUP - ZMUTP
ZMULM = ZMUM - ZMUTM
GAMP=0.5*(GAMMA(I,J)+GAMMA(I,JP1))
GAMM=0.5*(GAMMA(I,J)+GAMMA(I,JM1))
GKCPP = GAMP*(ZMULP/PRN+ZMUTP/PRNT)
GKCPM = GAMM*(ZMULM/PRN+ZMUTM/PRNT)
ENDIF
YYP=0.5*(Y(I,J)+Y(I,JP1))
YYM=0.5*(Y(I,J)+Y(I,JM1))
YZP=YYP*ZMUP
YZM=YYM*ZMUM
AAP1=A1(I,J)*YZP
AAM1=A1(I,JM1)*YZM
AAP2=A2(I,J)*YZP
AAM2=A2(I,JM1)*YZM
AAP3=A3(I,J)*YZP
AAM3=A3(I,JM1)*YZM
AAP4=A4(I,J)*YYP*GKCPP
AAM4=A4(I,JM1)*YYM*GKCPM
UP=U(I,JP1)-U(I,J)
UM=-U(I,JM1)+U(I,J)
VP=V(I,JP1)-V(I,J)
VM=V(I,J)-V(I,JM1)
ERP=E(I,JP1)/RHO(I,JP1)-E(I,J)/RHO(I,J)
ERM=E(I,J)/RHO(I,J)-E(I,JM1)/RHO(I,JM1)
U2P=U(I,JP1)**2-U(I,J)**2
U2M=U(I,J)**2-U(I,JM1)**2
V2P=V(I,JP1)**2-V(I,J)**2
V2M=V(I,J)**2-V(I,JM1)**2
UVF=U(I,JP1)*V(I,JP1)-U(I,J)*V(I,J)
UVM=U(I,J)*V(I,J)-U(I,JM1)*V(I,JM1)
G(I,J,1)=0.
G(I,J,2)=(AAP1*UP-AAM1*UM)+(AAP2*VP-AAM2*VM)
G(I,J,3)=(AAP2*UP-AAM2*UM)+(AAP3*VP-AAM3*VM)
G(I,J,4)=(AAP4*ERP-AAM4*ERM)+0.5*((AAP1-AAP4)*U2P-
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```
>     (AAM1-AAM4)*U2M)+0.5*((AAP3-AAP4)*V2P-(AAM3-AAM4)*V2M)+  
>     (AAP2*UVP-AAM2*UVM)  
C*  
C* INSERT THE EXTRA FIRST ORDER TERMS IN CYLINDRICAL COORDINATE  
C* SYSTEMS  
C*  
EYJ=ETAY(I,J)/RJ(I,J)  
EXJ=ETAX(I,J)/RJ(I,J)  
DMUV=0.5*(ZMU(I,JP1)*V(I,JP1)-ZMU(I,JM1)*V(I,JM1))  
DDV =0.5*(V(I,JP1)-V(I,JM1))  
DMUV2=0.5*(ZMU(I,JP1)*V(I,JP1)**2-ZMU(I,JM1)*V(I,JM1)**2)  
DMUUV=0.5*(ZMU(I,JP1)*U(I,JP1)*V(I,JP1)-  
*           ZMU(I,JM1)*U(I,JM1)*V(I,JM1))  
DDU =0.5*(U(I,JP1)-U(I,JM1))  
DDMU=0.5*(ZMU(I,JP1)-ZMU(I,JM1))  
G(I,J,2)=G(I,J,2)-2./3.*EXJ*DMUV  
G(I,J,3)=G(I,J,3)+2./3.*((ZMU(I,J)*EXJ*DDU-V(I,J)*EYJ*DDMU))  
G(I,J,4)=G(I,J,4)-2./3.*((EYJ*DMUV2+EXJ*DMUUV))  
30 CONTINUE  
RETURN  
END  
C-----  
C ** RIGHT HAND SIDE CALCULATION  
C-----  
SUBROUTINE RHSCL  
C ****  
IMPLICIT REAL*8(A-H,O-Z)  
PARAMETER (IZ=150,JZ=100)  
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),  
>          P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)  
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)  
>          ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)  
>          ,ZMUT(IZ,JZ)  
>          ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)  
COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,  
>          PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF,COND  
COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS  
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL  
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)  
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),  
>          (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))  
C****  
ENTRY RHS  
CALL FLUX  
EXII=2.*EXI  
EYII=EYI*2.  
DO 10 I=1,IL  
DO 10 J=1,JL  
DO 10 K=1,4  
10 DQ(I,J,K)=0.  
    I=1  
    DO 30 J=1,JL  
    DO 20 K=1,4  
C 20 DQ(I,J,K)=DQ(I,J,K)+(-3.*F(I,J,K)+4.*F(I+1,J,K)-  
C      >          F(I+2,J,K))/EXII
```

```

20 DQ(I,J,K)=DQ(I,J,K)+(F(I+1,J,K)-F(I,J,K))/EXI
  IF(J.EQ.1.OR.J.EQ.JL) GO TO 30
  DO 25 K=1,4
25 DQ(I,J,K)=DQ(I,J,K)+(G(I,J+1,K)-G(I,J-1,K))/EYII
30 CONTINUE
J=1
DO 50 I=1,IL
DO 40 K=1,4
C 40 DQ(I,J,K)=DQ(I,J,K)+(-3.*G(I,J,K)+4.*G(I,J+1,K)-
C      G(I,J+2,K))/EYII
40 DQ(I,J,K)=DQ(I,J,K)+(G(I,J+1,K)-G(I,J,K))/EYI
  IF(I.EQ.1.OR.I.EQ.IL) GO TO 50
  DO 45 K=1,4
45 DQ(I,J,K)=DQ(I,J,K)+(F(I+1,J,K)-F(I-1,J,K))/EXII
50 CONTINUE
I=IL
DO 70 J=1,JL
DO 60 K=1,4
C 60 DQ(I,J,K)=DQ(I,J,K)+(F(I-2,J,K)-4.*F(I-1,J,K)-
C      3.*F(I,J,K))/EXII
60 DQ(I,J,K)=DQ(I,J,K)+(F(I,J,K)-F(I-1,J,K))/EXI
  IF(J.EQ.1.OR.J.EQ.JL) GO TO 70
  DO 65 K=1,4
65 DQ(I,J,K)=DQ(I,J,K)+(G(I,J+1,K)-G(I,J-1,K))/EYII
70 CONTINUE
J=JL
DO 90 I=1,IL
DO 80 K=1,4
CHK1
80 DQ(I,J,K)=DQ(I,J,K)+(G(I,J-2,K)-4.*G(I,J-1,K)-
  3.*G(I,J,K))/EYII
CHK1 80 DQ(I,J,K)=DQ(I,J,K)+(G(I,J,K)-G(I,J-1,K))/EYI
  IF(I.EQ.1.OR.I.EQ.IL) GO TO 90
  DO 85 K=1,4
85 DQ(I,J,K)=DQ(I,J,K)+(F(I+1,J,K)-F(I-1,J,K))/EXII
90 CONTINUE
DO 100 I=2,IL1
DO 100 J=2,JL1
  IP1=I+1
  IM1=I-1
  JP1=J+1
  JM1=J-1
  DO 100 K=1,4
  DQ(I,J,K)=DQ(I,J,K)+(F(IP1,J,K)-F(IM1,J,K))/EXII+
    (G(I,JP1,K)-G(I,JM1,K))/EYII
100 CONTINUE
DO 200 I=1,IL
DO 200 J=2,JL
  DQ(I,J,3)=DQ(I,J,3)-P(I,J)/RJ(I,J)
200 CONTINUE
  RETURN
C* VISCOSUS RIGHT HAND SIDE
C*
  ENTRY VRHS
  CALL VFLUX

```

```

DO 300 I=2,IL
DO 300 J=2,JL1
DQ(I,J,3)=DQ(I,J,3)+4./3.*ZMU(I,J)*V(I,J)/(RJ(I,J)*Y(I,J))
DO 300 K=2,4
300 DQ(I,J,K)=DQ(I,J,K)-G(I,J,K)
RETURN
END
C ****
C SERVICE SUBROUTINE
C ****
      SUBROUTINE SUPPLY
      IMPLICIT REAL*8(A-H,O-Z)
      PARAMETER (IZ=150,JZ=100)
      COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
>           P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
      COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
>           ,RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
>           ,ZMUT(IZ,JZ)
>           ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
      COMMON/CONST/AIN,ATH,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
>           PRNT,PB,RM1,SUM(4),ZMVO,REN,PRN,TWALL,TREF,COND
      COMMON/CONST1/CP(IZ,JZ),CV(IZ,JZ),GAMMA(IZ,JZ),GM1(IZ,JZ),RGAS
      COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,ISUP,IVISC,IWALL
      DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
      EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
>           (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C ****
      DIMENSION SS(4),SS1(4),SS2(4)
      ENTRY CHECK
      DO 10 K=1,4
      SS1(K)=0.D0
10    SS2(K)=0.D0
      IF(IVISC.EQ.1)THEN
      JEND=JL1
      ELSE
      JEND=JL
      ENDIF
      IF(ISUP.EQ.3)THEN
      IBEG=2
      ELSE
      IBEG=1
      ENDIF
      DO 20 I=IBEG,IL
      DO 20 J=2,JEND
      DO 20 K=1,4
      QQ=Q(I,J,K)
C     IF(QQ.EQ.0.D0)GO TO 20
      SS1(K)=SS1(K)+(DQ(I,J,K)*RJ(I,J)/Y(I,J))**2
      SS2(K)=SS2(K)+QQ**2
20    CONTINUE
      DO 30 K=1,4
30    SS(K)=DSQRT(SS1(K)/SS2(K))
      WRITE(19,500)NADV,(SS(K),K=1,4)
500    FORMAT(I5,3X,4(1X,E14.7))
      RETURN

```

```

E/ UPT MASS
F1=MARCOS(-1.D0)
DO 80 I=1,IL
E RT=0.
DO 75 J=1,JL1
DLR=DSQRT((X(I,J+1)-X(I,J))**2+(Y(I,J+1)-Y(I,J))**2)
CXY=DSQRT(SAIX(I,J)**2+SAIY(I,J)**2)
CXCY1=DSQRT(SAIX(I,J+1)**2+SAIY(I,J+1)**2)
FLRT=FLRT+0.5*PPI*(Y(I,J+1)+Y(I,J))*DELR
      *(RHO(I,J+1)*UN(I,J+1)/CXCY1+RHO(I,J)*UN(I,J)/CXCY)
75 CONTINUE
WRITE(22,789)I,FLRT
80 CONTINUE
789 E0FMAT(1X,I8,E14.7)
RETURN
ENTRY OUTPUT
WRITE(22,550)NADV
550 E0FMAT(//10(1H*)/' NADV=' ,I5//)
DO 50 I=1,IL
DO 50 J=1,JL
S1=(E(I,J)/RHO(I,J)-GM1(I,J)*0.5/GAMMA(I,J)*(U(I,J)**2+
      V(I,J)**2))/CV(I,J)
L1=(E(I,J)/RHO(I,J)-0.5*(U(I,J)**2+V(I,J)**2))/CV(I,J)
I1A=DSQRT((U(I,J)*U(I,J)+V(I,J)*V(I,J))/GAMMA(I,J)
      *RHO(I,J)/P(I,J))
S2=E(I,J)*(ST/TT)**(GAMMA(I,J)/GM1(I,J))
WRITE(18,607)X(I,J),Y(I,J),P(I,J),RMA,TT,SP
WRITE(66) (Q(I,J,K),K=1,4),DELTAU(I,J)
607 E0FMAT(6(1X,E14.7))
C WRITE(6,600)I,J,RHO(I,J),U(I,J),V(I,J),E(I,J),ST
C WRITE(6,650)P(I,J),UN(I,J),VN(I,J),SP,TT
600 E0FMAT(1X,'#',I2,',',I2,3X,5(1X,E10.3))
650 E0FMAT(10X,5(1X,E10.3))
50 CONTINUE
C
C WRITE THE LAST TWO LINES
C
DO 55 I=116,117
DO 55 J=1,JL
55 WRITE(68) (Q(I,J,K),K=1,4)
C
RETURN
END
C ****
C*
C* LIBRARY SUBROUTINES
C*
SUBROUTINE EEL(J,MM,JMAX,E,EL,AM,BM,CM,DM,IN,AL,BE)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION IN(MM),E(MM,MM,JMAX),EL(MM,JMAX)
DIMENSION AM(MM,MM),BM(MM,MM),CM(MM,MM),DM(MM)
DIMENSION AL(MM,MM),BE(MM)
DO 30 M=1,MM
TP=0.ODO
DO 20 N=1,MM

```

```

T1=0.0D0
IF(J.EQ.1)GO TO 10
TP=TP+AM(M,N)*EL(N,J-1)
DO 5 K=1,MM
5 T1=T1+AM(M,K)*E(K,N,J-1)
10 CONTINUE
AL(M,N)=BM(M,N)-T1
20 CONTINUE
EL(M,J)=DM(M)+TP
30 CONTINUE
DO 50 M=1,MM
DO 40 N=1,MM
40 E(M,N,J)=CM(M,N)
50 CONTINUE
CALL AXB(MM,MM,AL,E(1,1,J),BE,0,IN)
CALL AXB(MM,1,AL,EL(1,J),BE,1,IN)
RETURN
END

```

C-----

```

SUBROUTINE SOLU(W,JMAX,MM,E,EL)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION W(MM,JMAX),E(MM,MM,JMAX),EL(MM,JMAX)
DO 40 M=1,MM
W(M,JMAX)=EL(M,JMAX)
40 CONTINUE
DO 50 J1=2,JMAX
J=JMAX+1-J1
DO 46 M=1,MM
SUM=0.0D0
DO 44 K=1,MM
SUM=SUM+E(M,K,J)*W(K,J+1)
44 CONTINUE
W(M,J)=SUM+EL(M,J)
46 CONTINUE
50 CONTINUE
RETURN
END

```

C-----

```

SUBROUTINE AXB(N,M,A,B,X,INIT,IPS)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION A(N,N),B(N,M),IPS(N),X(N)
IF(INIT.EQ.0)CALL DECOMP(N,A,IPS)
DO 10 I=1,M
CALL SOLV(N,A,B(1,I),X,IPS)
10 CONTINUE
RETURN
END

```

C-----

```

SUBROUTINE DECOMP(N,UL,IPS)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION UL(N,N),IPS(N)
DO 5 I=1,N
IPS(I)=I
5 CONTINUE
NM1=N-1

```

FILE: A1 FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STATE

```
      K=1,NM1
      DO 10 ODO
      L=1,I=K,N
      T=1,T5(I)
      CALL DABS(UL(IP,K))
      SIZE=BIG)11,11,10
10  L=G-SIZE
      KPIV=I
11  CONTINUE
      (IP,IDXPIV-K)14,15,14
14  I=1,IPS(K)
      IPS(K)=IPS(IDXPIV)
      IPS(IDXPIV)=J
15  IP=IPS(K)
      IP=UL(KP,K)
      IP=IP+1
      I=1,N,I=KP1,N
      X=IPS(I)
      EM=UL(IP,K)/PIVOT
      EM=EM,K)==-EM
      I=1,N,J=KP1,N
      UL(IP,J)=UL(IP,J)+EM*UL(KP,J)
16  CONTINUE
17  CONTINUE
      RETURN
      END
```

C-----

```
SUBROUTINE SOLV(N,UL,B,X,IPS)
      REAL*8 (A-H,O-Z)
      DIMENSION UL(N,N),B(N),X(N),IPS(N)
      N=1=N+1
      IP=IPS(1)
      I=1,I=B(IP)
      I=2,I=2,N
      IP=IPS(I)
      IM1=I+1
      SUM=0.ODO
      DO 1 J=1,IM1
1     SUM=SUM+UL(IP,J)*X(J)
2     X(I)=B(IP)-SUM
      IP=IPS(N)
      B(N)=X(N)/UL(IP,N)
      DO 4 IBACK=2,N
      I=NP1-IBACK
      IP=IPS(I)
      IP=I+1
      SUM=0.ODO
      DO 3 J=IP1,N
3     SUM=SUM+UL(IP,J)*B(J)
4     B(I)=(X(I)-SUM)/UL(IP,I)
      RETURN
      END
```

C-----

```
C      SET ZERO FOR MATRIX (M,M)
      SUBROUTINE SZERO(M,A)
```

```

IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(M,M)
DO 10 I=1,M
DO 10 J=1,M
A(I,J)=0.0D0
10 CONTINUE
RETURN
END

```

C-----

```

C SCALAR*METRIC (M,M)
SUBROUTINE SMM(M,C,A,B)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(M,M),B(M,M)
DO 10 I=1,M
DO 10 J=1,M
B(I,J)=C*A(I,J)
10 CONTINUE
RETURN
END

```

C-----

```

C METRIX*METRIX (M*M)
SUBROUTINE MMM(M,A,B,C)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(M,M),B(M,M),C(M,M)
DO 10 I=1,M
DO 10 J=1,M
C(I,J)=0.0D0
DO 10 K=1,M
C(I,J)=C(I,J)+A(I,K)*B(K,J)
10 CONTINUE
RETURN
END

```

C*

```

SUBROUTINE SYH(IL,IU,BB,DD,AA,CC)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION AA(1),BB(1),CC(1),DD(1)

```

C....

C.... SUBROUTINE SYH SOLVES TRIDIAGONAL SYSTEM BY ELIMINATION

C.... IL = SUBSCRIPT OF FIRST EQUATION

C.... IU = SUBSCRIPT OF LAST EQUATION

C.... BB = COEFFICIENT BEHIND DIAGONAL

C.... DD = COEFFICIENT ON DIAGONAL

C.... AA = COEFFICIENT AHEAD OF DIAGONAL

C.... CC = ELEMENT OF CONSTANT VECTOR

C....

C.... ESTABLISH UPPER TRIANGULAR MATRIX

C....

```

LP = IL+1
DO 10 I = LP,IU
R = BB(I)/DD(I-1)
DD(I) = DD(I)-R*AA(I-1)
10 CC(I) = CC(I)-R*CC(I-1)

```

C...

C... BACK SUBSTITUTION

C...

FILE: AXI2DV FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STAT

```
CC(IU) = CC(IU)/DD(IU)
DO 20 I =LP,IU
J = IU-I+IL
20 CC(J) = (CC(J)-AA(J)*CC(J+1))/DD(J)
C...
C... SOLUTION STORED IN CC
C...
      RETURN
      END
C*****SUBROUTINE INVER(M,A,AINV)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(4,4),B(4,4),AINV(4,4),COF(4,4)
A11=A(1,1)
A12=A(1,2)
A13=A(1,3)
A14=A(1,4)
A21=A(2,1)
A22=A(2,2)
A23=A(2,3)
A24=A(2,4)
A31=A(3,1)
A32=A(3,2)
A33=A(3,3)
A34=A(3,4)
A41=A(4,1)
A42=A(4,2)
A43=A(4,3)
A44=A(4,4)
DET=A11*(A22*A33*A44+A23*A34*A42+A24*A43*A32-A24*A33*A42
> -A23*A32*A44-A22*A43*A34)-
>     A12*(A21*A33*A44+A23*A34*A41+A24*A43*A31-A24*A33*A41
> -A23*A31*A44-A21*A43*A34)+
>     A13*(A21*A32*A44+A22*A34*A41+A24*A42*A31-A24*A32*A41
> -A22*A31*A44-A21*A42*A34)-
>     A14*(A21*A32*A43+A22*A33*A41+A23*A42*A31-A23*A32*A41
> -A22*A31*A43-A21*A42*A33)
COF(1,1)=A22*A33*A44+A23*A34*A42+A24*A43*A32-A24*A33*A42
> -A23*A32*A44-A22*A43*A34
COF(1,2)=-(A21*A33*A44+A23*A34*A41+A24*A43*A31-A24*A33*A41
> -A23*A31*A44-A21*A43*A34)
COF(1,3)=A21*A32*A44+A22*A34*A41+A24*A42*A31-A24*A32*A41
> -A22*A31*A44-A21*A42*A34
COF(1,4)=-(A21*A32*A43+A22*A33*A41+A23*A42*A31-A23*A32*A41
> -A22*A31*A43-A21*A42*A33)
COF(2,1)=-(A12*A33*A44+A13*A34*A42+A14*A32*A43-A14*A33*A42
> -A13*A32*A44-A12*A43*A34)
COF(2,2)=A11*A33*A44+A13*A34*A41+A14*A31*A43-A14*A33*A41
> -A13*A31*A44-A11*A43*A34
COF(2,3)=-(A11*A32*A44+A12*A34*A41+A14*A31*A42-A14*A32*A41
> -A12*A31*A44-A11*A42*A34)
COF(2,4)=A11*A32*A43+A12*A33*A41+A13*A31*A42-A13*A32*A41
> -A12*A31*A43-A11*A42*A33
COF(3,1)=A12*A23*A44+A13*A24*A42+A14*A22*A43-A14*A23*A42
> -A13*A22*A44-A12*A43*A24
```

```

COF(3,2)=-(A11*A23*A44+A13*A24*A41+A14*A21*A43-A14*A23*A41
> -A13*A21*A44-A11*A43*A24)
COF(3,3)=A11*A22*A44+A12*A24*A41+A14*A21*A42-A14*A22*A41
> -A12*A21*A44-A11*A42*A24
COF(3,4)=-(A11*A22*A43+A12*A23*A41+A13*A21*A42-A13*A22*A41
> -A12*A21*A43-A11*A42*A23)
COF(4,1)=-(A12*A23*A34+A13*A24*A32+A14*A22*A33-A14*A23*A32
> -A13*A22*A34-A12*A33*A24)
COF(4,2)=A11*A23*A34+A13*A24*A31+A14*A21*A33-A14*A23*A31
> -A13*A21*A34-A11*A33*A24
COF(4,3)=-(A11*A22*A34+A12*A24*A31+A14*A21*A32-A14*A22*A31
> -A12*A21*A34-A11*A32*A24)
COF(4,4)=A11*A22*A33+A12*A23*A31+A13*A21*A32-A13*A22*A31
> -A12*A21*A33-A11*A32*A23
AINV(1,1)=COF(1,1)/DET
AINV(1,2)=COF(2,1)/DET
AINV(1,3)=COF(3,1)/DET
AINV(1,4)=COF(4,1)/DET
AINV(2,1)=COF(1,2)/DET
AINV(2,2)=COF(2,2)/DET
AINV(2,3)=COF(3,2)/DET
AINV(2,4)=COF(4,2)/DET
AINV(3,1)=COF(1,3)/DET
AINV(3,2)=COF(2,3)/DET
AINV(3,3)=COF(3,3)/DET
AINV(3,4)=COF(4,3)/DET
AINV(4,1)=COF(1,4)/DET
AINV(4,2)=COF(2,4)/DET
AINV(4,3)=COF(3,4)/DET
AINV(4,4)=COF(4,4)/DET
C CALL MMM(4,A,AINV,B)
C DO 1 MM=1,4
C WRITE(5,10) (B(MM,NN),NN=1,4)
C 1 CONTINUE
10 FORMAT(4D16.7)
RETURN
END
*****
SUBROUTINE MMV(M,A,B,C)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(M,M),B(M),C(M)
DO 10 I=1,M
C(I)=0.D0
DO 10 K=1,M
C(I)=C(I)+A(I,K)*B(K)
10 CONTINUE
RETURN
END
*****
SUBROUTINE CPGAM(CP,CV,GAMMA,GM1,R,I,J,
> RHO,RHOU,RHOV,E,TCP)
*****
PARAMETER(IZ=150,JZ=100)
IMPLICIT REAL*8 (A-H,O-Z)
COMMON/CPCOFF/ CPA1,CPA2,CPA3,CPA4,CPA5,CPA6,CPA7

```

FILE: AXI2DV FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STAT

```
> ,CPA8,CPA9,CPA10,ENE(101)
C=====
    IF(TCP.NE.0.0) GOTO 20
    UU=RHOU/RHO
    VV=RHOV/RHO
    EE=E/RHO-0.5*(UU**2+VV**2)
    TT=300.0
    IF(EE.LE.ENE(1)) GO TO 20
    DO 10 MM=1,101
        EA= EE - ENE(MM)
        EB= EE - ENE(MM+1)
        ESIGN= EA*EB
        IF(ESIGN.LE.0.DO)THEN
            T1=300.0+27.611*DFLOAT(MM-1)
            T2=300.0+27.611*DFLOAT(MM)
            TT=(T2*EA-T1*EB)/(EA-EB)
            GO TO 20
        ELSE
        END IF
10    CONTINUE
    TT=3061.1DO
20    CONTINUE
    IF(TCP.NE.0.0) TT=TCP
C*
    IF(TT.LE.1000.0)THEN
        CP=(CPA6+CPA7*TT+CPA8*TT**2+CPA9*TT**3+CPA10*TT**4)
        CV=CP-R
    ELSE
        CP=(CPA1+CPA2*TT+CPA3*TT**2+CPA4*TT**3+CPA5*TT**4)
        CV=CP-R
    END IF
    GAMMA=CP/CV
    GM1=GAMMA-1.0
    RETURN
    END
C*****
SUBROUTINE CPCOEF
C*****
IMPLICIT REAL*8 (A-H,O-Z)
COMMON/CPCOFF/ CPA1,CPA2,CPA3,CPA4,CPA5,CPA6,CPA7
> ,CPA8,CPA9,CPA10,ENE(101)
DIMENSION Y(10),A1(10),A2(10),A3(10),A4(10),A5(10)
> ,A6(10),A7(10),A8(10),A9(10),A10(10),WM(10)
DATA RU,WMMIX/8314.3,20.405/
C=====
C CO
    WM(1)=28.010
    Y(1)= 0.13108
C CO2
    WM(2)=44.0
    Y(2)= 0.03636
C H
    WM(3)=1.0
    Y(3)= 0.02387
C H2
```

WM(4)=2.0
Y(4)= 0.15802
C H2O
WM(5)=18.0
Y(5)= 0.32366
C NO
WM(6)=30.0
Y(6)= 0.00260
C N2
WM(7)=28.0
Y(7)= 0.30407
C O
WM(8)=16.0
Y(8)= 0.00158
C OH
WM(9)=17.0
Y(9)= 0.01744
C O2
WM(10)=32.0
Y(10)= 0.00129
C-----CO
A1(1)= 0.29840696E+01
A2(1)= 0.14891390E-02
A3(1)=-0.57899684E-06
A4(1)= 0.10364577E-09
A5(1)=-0.69353550E-14
C
A6(1)= 0.37100928E+01
A7(1)=-0.16190964E-02
A8(1)= 0.36923594E-05
A9(1)=-0.20319674E-08
A10(1)= 0.23953344E-12
C-----CO2
A1(2)= 0.44608041E+01
A2(2)= 0.30981719E-02
A3(2)=-0.12392571E-05
A4(2)= 0.22741325E-09
A5(2)=-0.15525954E-13
C
A6(2)= 0.24007797E+01
A7(2)= 0.87350957E-02
A8(2)=-0.66070878E-05
A9(2)= 0.20021861E-08
A10(2)= 0.63274039E-15
C-----H
A1(3)= 0.25000000E+01
A2(3)= 0.00000000
A3(3)= 0.00000000
A4(3)= 0.00000000
A5(3)= 0.00000000
C
A6(3)= 0.25000000E+01
A7(3)= 0.00000000
A8(3)= 0.00000000
A9(3)= 0.00000000

FILE: AXI2DV FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STA

A10(3)= 0.00000000

C-----H2

A1(4)= 0.30558123E+01

A2(4)= 0.59740400E-03

A3(4)=-0.16747471E-08

A4(4)=-0.21247544E-10

A5(4)= 0.25195487E-14

C

A6(4)= 0.29432327E+01

A7(4)= 0.34815509E-02

A8(4)=-0.77713819E-05

A9(4)= 0.74997496E-08

A10(4)=-0.25203379E-11

C-----H2O

A1(5)= 0.26340654E+01

A2(5)= 0.31121899E-02

A3(5)=-0.90278449E-06

A4(5)= 0.12673054E-09

A5(5)=-0.69164732E-14

C

A6(5)= 0.41675564E+01

A7(5)=-0.18106868E-02

A8(5)= 0.59450878E-05

A9(5)=-0.48670871E-08

A10(5)= 0.15284144E-11

C-----NO

A1(6)= 0.31486543E+01

A2(6)= 0.14151823E-02

A3(6)=-0.57574881E-06

A4(6)= 0.10738529E-09

A5(6)=-0.73900199E-14

C

A6(6)= 0.42484931E+01

A7(6)=-0.48661106E-02

A8(6)= 0.11634155E-04

A9(6)=-0.99768494E-08

A10(6)= 0.30483948E-11

C-----N2

A1(7)= 0.28536374E+01

A2(7)= 0.16014368E-02

A3(7)=-0.62888336E-06

A4(7)= 0.11428932E-09

A5(7)=-0.77953822E-14

C

A6(7)= 0.37034288E+01

A7(7)=-0.14179405E-02

A8(7)= 0.28625094E-05

A9(7)=-0.12018374E-08

A10(7)=-0.13475522E-13

C-----O

A1(8)= 0.25342961E+01

A2(8)=-0.12478170E-04

A3(8)=-0.12562724E-07

A4(8)= 0.69029862E-11

A5(8)=-0.63797095E-15

C

A6(8)= 0.30309401E+01
 A7(8)=-0.22525853E-02
 A8(8)= 0.39824540E-05
 A9(8)=-0.32604921E-08
 A10(8)= 0.10152035E-11

C-----OH

A1(9)= 0.28897814E+01
 A2(9)= 0.10005879E-02
 A3(9)=-0.22048807E-06
 A4(9)= 0.20191288E-10
 A5(9)=-0.39409831E-15

C

A6(9)= 0.38737300E+01
 A7(9)=-0.13393772E-02
 A8(9)= 0.16348351E-05
 A9(9)=-0.52133639E-09
 A10(9)= 0.41826974E-13

C-----O2

A1(10)= 0.36122139E+01
 A2(10)= 0.74853166E-03
 A3(10)=-0.19820647E-06
 A4(10)= 0.33749008E-10
 A5(10)=-0.23907374E-14

C

A6(10)= 0.37837135E+01
 A7(10)=-0.30233634E-02
 A8(10)= 0.99492751E-05
 A9(10)=-0.98189101E-08
 A10(10)= 0.33031825E-11

C=====

CPA1=0.DO
 CPA2=0.DO
 CPA3=0.DO
 CPA4=0.DO
 CPA5=0.DO
 CPA6=0.DO
 CPA7=0.DO
 CPA8=0.DO
 CPA9=0.DO
 CPA10=0.DO
 DO 10 J=1,10
 CPA1=CPA1+Y(J)*A1(J)*RU/WMMIX
 CPA2=CPA2+Y(J)*A2(J)*RU/WMMIX
 CPA3=CPA3+Y(J)*A3(J)*RU/WMMIX
 CPA4=CPA4+Y(J)*A4(J)*RU/WMMIX
 CPA5=CPA5+Y(J)*A5(J)*RU/WMMIX
 CPA6=CPA6+Y(J)*A6(J)*RU/WMMIX
 CPA7=CPA7+Y(J)*A7(J)*RU/WMMIX
 CPA8=CPA8+Y(J)*A8(J)*RU/WMMIX
 CPA9=CPA9+Y(J)*A9(J)*RU/WMMIX
 CPA10=CPA10+Y(J)*A10(J)*RU/WMMIX

10 CONTINUE

C...

R=RU/WMMIX

FILE: AXI2IN FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STAT

```
DO 20 MM=1,101
TT=300.0+27.611*DFLOAT(MM-1)
IF(TT.LE.1000.0)THEN
  CP=(CPA6+CPA7*TT+CPA8*TT**2+CPA9*TT**3+CPA10*TT**4)
  CV=CP-R
  ENE(MM)=CV*TT
ELSE
  CP=(CPA1+CPA2*TT+CPA3*TT**2+CPA4*TT**3+CPA5*TT**4)
  CV=CP-R
  ENE(MM)=CV*TT
END IF
20  CONTINUE
RETURN
END
//DATA.INPUT DD *
&INPUT IL=125,JL=80,NBEG=1,NEND=30,NITER=30,P0=1.D+06,T0=3061.1D0,
      CFL=5.0, OMEGAX=0.25, OMEGAY=0.25, RM1=0.04, RM2=1.2, ISUP=1,
      AIN=1.0, ATH=0.8, RL=1.3, THETA=1.0,CPO=7152.4853,GAMMA0=1.17,
      ITIME=1,IREAD=1,FST=0.00,TWALL=3512.07,FSTY=0.9,PB=0.,
      IVISC=1,IWALL=0,PRN=0.7,REN=1.D5,TREF=3000.,ZMU0=0.D0,
      PRNT=0.7D0, COND=0.0,
&END
//DATA.FT38FO01 DD DSN=STU.I19500.MYH100.HERMES.CONV.H125M80.VIS,
//  DISP=(OLD,KEEP),VOL=REF=STU.I19500.MYH100.LIB,
//  DCB=(RECFM=VBS,LRECL=80,BLKSIZE=3120),
//  SPACE=(TRK,(9,5),RLSE)
//DATA.FT66FO01 DD DSN=STU.I19500.MYH100.HERMES.CONV.RERUN.VIS,
//  DISP=(NEW,KEEP),VOL=REF=STU.I19500.MYH100.LIB,
//  DCB=(RECFM=VBS,LRECL=80,BLKSIZE=3120),
//  SPACE=(TRK,(9,5),RLSE)
//DATA.FT19FO01 DD DSN=STU.I19500.MYH100.HERMES.CONV.DQ.VIS,
//  DISP=(NEW,KEEP),VOL=REF=STU.I19500.MYH100.LIB,
//  DCB=(RECFM=FB,LRECL=80,BLKSIZE=3120),
//  SPACE=(TRK,(9,5),RLSE)
//DATA.FT18FO01 DD DSN=STU.I19500.MYH100.HERMES.CONV.SOLU.VIS,
//  DISP=(NEW,KEEP),VOL=REF=STU.I19500.MYH100.LIB,
//  DCB=(RECFM=FB,LRECL=130,BLKSIZE=3120),
//  SPACE=(TRK,(9,5),RLSE)
//DATA.FT22FO01 DD DSN=STU.I19500.MYH100.HERMES.CONV.MASS.VIS,
//  DISP=(NEW,KEEP),VOL=REF=STU.I19500.MYH100.LIB,
//  DCB=(RECFM=FB,LRECL=130,BLKSIZE=3120),
//  SPACE=(TRK,(9,5),RLSE)
//DATA.FT68FO01 DD DSN=STU.I19500.MYH100.HERMES.CONV.LINE.VIS,
//  DISP=(NEW,KEEP),VOL=REF=STU.I19500.MYH100.LIB,
//  DCB=(RECFM=VBS,LRECL=80,BLKSIZE=3120),
//  SPACE=(TRK,(9,5),RLSE)
// EXEC PROMPTME
```

VENKATESWARAN SANKA (V19)

PNSVIS FOR

X14140

USERID: V19 ORIGIN: PSUVM CREATED: 06/20/89 15:42:50
FILENAME: PNSVIS FOR CLASS: A FORMAT:J
SPOOLID: PS21 RECS: 3011 COPY: 1 DUPLICATE: 1
PRINTED AT: PSUVM ID: \$PPCBP01 AT: 06/20/89 15:42:54

*

* THIS FILE WAS SENT BY THE COMMAND:
* PRT3812 PNSVIS FOR A1 (PPCB1 COPIES 1 ORIENT N FONT 11
*

*

VENKATESWARAN SANKA (V19)

PNSVIS FOR

FILE: PNSVIS FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STA

```
//STIXXXXX JOB
/*JP T=500, L=10000
// EXEC PGM=IEFBR14
//*
//D DD VOL=REF=STU.I19500.MYH100.LIB,DISP=(OLD,DELETE),
//      DSN=STU.I19500.MYH100.HERMES2.DIF.SOLU.VIS
// EXEC FVCG,PARM.SOURCE='OPT(3)'
//* EXEC FWCG
//SYSIN DD *
C   THIS VERSION USES TRUE JACOBIAN
C*****
C*      PROGRAM NAME: NOZZLE
C*      AXISYMMETRIC SUPERSONIC NOZZLE FLOW
C*      IN GENERAL COORDINATE SYSTEM
C*      USING TIME ITERATIVE UW/CD DDADI METHOD
C*      WITH THIN-LAYER APPROXIMATED NAVIER-STOKES EQ.
C*****
C*
C*  MAIN PROGRAM
C*
C*****
IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=80)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
>          P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
>          ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
>          ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
>CFL1,PRNT,PB,RM1,SUM(4),ZMU0,REN,PRN,TWALL,TREF
>,BIOT,TW1
COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
>          ,IWBC,IFLOW
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
>          (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****
CALL INITIA
DO 10 NADV=NBEG,NEND
CALL SOLVE
CALL CHECK
10 CONTINUE
CALL MASS
CALL OUTPUT
STOP
END
C*
C*  SET UP INITIAL CONDITION
C*
SUBROUTINE INITIA
C*****
IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=80)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
```

FILE: PNSVIS FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STA

```
>          P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
> ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
> ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
>CFL1,PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF
>,BIOT,TW1
COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
> ,IWBC,IFLOW
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****  
C*
C*      IF THE DIMENSION IN COMMON BLOCK MUST BE CHANGED
C*      PLEASE CHANGE THE PARAMETER STATEMENT
C*
DIMENSION SS(3500,4)
NAMELIST/INPUT/IL,JL,NEND,PO,TO,CFL,OMEGAX,OMEGAY,RM1,AIN,FST,
> NITER,AEX,RL,THETA,CPO,GAMMAO,NBEG,ITIME,IVISC,NORD,IWALL,RM2
> ,IREAD,PRN,REN,TREF,ZMUO,TWALL,FSTY,PB,PRNT,CFL1,IWBC,BIOT,TW1
> ,IFLOW
CALL ERRSET(208,256,-1,0,0,0)
C... IL=TOTAL GRID NUMBER IN XI DIRECTION
C... JL=TOTAL GRID NUMBER IN ETA DIRECTION
C... NBEG= COUNTING INDEX OF ITERATION STEP
C      =1 FOR THE FIRST RUN
C      =ANY NUMBER EXCEPT 1 FOR RERUN
C... NEND= NUMBER OF ITERATIONS FOR THE FIRST RUN ONLY
C... NITER=NUMBER IF ITERATIONS TO BE RUN WHEN RERUN(NBEG.NE.1)
C... PO = STAGNATION PRESSURE
C... PB=THE BACK PRESSURE AT THE EXIT OF NOZZLE
C      =0. (SUBSONIC FLOW EXTRAPOLATED FROM INTERIOR)
C      = THE SPECIFIED BACK PRESSURE (FIXED THE PRESSURE FOR
C      SUBSONIC PORTION AT EXIT)
C... TG = STAGNATION TEMPERATURE
C... CFL = CFL NUMBER
C... CFL1= CFL NUMBER FOR PNS MARCHING
C... OMEGAX=ARTIFICIAL DISSIPATION CONSTANT IN XI DIRECTION
C... OMEGAY=ARTIFICIAL DISSIPATION CONSTANT INETA DIRECTION
C... IREAD = 0 FOR DEFAULT CONICAL NOZZLE
C      1 READ GRID FROM DATA FILE
C... RM1 =THE INITIAL GUESS FOR INLET MACH NUMBER
C... RM2 =THE INITIAL GUESS FOR EXIT MACH NUMBER
C... AIN =THE INLET RADIUS FOR CONICAL NOZZLE (IGNORED IN IREAD=1)
C... AEX =THE EXIT RADIUS FOR CONICAL NOZZLE (IGNORED IF IREAD=1)
C... RL =TOTAL LENGTH OF CONICAL NOZZLE (IGNORED IF OREAD=1)
C... ITIME= 0 FOR CONSTANT DT    1 FOR CONSTANT CFL
C... IVISC= 0 INVISCID FLOW
C      1 VISCOUS FLOW
C... NORD = 0 FOR FIRST ORDER UPWIND IN XI
C      1 FOR SECOND ORDER UPWIND IN XI
C... FST = STRETCHING FACTOR IN XI DIRECTIO (0 FOR UNIFORM GRID)
C... FSTY= STRETCHING FACTOR IN ETA DIRECTION (0 FOR UNIFORM GRID)
```

C* SPECIFIC HEAT
C* THERMAL NUMBER
C* IFLW=1 FOR FLOW
C* IFLW=-1 FOR REVERSE FLOW

C* (IF IFLW=1, TURN OFF IN THIS SUBROUTINE)

C* IFLW=1
C* IWALL TEMPERATURE
C* TREF
C* ZMHIC = THE VISCOSITY OF COOLING LIQUID
C* TREF = THE INLET (M. CP/2 PI K YIN)
C* IFLW=1 FOR FLOW FROM INLET TO EXIT
C* IFLW=-1 FOR FLOW FROM EXIT TO INLET

C* (IF IFLW=1, ONLY VALID FOR IFLW=-1)

C... TWA = THE AVERAGE WALL TEMPERATURE FOR IWALL=1

C... TREF = THE REFERENCE TEMPERATURE FOR VISCOSITY CALCULATION

C... ZMHIC = THE VISCOSITY AT T=TREF

C... IWFB = 0 FOR EXPLICIT WALL B. C.
C... IWFB = 1 FOR IMPLICIT WALL B. C.

C ** READ INPUT DATA
 REAL(S,INPUT)
 WRITE(18,INPUT)

C ** SET UP GEOMETRY
 IL1=IL-1
 JL1=JL-1

C
 CALL CRASH

C
 PI=3.141592653589793D0

C TURN ON REVERSE COOLING FLOW
 IF(NBEG.EQ.1) IFLW=1

C
 DO 10 I=1,IL
 AREA(I)=AIN+(AEX-AIN)*DFLOAT(I-1)/DFLOAT(IL1)

10 CONTINUE
 DO 20 I=1,IL
 DO 20 J=1,JL
 X(I,J)=DFLOAT(I-1)/DFLOAT(IL1)*RL

20 Y(I,J)=DFLOAT(J-1)/DFLOAT(JL1)*AREA(I)
 IF(FST.NE.0.D0)THEN
 DO=(FST-1.0)/(FST**IL1-1.)*RL
 DO 15 I=1,IL
 XL=DO*(FST**((I-1)-1.)/(FST-1.))
 AREA(I)=AIN+XL/RL*(AEX-AIN)

15 DO 15 J=1,JL
 X(I,J)=XL
 Y(I,J)=DFLOAT(J-1)/DFLOAT(JL1)*AREA(I)

15 CONTINUE
 ELSE
 ENDIF

C* STRETCH THE GRID ALONG Y-DIRECETION IN VISCOUS CASE
 IF(FSTY.NE.0.D0)THEN
 DO 17 I=1,IL

```

        Y(I,1)=0.
        DAO=(1.-FSTY)/(1.-FSTY**JL1)*AREA(I)
        DO 17 J=2,JL
            Y(I,J)=Y(I,J-1)+DAO*FSTY**(J-2)
17      CONTINUE
        ELSE
        ENDIF
C * READ GRID FROM DATA FILE
        IF(IREAD.EQ.1)THEN
        DO 25 I=1,IL
        DO 25 J=1,JL
        READ(38)III,JJJ,X(I,J),Y(I,J)
25      CONTINUE
        ELSE
        END IF
C ** COORDINATE TRANSFORMATION
        EXI=1.0
        EYI=1.0
        DO 30 I=1,IL
        IP1=I
        IM1=I-1
        IF(I.EQ.1)IM1=1
        IF(I.EQ.1)IP1=2
        DSAI=2.*EXI
        IF(I.EQ.1.OR.I.EQ.IL)DSAI=EXI
        DO 30 J=1,JL
        JP1=J+1
        JM1=J-1
        IF(J.EQ.1)JM1=1
        IF(J.EQ.JL)JP1=JL
        DETA=2.*EYI
        IF(J.EQ.1.OR.J.EQ.JL)DETA=EYI
        XSAI=(X(IP1,J)-X(IM1,J))
        YSAI=(Y(IP1,J)-Y(IM1,J))
        XETA=(X(I,JP1)-X(I,JM1))/DETA
        YETA=(Y(I,JP1)-Y(I,JM1))/DETA
        IF(I.GT.2.AND.I.LT.IL1)THEN
            XSAI=XSAI+NORD*0.5*(X(I,J)-2.*X(I-1,J)+X(I-2,J))
            YSAI=YSAI+NORD*0.5*(Y(I,J)-2.*Y(I-1,J)+Y(I-2,J))
        ENDIF
        IF(J.EQ.1)THEN
            XETA=XETA-0.5*(X(I,J)-2.*X(I,J+1)+X(I,J+2))
            YETA=YETA-0.5*(Y(I,J)-2.*Y(I,J+1)+Y(I,J+2))
        ELSE
        ENDIF
C
        IF(J.EQ.JL) THEN
        XETA=(3.D0*X(I,JL)-4.D0*X(I,JL-1)+X(I,JL-2))*0.5D0
        YETA=(3.D0*Y(I,JL)-4.D0*Y(I,JL-1)+Y(I,JL-2))*0.5D0
        ELSE
        ENDIF
C
        RJP=XSAI*YETA-XETA*YSAI
        RJ(I,J)=1./RJP
        SAIX(I,J)=YETA/RJP
    
```

```

      SAIY(I,J)=-XETA/RJP
      ETAX(I,J)=-YSAI/RJP
  30    ETAY(I,J)=XSAI/RJP
C ** INITIALIZATION
      RGAS=8314.3/20.405
      R=RGAS
      DO 991 I=1,IL
      DO 991 J=1,JL
      TTT=3061.1DO
      CALL CPGAM(CP(I,J),CV(I,J),GAMMA(I,J),GM1(I,J),RGAS,I,J,
> RHO(I,J),RHOU(I,J),RHOV(I,J),E(I,J),TTT)
  991 CONTINUE
C      GM10=GAMMA0-1.
C      R=CPO*GM10/GAMMA0
C      CVO=CPO/GAMMA0
C
C*
C* GIVE THE INITIAL VALUE OF VISCOSTY
C* IF THE VISCOSITY AT T=TREF IS GIVEN FROM INPUT
C* THE CALCULATION FOR ZMU0 MUST BE SWITCHED OFF
C*
C      TIN=T0/(1.+0.5*GM10*RM1**2)
C      UIN=RM1*DSQRT(GAMMA0*R*TIN)
C      PIN=PO*(TIN/T0)**(GAMMA0/GM10)
C      RIN=PIN/(R*TIN)
C      BIOT=BIOT*Y(1,JL)
C      ZMU0=(RIN*UIN*AREA(1)*2.)/REN
C* CALCULATE METRIC TERMS AT MID POINTS
C*
      CALL MCONST
C ** SKIP TO RERUN THE CODE
      IF(NBEG.NE.1)GOTO 300
C ** READ IN THE STARTING LINES
      DO 60 I=1,2
      DO 60 J=1,JL
      READ(68) (Q(I,J,K),K=1,4)
      TCP=0.DO
      CALL CPGAM(CP(I,J),CV(I,J),GAMMA(I,J),GM1(I,J),RGAS,I,J,
> RHO(I,J),RHOU(I,J),RHOV(I,J),E(I,J),TCP)
  50    CONTINUE
      U(I,J)=RHOU(I,J)/RHO(I,J)
      V(I,J)=RHOV(I,J)/RHO(I,J)
      UN(I,J)=U(I,J)*SAIX(I,J)+V(I,J)*SAIY(I,J)
      VN(I,J)=U(I,J)*ETAX(I,J)+V(I,J)*ETAY(I,J)
      P(I,J) =GM1(I,J)*(E(I,J)-0.5*RHO(I,J)*(U(I,J)**2+V(I,J)**2))
  60    CONTINUE
C      REWIND 68
C
      RETURN
  300  CONTINUE
  310  READ(19,720,END=1000)NDUM,(SS(NDUM,K),K=1,4)
      GOTO 310
1000  CONTINUE
      REWIND 19
      NBEG=NDUM+1

```

```

NEND=NBEG+NITER-1
DO 320 N=1,NDUM
320 WRITE(19,720)N,(SS(N,K),K=1,4)
720 FORMAT(I5,3X,4(1X,E14.7))
DO 330 I=1,IL
DO 330 J=1,JL
READ(66) (Q(I,J,K),K=1,4),DELTAU(I,J)
TCP=0.D0
CALL CPGAM(CP(I,J),CV(I,J),GAMMA(I,J),GM1(I,J),RGAS,I,J,
> RHO(I,J),RHOI(I,J),RHOV(I,J),E(I,J),TCP)
U(I,J)=RHOI(I,J)/RHO(I,J)
V(I,J)=RHOV(I,J)/RHO(I,J)
UN(I,J)=U(I,J)*SAIX(I,J)+V(I,J)*SAIY(I,J)
VN(I,J)=U(I,J)*ETAX(I,J)+V(I,J)*ETAY(I,J)
P(I,J) =GM1(I,J)*(E(I,J)-0.5*RHO(I,J)*(U(I,J)**2+V(I,J)**2))
CO=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
CX=DSQRT(SAIX(I,J)**2+SAIY(I,J)**2)
CY=DSQRT(ETAX(I,J)**2+ETAY(I,J)**2)
CX=(UN(I,J)+CX*CO)/EXI
CY=(VN(I,J)+CY*CO)/EYI
EIGNN=DABS(CX)
IF(EIGNN.LE.DABS(CY))EIGNN=DABS(CY)
DELTAU(I,J)=CFL/EIGNN
330 CONTINUE
REWIND 66
RETURN
END

```

C-----

SUBROUTINE SOLVE

```

C*
C*   SOLVE SUBROUTINE
C*
C***** ****
IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=80)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
>          P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
>          ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
>          ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
>CFL1,PRNT,PB,RM1,SUM(4),ZMU0,REN,PRN,TWALL,TREF
>,BIOT,TW1
COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
>          ,IWBC,IFLOW
DIMENSION RHO(IZ,JZ),RHOI(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOI(1,1)),
>          (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C***** ****

```

C*
C* STRAT THE CODE BY PNS A PLUS MARCHING
C*

```

IF(NADV.NE.1)GOTO 5
CALL PNS

```

FILE: PNSVIS FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STAT

```
      RETURN
5      CONTINUE
C*
CALL FLUX(1)
CALL FLUX(2)
IF(IVISC.EQ.1)THEN
  CALL MULAM(1)
  CALL MULAM(2)
ENDIF
DO 40 I=3,IL
C*
C* THIS DO LOOP CONTROLS THE LOCAL ITERATION FOR
C* EACH CONSTANT XI LINE
C*
DO 35 LOCAL=1,1
CALL RHS(I)
IF(IVISC.EQ.1) THEN
  CALL MULAM(I)
  IF(PRNT.NE.0.DO) CALL MUTUR(I)
ENDIF
IF(IVISC.EQ.1)CALL VRHS(I)
C* CALCULATE RESIDUAL
DO 10 J=1,JL
DO 10 K=1,4
10 DQ(I,J,K)=-DELTAU(I,J)*DQ(I,J,K)
C*
C* ADD ETA-DIRECTION 4TH ORDER ARITFICIAL VISCOSITY
C*
IF(OMEGAY.NE.0.DO)CALL ADDY(I)
C*
C* SOLVE L-ETA OPERATOR
C*
CALL COEFY(I)
C*
C* UPDATE VARIABLES AFTER X-SWEEP
C*
C       JEND=JL
C       IF(IVISC.EQ.1)JEND=JL1
DO 20 J=2,JL
RJJ=RJ(I,J)/Y(I,J)
DO 15 K=1,4
15 Q(I,J,K)=Q(I,J,K)+DQ(I,J,K)*RJJ
TCP=0.DO
CALL CPGAM(CP(I,J),CV(I,J),GAMMA(I,J),GM1(I,J),RGAS,I,J,
> RHO(I,J),RHOU(I,J),RHOV(I,J),E(I,J),TCP)
U(I,J)=RHOU(I,J)/RHO(I,J)
V(I,J)=RHOV(I,J)/RHO(I,J)
UN(I,J)=SAIX(I,J)*U(I,J)+SAIY(I,J)*V(I,J)
VN(I,J)=U(I,J)*ETAX(I,J)+ETAY(I,J)*V(I,J)
P(I,J)=GM1(I,J)*(E(I,J)-0.5*RHO(I,J)*(U(I,J)**2+V(I,J)**2))
20 CONTINUE
CALL CLBC(I)
IF(IVISC.EQ.1.AND.IWBC.EQ.0)CALL WALLBC(I)
35 CONTINUE
40 CONTINUE
```

```

C*
C* BACKWARD SWEEP I
C*
DO 90 IB=2, IL-2
I=IL-IB+1
DO 86 LOCAL=1, 1
CALL RHS(I)
IF(IVISC.EQ.1) THEN
CALL MULAM(I)
IF(PRNT.NE.0.DO) CALL MUTUR(I)
ENDIF
IF(IVISC.EQ.1)CALL VRHS(I)
DO 50 J=1, JL
DO 50 K=1, 4
50 DQ(I,J,K)=-DELTAU(I,J)*DQ(I,J,K)
IF(OMEGAY.NE.0.DO)CALL ADDY(I)
CALL COEFY(I)
C*
C* UPDATING VARIABLES
C*
DO 70 J=2, JL
RJJ=RJ(I,J)/Y(I,J)
DO 60 K=1, 4
60 Q(I,J,K)=Q(I,J,K)+DQ(I,J,K)*RJJ
TCP=0.DO
CALL CPGAM(CP(I,J),CV(I,J),GAMMA(I,J),GM1(I,J),RGAS,I,J,
> RHO(I,J),RHOU(I,J),RHOV(I,J),E(I,J),TCP)
U(I,J)=RHOU(I,J)/RHO(I,J)
V(I,J)=RHOV(I,J)/RHO(I,J)
UN(I,J)=U(I,J)*SAIX(I,J)+V(I,J)*SAIY(I,J)
VN(I,J)=U(I,J)*ETAX(I,J)+V(I,J)*ETAY(I,J)
P(I,J)=GM1(I,J)*(E(I,J)-0.5*RHO(I,J)*(U(I,J)**2+V(I,J)**2))
CO=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
CX=DSQRT(SAIX(I,J)**2+SAIY(I,J)**2)
CY=DSQRT(ETAX(I,J)**2+ETAY(I,J)**2)
CX=(UN(I,J)+CX*CO)
CY=(VN(I,J)+CY*CO)
EIGNN=DABS(CX)
IF(EIGNN.LE.DABS(CY))EIGNN=DABS(CY)
DELTAU(I,J)=ITIME*CFL/EIGNN+(1-ITIME)*DELTAU(I,J)
70 CONTINUE
C *
C * CENTERLINE BOUNDARY CONDITIONS
CALL CLBC(I)
IF(IVISC.EQ.1.AND.IWBC.EQ.0)CALL WALLBC(I)
86 CONTINUE
90 CONTINUE
RETURN
END
C*
C* THIS SUBROUTINE SOLVE THE FLOW FIELD BY
C* MARCHING IN XI DIRECTION
C*
SUBROUTINE PNS
*****

```

```

IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=80)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
>          P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
>          ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
>          ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
>CFL1,PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF
>,BIOT,TW1
COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
>          ,IWBC,IFLOW
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
>          (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C***** ****
C* DIMENSION SS(4)
C* DATA INNER/200/
C ** FORWARD SWEEP
      WRITE(19,*)' **** PNS MARCHING BEGINS ****'
      IF(IVISC.EQ.1) CALL MULAM(1)
      IF(IVISC.EQ.1) CALL MULAM(2)
      CALL FLUX(1)
      CALL FLUX(2)
      DO 999 I=3,IL
      WRITE(19,*)' ### I=' , I
C*
C* GIVE THE INITIAL GUESS FROM PREVIOUS LINE
C*
      DO 17 J=1,JL
      C   DELTAU(I,J)=DELTAU(I-1,J)
      DO 16 K=1,4
      16 Q(I,J,K)=Q(I-1,J,K)
      TCP=0.0
      CALL CPGAM(CP(I,J),CV(I,J),GAMMA(I,J),GM1(I,J),RGAS,I,J,
> RHO(I,J),RHOU(I,J),RHOV(I,J),E(I,J),TCP)
      RHO(I,J)=RHO(I-1,J)
      U(I,J)=U(I-1,J)
      V(I,J)=V(I-1,J)
      UN(I,J)=U(I,J)*SAIX(I,J)+V(I,J)*SAIY(I,J)
      VN(I,J)=U(I,J)*ETAX(I,J)+V(I,J)*ETAY(I,J)
      IF(J.EQ.JL) VN(I,J)=0.0
      IF(J.EQ.JL)V(I,J)=-U(I,J)*ETAX(I,J)/ETAY(I,J)
      IF(J.EQ.JL) Q(I,J,2)=RHO(I,J)*U(I,J)
      IF(J.EQ.JL) Q(I,J,3)=RHO(I,J)*V(I,J)
      P(I,J)=P(I-1,J)
      17 CONTINUE
      C   IF(I.EQ.2) THEN
      DO 19 J=1,JL
      CO=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
      CY=VN(I,J)+DSQRT(ETAX(I,J)**2+ETAY(I,J)**2)*CO
      CX=UN(I,J)+DSQRT(SAIX(I,J)**2+SAIY(I,J)**2)*CO
      DELTAU(I,J)=CFL1/DABS(CY)
      C   DELTAU(I,J)=CFL1/DABS(CX)

```

```

19    CONTINUE
C     ENDIF
C*
DO 998 ICOUNT=1, INNER
C* RHS CALCULATION
CALL RHS(I)
IF(IVISC.EQ.1) CALL MULAM(I)
IF(PRNT.NE.0.DO) CALL MUTUR(I)
IF(IVISC.EQ.1) CALL VRHS(I)
DO 40 J=1,JL
DO 40 K=1,4
40 DQ(I,J,K)=-DELTAU(I,J)*DQ(I,J,K)
C*
C* ADD FTA-DIRECTION 4TH ORDER ARTIFICIAL VISCOSITY
C*
IF(OMEGAY.NE.0.ODO)CALL ADDY(I)
C*
C* SOLVE LETA-OPERATOR
C*
CALL COEFY(I)
C*
C* UPDATING VARIABLES
C*
DO 70 J=2,JL
RJJ=RJ(I,J)/Y(I,J)
DO 60 K=1,4
60 Q(I,J,K)=Q(I,J,K)+DQ(I,J,K)*RJJ
TCP=0.DO
CALL CPGAM(CP(I,J),CV(I,J),GAMMA(I,J),GM1(I,J),RGAS,I,J,
> RHO(I,J),RHOU(I,J),RHOV(I,J),E(I,J),TCP)
U(I,J)=RHOU(I,J)/RHO(I,J)
V(I,J)=RHOV(I,J)/RHO(I,J)
UN(I,J)=U(I,J)*SAIX(I,J)+V(I,J)*SAIY(I,J)
VN(I,J)=U(I,J)*ETAX(I,J)+V(I,J)*ETAY(I,J)
P(I,J)=GM1(I,J)*(E(I,J)-0.5*RHO(I,J)*(U(I,J)**2+V(I,J)**2))
CO=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
CX=DSQRT(SAIX(I,J)*SAIX(I,J)+SAIY(I,J)*SAIY(I,J))
CY=DSQRT(ETAX(I,J)*ETAX(I,J)+ETAY(I,J)*ETAY(I,J))
CX=(UN(I,J)+CX*CO)/EXI
CY=(VN(I,J)+CY*CO)/EYI
EIGNN=DABS(CY)
DELTAU(I,J)=ITIME*CFL1/EIGNN+(1-ITIME)*DELTAU(I,J)
70 CONTINUE
C*
C* EXTRAPOLATE FROM FIELD POINT TO CENTER LINE
C*
CALL CLBC(I)
IF(IVSC.EQ.1.AND.IWBC.EQ.0)CALL WALLBC(I)
C*
C* CALCULATE THE ERROR
C*
DO 110 K=1,4
110 SS(K)=0.
DO 120 J=1,JL
DO 120 K=1,4

```

```

QQ=Q(I,J,K)
IF(QQ.EQ.0.DO.OR.Y(I,J).EQ.0.DO)GO TO 120
SS(K)=SS(K)+(DQ(I,J,K)/(QQ*Y(I,J)/RJ(I,J)))**2
120 CONTINUE
QSUM=0.
DO 130 K=1,4
QSUM=QSUM+DSQRT(SS(K))
130 SS(K)=DSQRT(SS(K))/(IL*JL)
QSUM=QSUM/4./(IL*JL)
IF(QSUM.LE.1.D-13) GOTO 995
WRITE(19,500) ICOUNT, (SS(K),K=1,4)
500 FORMAT(I5,3X,4(1X,E14.7))
998 CONTINUE
995 CONTINUE
WRITE(19,510) (SS(K),K=1,4)
510 FORMAT(' &&& ',4(1X,E14.7))
999 CONTINUE
WRITE(19,*) ' **** PNS MARCHING ENDS *****'
CALL MASS
RETURN
END

C*
C* SUBROUTINE FOR CALCULATING METRIC TERMS
C* AT THE MIDPOINT
SUBROUTINE MCONST
C***** ****
IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=80)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
> P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
> ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
> ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
> CFL1,PRNT,PB,RM1,SUM(4),ZMU0,REN,PRN,TWALL,TREF
>,BIOT,TW1
COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,ILL,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
> ,IWBC,IFLOW
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****
DATA FD3,OD3/1.33333333333,0.33333333333/
DO 20 I=2,IL
DO 20 J=1,JL1
IF(I.EQ.IL)THEN
XSAI=0.5*(X(I,J)+X(I,J+1)-X(I-1,J)-X(I-1,J+1))
YSAI=0.5*(Y(I,J)+Y(I,J+1)-Y(I-1,J)-Y(I-1,J+1))
ELSE
YSAI=0.25*(Y(I+1,J+1)+Y(I+1,J)-Y(I-1,J+1)-Y(I-1,J))
XSAI=0.25*(X(I+1,J+1)+X(I+1,J)-X(I-1,J+1)-X(I-1,J))
END IF
YETA=Y(I,J+1)-Y(I,J)
XETA=X(I,J+1)-X(I,J)

```

```

RJJ=1./(XSAI*YETA-XETA*YSAI)
A1(I,J)=RJJ*(FD3*YSAI**2+XSAI**2)
A2(I,J)=-RJJ*OD3*XSAI*YSAI
A3(I,J)=RJJ*(YSAI**2+FD3*XSAI**2)
A4(I,J)=RJJ*(XSAI**2+YSAI**2)
20 CONTINUE
RETURN
END
C-----SUBROUTINE SMOOTH
C*
C* ADD ARTIFICIAL DISSIPATIONAL TERM FOR SAI,ETA-DIRECTION
C*
C*****IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=80)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
> P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
> ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
> ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
> CFL1,PRNT,PB,RM1,SUM(4),ZMU0,REN,PRN,TWALL,TREF
>,BIOT,TW1
COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
> ,IWBC,IFLOW
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****DIMENSION ADD(4)
C ** SAI-DIRECTION
ENTRY ADDX
COEF=0.125D0*OMEGAX
DO 70 J=1,JL
DO 70 I=1,IL
IF(I.EQ.1) GO TO 10
IF(I.EQ.2) GO TO 20
IF(I.EQ.IL1) GO TO 30
IF(I.EQ.IL) GO TO 40
DO 5 K=1,4
5 ADD(K)=COEF*(Q(I+2,J,K)-4.*Q(I+1,J,K)
> +6.*Q(I,J,K)-4.*Q(I-1,J,K)
> +Q(I-2,J,K))
GO TO 50
10 DO 15 K=1,4
QM=2.*Q(1,J,K)-Q(2,J,K)
QMM=2.*QM-Q(1,J,K)
15 ADD(K)=COEF*(Q(I+2,J,K)-4.*Q(I+1,J,K)
> +6.*Q(I,J,K)-4.*QM+QMM)
GO TO 50
20 DO 25 K=1,4
QMM=2.*Q(1,J,K)-Q(2,J,K)
25 ADD(K)=COEF*(Q(I+2,J,K)-4.*Q(I+1,J,K)

```

```

>          +6.*Q(I,J,K)-4.*Q(I-1,J,K)
>          +QMM)
GO TO 50
30 DO 35 K=1,4
QPP=2.*Q(I+1,J,K)-Q(I,J,K)
35 ADD(K)=COEF*(QPP-4.*Q(I+1,J,K)+6.*Q(I,J,K)
>          -4.*Q(I-1,J,K)+Q(I-2,J,K)
>          )
GO TO 50
40 DO 45 K=1,4
QP=2.*Q(I,J,K)-Q(I-1,J,K)
QPP=2.*QP-Q(I,J,K)
45 ADD(K)=COEF*(QPP-4.*QP+6.*Q(I,J,K)-4.*Q(I-1,J,K)+Q(I-2,J,K))
50 CONTINUE
DO 60 K=1,4
60 DQ(I,J,K)=DQ(I,J,K)-ADD(K)/RJ(I,J)*Y(I,J)
70 CONTINUE
RETURN
C **
C   ADD ETA-DLRECTLON 4TH ORDER ARTLFLCLAL VLSCOSLTY
C **
      ENTRY ADDY(II)
I=II
COEF=0.125DO*OMEGAY
DO 170 J=1,JL
IF(J.EQ.1) GO TO 110
IF(J.EQ.2) GO TO 120
IF(J.EQ.JL1) GO TO 130
IF(J.EQ.JL) GO TO 140
DO 95 K=1,4
95 ADD(K)=COEF*(Q(I,J+2,K)-4.*Q(I,J+1,K)
>          +6.*Q(I,J,K)-4.*Q(I,J-1,K)
>          +Q(I,J-2,K))
GO TO 150
110 DO 115 K=1,4
QM=2.*Q(I,1,K)-Q(I,2,K)
QMM=2.*QM-Q(I,1,K)
115 ADD(K)=COEF*(Q(I,J+2,K)-4.*Q(I,J+1,K)
>          +6.*Q(I,J,K)-4.*QM+QMM)
GO TO 150
120 DO 125 K=1,4
QMM=2.*Q(I,1,K)-Q(I,2,K)
125 ADD(K)=COEF*(Q(I,J+2,K)-4.*Q(I,J+1,K)
>          +6.*Q(I,J,K)-4.*Q(I,J-1,K)
>          +QMM)
GO TO 150
130 DO 135 K=1,4
QPP=2.*Q(I,J+1,K)-Q(I,J,K)
135 ADD(K)=COEF*(QPP-4.*Q(I,J+1,K)+6.*Q(I,J,K)
>          -4.*Q(I,J-1,K)+Q(I,J-2,K)
>          )
GO TO 150
140 DO 145 K=1,4
QP=2.*Q(I,J,K)-Q(I,J-1,K)

```

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```
QPP=2.*QP-Q(I,J,K)
145 ADD(K)=COEF*(QPP-4.*QP+6.*Q(I,J,K)-4.*  
    > Q(I,J-1,K)+Q(I,J-2,K))
150 CONTINUE
DO 160 K=1,4
160 DQ(I,J,K)=DQ(I,J,K)-ADD(K)/RJ(I,J)*Y(I,J)
170 CONTINUE
RETURN
END
C
C ** SUBROUTINE FOR CENTER LINE BOUNDARY CONDITIONS
SUBROUTINE BC
C-----
IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=80)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
> P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
> ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
> ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
> CFL1,PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF
> ,BIOT,TW1
COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
> ,IWBC,IFLOW
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****
DATA SCONST/196./
ENTRY CLBC(II)
I=II
C * THE QUANTITIES EXTRAPOLATED ARE U,P,T AND LET V=0
C
SY=SAIY(I,1)
EY=ETAY(I,1)
DENOM=SY-1.5*EY
IF(I.NE.2.AND.I.LT.IL1)DENOM=DENOM+0.5*NORD*SY
IF(I.EQ.1)THEN
UIM1=0.
PIM1=0.
RIM1=1.0
ELSE
UIM1=U(I-1,1)
PIM1=P(I-1,1)
RIM1=RHO(I-1,1)
END IF
V(I,1)=0.
U(I,1)=(SY*UIM1-0.5*EY*(4.*U(I,2)-U(I,3)))/DENOM
IF(I.NE.2.AND.I.LT.IL1) U(I,1)=U(I,1)+NORD*SY*(U(I-1,1)-
* 0.5*U(I-2,1))/DENOM
UN(I,1)=SAIX(I,1)*U(I,1)
VN(I,1)=ETAX(I,1)*U(I,1)
P(I,1)=(SY*PIM1-0.5*EY*(4.*P(I,2)-P(I,3)))/DENOM
```

```

    IF(I.NE.2.AND.I.LT.IL1) P(I,1)=P(I,1)+NORD*SY*(P(I-1,1)-
*   0.5*P(I-2,1))/DENOM
    RIV=1./RGAS
    TIM1=PIM1/RIM1*RIV
    T2=P(I,2)/RHO(I,2)*RIV
    T3=P(I,3)/RHO(I,3)*RIV
    T1=(SY*TIM1-0.5*EY*(4.*T2-T3))/DENOM
    IF(I.NE.2.AND.I.LT.IL1)THEN
      TIM2=P(I-2,1)/RHO(I-2,1)*RIV
      T1=T1+NORD*SY*(TIM1-0.5*TIM2)/DENOM
    ENDIF
    CALL CPGAM(CP(I,1),CV(I,1),GAMMA(I,1),GM1(I,1),RGAS,I,1,
> RHO(I,1),RHOU(I,1),RHOV(I,1),E(I,1),T1)
    RHO(I,1)=P(I,1)/T1*RIV
    RHOU(I,1)=RHO(I,1)*U(I,1)
    RHOV(I,1)=RHO(I,1)*V(I,1)
    E(I,1)=P(I,1)/GM1(I,1)+0.5*RHO(I,1)*(U(I,1)**2+V(I,1)**2)
    RETURN
C*
ENTRY WALLBC(II)
I=II
J=JL
CC1=ETAX(I,J)*SAIX(I,J)+ETAY(I,J)*SAIY(I,J)
CC2=ETAX(I,J)**2+ETAY(I,J)**2
IF(I.NE.IL)THEN
  AM=-0.5*CC1
  BM=1.5*CC2
  CM=0.5*CC1
  DM=CC2*(2.*P(I,J-1)-0.5*P(I,J-2))
ELSE
  AM=-CC1
  BM=CC1+1.5*CC2
  CM=0.
  DM=CC2*(2.*P(I,J-1)-0.5*P(I,J-2))
ENDIF
IP1=I+1
IF(I.EQ.IL)IP1=IL
PSOL=(DM-AM*P(I-1,J)-CM*P(IP1,J))/BM
IF(I.EQ.IL.AND.PB.NE.0.DO)PSOL=PB
RIV=1./RGAS
IF(IWALL.EQ.0)THEN
  T1=P(I,J-1)*RIV/RHO(I,J-1)
  T2=P(I,J-2)*RIV/RHO(I,J-2)
  DM=CC2*(2.*T1-0.5*T2)
  TIM1=P(I-1,J)*RIV/RHO(I-1,J)
  TIP1=P(IP1,J)*RIV/RHO(IP1,J)
  TSOL=(DM-AM*TIM1-CM*TIP1)/BM
ELSE
ENDIF
IF(IWALL.EQ.0)THEN
  TT=TSOL
ELSE
  TT=TWALL
ENDIF
PP=PSOL

```

```

U(I,JL)=0.
V(I,JL)=0.
RHOU(I,JL)=0.
RHOV(I,JL)=0.
RHOO=PP*RIV/TT
RHO(I,JL)=RHOO
CALL CPGAM(CP(I,JL),CV(I,JL),GAMMA(I,JL),GM1(I,JL),RGAS,I,JL,
> RHO(I,JL),RHOU(I,JL),RHOV(I,JL),E(I,JL),TT)
E(I,JL)=PP/GM1(I,JL)
P(I,JL)=PP
UN(I,JL)=0.
VN(I,JL)=0.
RETURN

```

```

C*
C* LAMINAR VISCOSITY CALCULATION
C*
```

```

C ENTRY MULAM(II)
```

```

C I=III
```

```

C* USE SUTHERLAND LAW
```

```

C DO 60 J=1,JL
```

```

C TOS=TREF+SCONST
```

```

C TT=(E(I,J)/RHO(I,J)-0.5*(U(I,J)**2+V(I,J)**2))/CV(I,J)
```

```

C TTS=TT+SCONST
```

```

C ZMU(I,J)=ZMUO*TOS/TTS*(TT/TREF)**1.5
```

```

C ZMU(I,J)=ZMUO
```

```

C ZMU(I,J)=ZMUO*(TT/TREF)**0.67
```

```

C 60 CONTINUE
```

```

C RETURN
```

```

C END
```

```

C*****SUBROUTINE MULAM(NN)*****

```

```

C*****IMPLICIT REAL*8(A-H,O-Z)

```

```

C PARAMETER (IZ=150,JZ=80)
```

```

C COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),

```

```

> P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
```

```

C COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
```

```

> ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
```

```

> ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
```

```

C COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,MEGAY,CFL,THETA,PO,TO,

```

```

>CFL1,FRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF
```

```

> ,BIOT,TW1
```

```

C COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
```

```

C COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL

```

```

> ,IWBC,IFLOW
```

```

DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
```

```

EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),

```

```

> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))

```

```

C*****B1=4.3222557667160623D-06

```

```

B2=3.8885996244952953D-08

```

```

B3=-3.7263546610032919D-12

```

```

C DO 50 NN=1,IL

```

```

DO 50 MM=1,JL

```

```

TT=(E(NN,MM)/RHO(NN,MM)-0.5*(U(NN,MM)**2+V(NN,MM)**2))/CV(NN,MM)

```

```

      ZMU(NN,MM)=B1+B2*TT+B3*TT*TT
50    CONTINUE
      RETURN
      END
C
C     BOLDWIN & LOMAX TURBULENCE MODEL
C
      SUBROUTINE MUTUR(II)
C***** ****
      IMPLICIT REAL*8(A-H,O-Z)
      PARAMETER (IZ=150,JZ=80)
      COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
>          P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
      COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
>          ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
>          ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
      COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
>CFL1,PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF
>,BIOT,TW1
      COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
      COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
>          ,IWBC,IFLOW
      DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
      EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
>          (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****
      DIMENSION YVERT(JZ),ZMUI(JZ)
      DATA AP,CCP,CKLEB,CWK,VKCON,XK/26., 1.6, .3, .25, .4, .0168/
      DATA ZMUI/JZ*0.0/
      I=II
      FYMAX = 0.0
      YMAX = 0.0
      UDIF=0.
      YVERT(JL) = 0.0
      TAUW = ZMU(I,JL)*DABS(ETAY(I,JL)*(U(I,JL)-U(I,JL-1))-
>          ETAX(I,JL)*(V(I,JL)-V(I,JL-1)))
      CYP = DSQRT(RHO(I,JL)*TAUW)/ZMU(I,JL)
C
      DO 10 KK = 2,JL1
      K = JL+1-KK
      YVER = YVERT(K+1) + 1.0/DSQRT(ETAX(I,K)**2 + ETAY(I,K)**2)
      OMG = DABS( ETAY(I,K)*(U(I,K+1)-U(I,K-1)).5
>          +SAIY(I,K)*(U(I,K) -U(I-1,K))
>          -ETAX(I,K)*(V(I,K+1)-V(I,K-1)).5
>          -SAIX(I,K)*(V(I,K) -V(I-1,K)) )
      YPLUS = CYP*YVER
      TURLEN = VKCON*YVER*(1.0D0 -DEXP(-YPLUS/AP))
      ZMUI(K) = RHO(I,K)*OMG*TURLEN**2
      FY = TURLEN/VKCON*OMG
      UTOTAL= DSQRT(U(I,K)**2+V(I,K)**2)
      IF(UTOTAL.GE.UDIF) UDIF=UTOTAL
      IF(FY .LT. FYMAX) GO TO 10
      FYMAX = FY
      YMAX = YVER
10    YVERT(K) = YVER

```

```

C
VXDIF = UDIF
FWAKE1=YMAX*FYMAX
FWAKE2=CWK*YMAX*VXDIF**2/FYMAX
FWAKE =DMIN1(FWAKE1,FWAKE2)

C
DO 20 KK = 2, JL1
K = JL+1-KK
FKLEB = (CKLEB*YVERT(K)/YMAX)**6
FKLEB = 1./(1.0 + 5.5*FKLEB)
ZM0 = XK*CCP*RHO(I,K)*FWAKE*FKLEB
IF(ZMUI(K).GT.ZM0) THEN
ZMUTUR = ZM0
ELSE
ZMUTUR = ZMUI(K)
END IF
ZMUT(K)= ZMUTUR
ZMU(I,K) = ZMU(I,K) + ZMUTUR
C      WRITE(77,119)K,Y(I,K),YVERT(K),U(I,K),ZMUI(K),ZM0,ZMU(I,K)
C119  FORMAT(2X,I3,6(2X,D13.6))
20    CONTINUE
C
ZMUT(1)=0.
ZMUT(JL)=0.
RETURN
END

C* SOURCE TERM JACOBIAN MATRIX
SUBROUTINE DHDQ(D,I,J)
C-----
IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=80)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
>          P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
>          ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
>          ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
>CFL1,PRNT,PB,RM1,SUM(4),ZM0,REN,PRN,TWALL,TREF
>,BIOT,TW1
COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
>          ,IWBC,IFLOW
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
>          (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****
DIMENSION D(4,4)
CALL SZERO(4,D)
IF(IVISC.EQ.0)THEN
R2MY=0.
ELSE
R2MY=4./3.*ZMU(I,J)/(Y(I,J)*Y(I,J)*RHO(I,J))
END IF
D(3,1)=-.5*GM1(I,J)*(U(I,J)**2+V(I,J)**2)/Y(I,J)+IVISC*V(I,J)*R2MY
D(3,2)=-GM1(I,J)*U(I,J)/Y(I,J)

```

FILE: PNSVIS FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STA

```
D(3,3)=-GM1(I,J)*V(I,J)/Y(I,J)-IVISC*R2MY
D(3,4)=GM1(I,J)/Y(I,J)
RETURN
END
SUBROUTINE JACCAL
C*
C* SUBROUTINE FOR JACOBIAN METRIX
C* IF IA=1, ACAP MATRIX
C* IF IA=2, BCAP MATRIX
C*
C*****IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=80)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
> P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
> ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
> ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
> CFL1,PRNT,PB,RM1,SUM(4),ZMU0,REN,PRN,TWALL,TREF
>,BIOT,TW1
COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,ILL,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
> ,IWBC,IFLOW
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****DIMENSION A(4,4),B(4,4),C(4,4),TEMP(4,4),BB(4,4),DIAG(4)
C*****
ENTRY JACOB(IA,A,I,J)
IF(IA.EQ.2)GO TO 10
CX=SAIX(I,J)
CY=SAIY(I,J)
CONTRA=UN(I,J)
GO TO 20
10 CX=ETAX(I,J)
CY=ETAY(I,J)
CONTRA=VN(I,J)
20 CONTINUE
PHI2=0.5*GM1(I,J)*(U(I,J)**2+V(I,J)**2)
A(1,1)=0.ODO
A(1,2)=CX
A(1,3)=CY
A(1,4)=0.DO
A(2,1)=CX*PHI2-U(I,J)*CONTRA
A(2,2)=CONTRA-(GAMMA(I,J)-2.)*CX*U(I,J)
A(2,3)=CY*U(I,J)-GM1(I,J)*CX*V(I,J)
A(2,4)=GM1(I,J)*CX
A(3,1)=CY*PHI2-V(I,J)*CONTRA
A(3,2)=CX*V(I,J)-GM1(I,J)*CY*U(I,J)
A(3,3)=CONTRA-CY*V(I,J)*(GAMMA(I,J)-2.)
A(3,4)=GM1(I,J)*CY
A(4,1)=CONTRA*(2.*PHI2-GAMMA(I,J)*E(I,J)/RHO(I,J))
A(4,2)=CX*(GAMMA(I,J)*E(I,J)/RHO(I,J)-PHI2)-GM1(I,J)*CONTRA
```

```

> *U(I,J)
A(4,3)=CY*(GAMMA(I,J)*E(I,J)/RHO(I,J)-PHI2)-GM1(I,J)*CONTRA
` *V(I,J)
A(4,4)=GAMMA(I,J)*CONTRA
RETURN
C*
C* SPLITTED JACOBIAN MATRIX IN XI-DIRECTION
C*
C* ENTRY AJACOB(IA,A,I,J)
C*
C* FOR THE FIRST ITERATION TURN OFF A MINUS
C*
IF(NADV.EQ.1.AND.IA.EQ.2) THEN
  CALL SZERO(4,A)
  RETURN
ENDIF
C
WRITE(6,*) I,J,RHO(I,J)
CO=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
CX=DSQRT(SAIX(I,J)**2+SAIY(I,J)**2)
CXCO=CX*CO
EIG1=UN(I,J)
EIG2=UN(I,J)
EIG3=UN(I,J)+CXCO
EIG4=UN(I,J)-CXCO
IF(IA.EQ.1)THEN
  DIAG(1)=0.5*(EIG1+DABS(EIG1))
  DIAG(2)=DIAG(1)
  DIAG(3)=0.5*(EIG3+DABS(EIG3))
  DIAG(4)=0.5*(EIG4+DABS(EIG4))
ELSE
  DIAG(1)=0.5*(EIG1-DABS(EIG1))
  DIAG(2)=DIAG(1)
  DIAG(3)=0.5*(EIG3-DABS(EIG3))
  DIAG(4)=0.5*(EIG4-DABS(EIG4))
ENDIF
CALL EIGEN(1,BB,I,J)
DO 40 II=1,4
  DO 40 JJ=1,4
    TEMP(II,JJ)=DIAG(II)*BB(II,JJ)
40 CONTINUE
CALL EIGAR(BB,I,J)
CALL MMM(4,BB,TEMP,A)
RETURN
C*
C* TRUE JACOBIAN FOR DE+-/DQ
C*
C* ENTRY TRUEJ(IA,A,I,J)
C CHECK THE FOURTH EIGEN VALUE
CO=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
CX=DSQRT(SAIX(I,J)**2+SAIY(I,J)**2)
CXCO=CX*CO
EIG4=UN(I,J)-CXCO
IF(UN(I,J).LT.0.D0)GOTO 60
IF(EIG4.LT.0.D0)GOTO 50
C

```

```

IF(IA.EQ.1)THEN
CX=SAIX(I,J)
CY=SAIY(I,J)
CONTRA=UN(I,J)
PHI2=0.5*GM1(I,J)*(U(I,J)**2+V(I,J)**2)
A(1,1)=0.ODO
A(1,2)=CX
A(1,3)=CY
A(1,4)=0.D0
A(2,1)=CX*PHI2-U(I,J)*CONTRA
A(2,2)=CONTRA-(GAMMA(I,J)-2.)*CX*U(I,J)
A(2,3)=CY*U(I,J)-GM1(I,J)*CX*V(I,J)
A(2,4)=GM1(I,J)*CX
A(3,1)=CY*PHI2-V(I,J)*CONTRA
A(3,2)=CX*V(I,J)-GM1(I,J)*CY*U(I,J)
A(3,3)=CONTRA-CY*V(I,J)*(GAMMA(I,J)-2.)
A(3,4)=GM1(I,J)*CY
A(4,1)=CONTRA*(2.*PHI2-GAMMA(I,J)*E(I,J)/RHO(I,J))
A(4,2)=CX*(GAMMA(I,J)*E(I,J)/RHO(I,J)-PHI2)-GM1(I,J)*CONTRA
> *U(I,J)
A(4,3)=CY*(GAMMA(I,J)*E(I,J)/RHO(I,J)-PHI2)-GM1(I,J)*CONTRA
> *V(I,J)
A(4,4)=GAMMA(I,J)*CONTRA
ELSE
CALL SZERO(4,A)
ENDIF
RETURN

```

C

```

50 CONTINUE
IF(NADV.EQ.1.AND.IA.EQ.2)THEN
CALL SZERO(4,A)
RETURN
ELSE
PHI2=0.5*GM1(I,J)*(U(I,J)**2+V(I,J)**2)
ERC=E(I,J)/RHO(I,J)/CO
ECR=E(I,J)*CO/RHO(I,J)
R1=SAIX(I,J)
R2=SAIY(I,J)
R1T=R1/CX
R2T=R2/CX
G2M2=(2.*GAMMA(I,J)-1.)*.5/GAMMA(I,J)
G23G=(-GAMMA(I,J)**2+3.*GAMMA(I,J)-1.)*.5/GAMMA(I,J)
G34G=(3.*GAMMA(I,J)-2.)*.25/GAMMA(I,J)
GM12=GM1(I,J)**2*.5/GAMMA(I,J)
CGEC=CO*.5/GAMMA(I,J)-0.25*GM1(I,J)*ERC
RKUU=CX*U(I,J)+R1T*UN(I,J)
RKVU=CX*V(I,J)+R2T*UN(I,J)
U2V2=PHI2/GM1(I,J)**2.
RKU2=.25*GM1(I,J)*(CX*.5*U2V2+UN(I,J)**2/CX)

```

C

```

IF(IA.EQ.1)THEN
A(1,1)=.25*GM1(I,J)*CX*ERC
A(1,2)=G2M2*R1-.25*GM1(I,J)*CX*U(I,J)/CO
A(1,3)=G2M2*R2-.25*GM1(I,J)*CX*V(I,J)/CO
A(1,4)=.25*GM1(I,J)*CX/CO

```

```

A(2,1)=-G2M2*U(I,J)*UN(I,J)+.5*R1*PHI2-CGEC*RKUU
A(2,2)=G23G*R1*U(I,J)+G2M2*UN(I,J)+.5*(CX+R1*R1T)/GAMMA(I,J)*CO-
> 0.25*GM1(I,J)*U(I,J)/CO*RKUU
A(2,3)=G2M2*R2*U(I,J)-.5*GM1(I,J)*R1*V(I,J)+.5*R1T*R2
> /GAMMA(I,J)*CO-0.25*GM1(I,J)*V(I,J)/CO*RKUU
A(2,4)=.5*GM1(I,J)*R1+.25*GM1(I,J)*RKUU/CO
A(3,1)=-G2M2*V(I,J)*UN(I,J)+0.5*R2*PHI2-CGEC*RKVU
A(3,2)=G2M2*R1*V(I,J)-.5*GM1(I,J)*R2*U(I,J)+0.5*R1*R2T
> /GAMMA(I,J)*CO-0.25*GM1(I,J)*U(I,J)/CO*RKVU
A(3,3)=G2M2*UN(I,J)+G23G*R2*V(I,J)+(CX+R2T*R2)*.5/GAMMA(I,J)*CO-
> 0.25*GM1(I,J)*V(I,J)/CO*RKVU
A(3,4)=.5*GM1(I,J)*R2+.25*GM1(I,J)*RKVU/CO
A(4,1)=GM12*UN(I,J)*U2V2-.5*GAMMA(I,J)*UN(I,J)*E(I,J)
> /RHO(I,J)+CX/GAMMA(I,J)*PHI2*CO-UN(I,J)**2*CO/GAMMA(I,J)/CX
> -.25*CX*ECR+Rku2*ERC
A(4,2)=-GM12*U(I,J)*UN(I,J)+.5*R1*GAMMA(I,J)*E(I,J)/RHO(I,J)
> -GM1(I,J)*.5/GAMMA(I,J)*R1*PHI2-G34G*CX*U(I,J)*CO+R1T
> /GAMMA(I,J)*UN(I,J)*CO-RKU2*U(I,J)/CO
A(4,3)=-GM12*V(I,J)*UN(I,J)+.5*R2*GAMMA(I,J)*E(I,J)/RHO(I,J)
> -GM1(I,J)*.5/GAMMA(I,J)*R2*PHI2-G34G*CX*V(I,J)*CO+R2T
> /GAMMA(I,J)*UN(I,J)*CO-RKU2*V(I,J)/CO
A(4,4)=.5*GAMMA(I,J)*UN(I,J)+.75*CX*CO+Rku2/CO
ELSE
G11G=(1.+GAMMA(I,J)-GAMMA(I,J)**2)*.5/GAMMA(I,J)
G22M=(GAMMA(I,J)**2-1.)*.5/GAMMA(I,J)
A(1,1)=-.25*GM1(I,J)*CX*ERC
A(1,2)=.5/GAMMA(I,J)*R1+.25*GM1(I,J)*CX*U(I,J)/CO
A(1,3)=.5/GAMMA(I,J)*R2+.25*GM1(I,J)*CX*V(I,J)/CO
A(1,4)=-.25*GM1(I,J)*CX/CO
A(2,1)=-.5/GAMMA(I,J)*U(I,J)*UN(I,J)+.5*R1*PHI2+CGEC*RKUU
A(2,2)=G11G*R1*U(I,J)+.5/GAMMA(I,J)*UN(I,J)-.5*(CX+R1*R1T)
> /GAMMA(I,J)*CO+0.25*GM1(I,J)*U(I,J)/CO*RKUU
A(2,3)=.5/GAMMA(I,J)*R2*U(I,J)-.5*GM1(I,J)*R1*V(I,J)-.5*R1T*R2
> /GAMMA(I,J)*CO+0.25*GM1(I,J)*V(I,J)/CC*RKUU
A(2,4)=.5*GM1(I,J)*R1-.25*GM1(I,J)*RKUU/CO
A(3,1)=-.5/GAMMA(I,J)*V(I,J)*UN(I,J)+0.5*R2*PHI2+CGEC*RKVU
A(3,2)=.5/GAMMA(I,J)*R1*V(I,J)-.5*GM1(I,J)*R2*U(I,J)-0.5*R1*R2T
> /GAMMA(I,J)*CO+0.25*GM1(I,J)*U(I,J)/CO*RKVU
A(3,3)=.5/GAMMA(I,J)*UN(I,J)+G11G*R2*V(I,J)-(CX+R2T*R2)*.5
> /GAMMA(I,J)*CO+0.25*GM1(I,J)*V(I,J)/CO*RKVU
A(3,4)=.5*GM1(I,J)*R2-.25*GM1(I,J)*RKVU/CO
A(4,1)=G22M*UN(I,J)*U2V2-.5*GAMMA(I,J)*UN(I,J)*E(I,J)/RHO(I,J)-
> CX/GAMMA(I,J)*PHI2*CO+UN(I,J)**2*CO/GAMMA(I,J)/CX
> +.25*CX*ECR-RKU2*ERC
A(4,2)=-G22M*U(I,J)*UN(I,J)+.5*R1*GAMMA(I,J)*E(I,J)/RHO(I,J)
> -(GAMMA(I,J)+1.)*.5/GAMMA(I,J)*R1*PHI2+G34G*CX*U(I,J)
> *CO-R1T/GAMMA(I,J)*UN(I,J)*CO+Rku2*U(I,J)/CO
A(4,3)=-G22M*V(I,J)*UN(I,J)+.5*R2*GAMMA(I,J)*E(I,J)/RHO(I,J)
> -(GAMMA(I,J)+1.)*.5/GAMMA(I,J)*R2*PHI2+G34G*CX*V(I,J)
> *CO-R2T/GAMMA(I,J)*UN(I,J)*CO+Rku2*V(I,J)/CO
A(4,4)=.5*GAMMA(I,J)*UN(I,J)-.75*CX*CO-RKU2/CO
ENDIF
ENDIF
RETURN
CONTINUE

```

```

C*
C* REVERSE FLOW REGION
C*
1010 IF(NADV.EQ.1) THEN
      WRITE(6,1010)
      FORMAT(' *** REVERSE FLOW FOR PNS MARCHING *** ')
      RETURN
ENDIF
EIG3=UN(I,J)+CXCO
IF(EIG3.LT.0.D0)THEN
  IF(IA.EQ.1)THEN
    CALL SZERO(4,A)
    RETURN
  ELSE
    CX=SAIX(I,J)
    CY=SAIY(I,J)
    CONTRA=UN(I,J)
    PHI2=0.5*GM1(I,J)*(U(I,J)**2+V(I,J)**2)
    A(1,1)=0.0D0
    A(1,2)=CX
    A(1,3)=CY
    A(1,4)=0.D0
    A(2,1)=CX*PHI2-U(I,J)*CONTRA
    A(2,2)=CONTRA-(GAMMA(I,J)-2.)*CX*U(I,J)
    A(2,3)=CY*U(I,J)-GM1(I,J)*CX*V(I,J)
    A(2,4)=GM1(I,J)*CX
    A(3,1)=CY*PHI2-V(I,J)*CONTRA
    A(3,2)=CX*V(I,J)-GM1(I,J)*CY*U(I,J)
    A(3,3)=CONTRA-CY*V(I,J)*(GAMMA(I,J)-2.)
    A(3,4)=GM1(I,J)*CY
    A(4,1)=CONTRA*(2.*PHI2-GAMMA(I,J)*E(I,J)/RHO(I,J))
    A(4,2)=CX*(GAMMA(I,J)*E(I,J)/RHO(I,J)-PHI2)-GM1(I,J)*CONTRA
    > *U(I,J)
    A(4,3)=CY*(GAMMA(I,J)*E(I,J)/RHO(I,J)-PHI2)-GM1(I,J)*CONTRA
    > *V(I,J)
    A(4,4)=GAMMA(I,J)*CONTRA
    RETURN
  ENDIF
ENDIF
C
PHI2=0.5*GM1(I,J)*(U(I,J)**2+V(I,J)**2)
ERC=E(I,J)/RHO(I,J)/CO
ECR=E(I,J)*CO/RHO(I,J)
R1=SAIX(I,J)
R2=SAIY(I,J)
R1T=R1/CX
R2T=R2/CX
G2M2=(2.*GAMMA(I,J)-1.)*.5/GAMMA(I,J)
G23G=(-GAMMA(I,J)**2+3.*GAMMA(I,J)-1.)*.5/GAMMA(I,J)
G34G=(3.*GAMMA(I,J)-2.)*.25/GAMMA(I,J)
GM12=GM1(I,J)**2*.5/GAMMA(I,J)
CGEC=CO*.5/GAMMA(I,J)-0.25*GM1(I,J)*ERC
RKUU=CX*U(I,J)+R1T*UN(I,J)
RKVU=CX*V(I,J)+R2T*UN(I,J)
U2V2=PHI2/GM1(I,J)*2.

```

RKU2=.25*GM1(I,J)*(CX*.5*U2V2+UN(I,J)**2/CX)
 G11G=(1.+GAMMA(I,J)-GAMMA(I,J)**2)*.5/GAMMA(I,J)
 G22M=(GAMMA(I,J)**2-1.)*.5/GAMMA(I,J)

C

```

IF (IA.EQ.1)THEN
A(1,1)=.25*GM1(I,J)*CX*ERC
A(1,2)=0.5/GAMMA(I,J)*R1-.25*GM1(I,J)*CX*U(I,J)/CO
A(1,3)=0.5/GAMMA(I,J)*R2-.25*GM1(I,J)*CX*V(I,J)/CO
A(1,4)=.25*GM1(I,J)*CX/CO
A(2,1)=-0.5/GAMMA(I,J)*U(I,J)*UN(I,J)+.5*R1*PHI2-CGEC*RKUU
A(2,2)=G11G*R1*U(I,J)+0.5/GAMMA(I,J)*UN(I,J)+.5*(CX+R1*R1T)
> /GAMMA(I,J)*CO-O.25*GM1(I,J)*U(I,J)/CO*RKUU
A(2,3)=0.5/GAMMA(I,J)*R2*U(I,J)-.5*GM1(I,J)*R1*V(I,J)+.5*R1T*R2
> /GAMMA(I,J)*CO-O.25*GM1(I,J)*V(I,J)/CO*RKUU
A(2,4)=.5*GM1(I,J)*R1+.25*GM1(I,J)*RKUU/CO
A(3,1)=-0.5/GAMMA(I,J)*V(I,J)*UN(I,J)+0.5*R2*PHI2-CGEC*RKVU
A(3,2)=0.5/GAMMA(I,J)*R1*V(I,J)-.5*GM1(I,J)*R2*U(I,J)+0.5*R1
> *R2T/GAMMA(I,J)*CO-O.25*GM1(I,J)*U(I,J)/CO*RKVU
A(3,3)=0.5/GAMMA(I,J)*UN(I,J)+G11G*R2*V(I,J)+(CX+R2T*R2)*.5
> /GAMMA(I,J)*CO-O.25*GM1(I,J)*V(I,J)/CO*RKVU
A(3,4)=.5*GM1(I,J)*R2+.25*GM1(I,J)*RKVU/CO
A(4,1)=G22M*UN(I,J)*U2V2-.5*GAMMA(I,J)*UN(I,J)*E(I,J)/RHO(I,J) +
> CX/GAMMA(I,J)*PHI2*CO-UN(I,J)**2*CO/GAMMA(I,J)/CX-.25
> *CX*ECR+RKU2*ERC
A(4,2)=-G22M*U(I,J)*UN(I,J)+.5*R1*GAMMA(I,J)*E(I,J)/RHO(I,J)
> -(GAMMA(I,J)+1.)*.5/GAMMA(I,J)*R1*PHI2-G34G*CX*U(I,J)
> *CO+R1T/GAMMA(I,J)*UN(I,J)*CO-RKU2*U(I,J)/CO
A(4,3)=-G22M*V(I,J)*UN(I,J)+.5*R2*GAMMA(I,J)*E(I,J)/RHO(I,J)
> -(GAMMA(I,J)+1.)*.5/GAMMA(I,J)*R2*PHI2-G34G*CX*V(I,J)
> *CO+R2T/GAMMA(I,J)*UN(I,J)*CC-RKU2*V(I,J)/CO
A(4,4)=.5*GAMMA(I,J)*UN(I,J)+.75*CX*CO+RKU2/CO
ELSE
A(1,1)=-.25*GM1(I,J)*CX*ERC
A(1,2)=G2M2*R1+.25*GM1(I,J)*CX*U(I,J)/CO
A(1,3)=G2M2*R2+.25*GM1(I,J)*CX*V(I,J)/CO
A(1,4)=-.25*GM1(I,J)*CX/CO
A(2,1)=-G2M2*U(I,J)*UN(I,J)+.5*R1*PHI2+CGEC*RKUU
A(2,2)=G23G*R1*U(I,J)+G2M2*UN(I,J)-.5*(CX+R1*R1T)/GAMMA(I,J)
> *CO+0.25*GM1(I,J)*U(I,J)/CO*RKUU
A(2,3)=G2M2*R2*U(I,J)-.5*GM1(I,J)*R1*V(I,J)-.5*R1T*R2
> /GAMMA(I,J)*CO+0.25*GM1(I,J)*V(I,J)/CO*RKUU
A(2,4)=.5*GM1(I,J)*R1-.25*GM1(I,J)*RKUU/CO
A(3,1)=-G2M2*V(I,J)*UN(I,J)+0.5*R2*PHI2+CGEC*RKVU
A(3,2)=G2M2*R1*V(I,J)-.5*GM1(I,J)*R2*U(I,J)-0.5*R1*R2T
> /GAMMA(I,J)*CO+0.25*GM1(I,J)*U(I,J)/CO*RKVU
A(3,3)=G2M2*UN(I,J)+G23G*R2*V(I,J)-(CX+R2T*R2)*.5/GAMMA(I,J)*CO+
> 0.25*GM1(I,J)*V(I,J)/CO*RKVU
A(3,4)=.5*GM1(I,J)*R2-.25*GM1(I,J)*RKVU/CO
A(4,1)=GM12*UN(I,J)*U2V2-.5*GAMMA(I,J)*UN(I,J)*E(I,J)
> /RHO(I,J)-CX/GAMMA(I,J)*PHI2*CO-UN(I,J)**2*CO/GAMMA(I,J)/CX+.25
> *CX*ECR-RKU2*ERC
A(4,2)=-GM12*U(I,J)*UN(I,J)+.5*R1*GAMMA(I,J)*E(I,J)/RHO(I,J)
> -GM1(I,J)*.5/GAMMA(I,J)*R1*PHI2+G34G*CX*U(I,J)*CO-R1T
> /GAMMA(I,J)*UN(I,J)*CO+RKU2*U(I,J)/CO
A(4,3)=-GM12*V(I,J)*UN(I,J)+.5*R2*GAMMA(I,J)*E(I,J)/RHO(I,J)

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>           -GM1(I,J)*.5/GAMMA(I,J)*R2*PHI2+G34G*CX*V(I,J)*CO-R2T
> /GAMMA(I,J)*UN(I,J)*CO+RKU2*V(I,J)/CO
A(4,4)=.5*GAMMA(I,J)*UN(I,J)-.75*CX*CO-RKU2/CO
ENDIF
RETURN
C*
C* VISCOUS TERM JACOBIAN MATRIX
C*
ENTRY VJACOB(A,B,C,I,J)
JP1=J+1
JM1=J-1
ZMUP=0.5*(ZMU(I,J)+ZMU(I,JP1))
ZMUM=0.5*(ZMU(I,J)+ZMU(I,JM1))
YYP =0.5*(Y(I,J)+Y(I,JP1))
YYM =0.5*(Y(I,J)+Y(I,JM1))
YJP =RJ(I,JP1)/Y(I,JP1)
IF(JM1.EQ.1)THEN
YJM=0.
ELSE
YJM =RJ(I,JM1)/Y(I,JM1)
ENDIF
IF(PRNT.EQ.0.DO)THEN
GAMP=0.5*(GAMMA(I,JP1)+GAMMA(I,J))
GAMM=0.5*(GAMMA(I,JM1)+GAMMA(I,J))
GKCPP=ZMUP*GAMP/PRN
GKCPM=ZMUM*GAMM/PRN
ELSE
ZMUTP = 0.5*(ZMUT(JP1)+ZMUT(J))
ZMUTM = 0.5*(ZMUT(JM1)+ZMUT(J))
ZMULP = ZMUP - ZMUTP
ZMULM = ZMUM - ZMUTM
GAMP=0.5*(GAMMA(I,JP1)+GAMMA(I,J))
GAMM=0.5*(GAMMA(I,JM1)+GAMMA(I,J))
GKCPP = GAMP*(ZMULP/PRN+ZMUTP/PRNT)
GKCPM = GAMM*(ZMULM/PRN+ZMUTM/PRNT)
ENDIF
EXJ=ETAX(I,J)/RJ(I,J)
EYJ=ETAY(I,J)/RJ(I,J)
ZMUU=ZMU(I,J)
OR=1./RHO(I,J)
ORP=1./RHO(I,JP1)
ORM=1./RHO(I,JM1)
ZMURP=ZMU(I,JP1)*ORP
ZMURM=ZMU(I,JM1)*ORM
UR =U(I,J)*OR
URP=U(I,JP1)*ORP
URM=U(I,JM1)*ORM
VR =V(I,J)*OR
VRM=V(I,JM1)*ORM
VRP=V(I,JP1)*ORP
UMRP=URP*ZMU(I,JP1)
UMRM=URM*ZMU(I,JM1)
VMRP=VRP*ZMU(I,JP1)
VMRM=VRM*ZMU(I,JM1)
U2R =UR*U(I,J)

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U2RP=URP*U(I,JP1)
U2RM=URM*U(I,JM1)
V2R =VR*V(I,J)
V2RP=VRP*V(I,JP1)
V2RM=VRM*V(I,JM1)
UVR =UR*V(I,J)
UVRP=URP*V(I,JP1)
UVRM=URM*V(I,JM1)
ER2 =E(I,J)*OR**2
ER2P=E(I,JP1)*ORP**2
ER2M=E(I,JM1)*ORM**2
ZRYJP=ZMURP*YJP
ZRYJM=ZMURM*YJM
ORYJP=ORP*YJP
ORYJM=ORM*YJM
VMRP=-ZMURP*V(I,JP1)*YJP
VMRM=-ZMURM*V(I,JM1)*YJM
URYJP=-URP*YJP
URYJM=-URM*YJM
VYJP=2.*ZMU(I,JP1)*VRP*YJP
VYJM=2.*ZMU(I,JM1)*VRM*YJM
V2YJP=-V2RP*2.*ZMU(I,JP1)*YJP
V2YJM=-V2RM*2.*ZMU(I,JM1)*YJM
UVYJP=-2.*ZMU(I,JP1)*UVRP*YJP
UVYJM=-2.*ZMU(I,JM1)*UVRM*YJM
VYJP2=VYJP*0.5
VYJM2=0.5*VYJM
UYJP=ZMU(I,JP1)*URP*YJP
UYJM=ZMU(I,JM1)*URM*YJM
AAP1= ZMUP*A1(I,J)*YYP
AAP2= ZMUP*A2(I,J)*YYP
AAP3= ZMUP*A3(I,J)*YYP
AAF4= GKCPP*A4(I,J)*YYP
AAM1= ZMUM*A1(I,JM1)*YYM
AAM2= ZMUM*A2(I,JM1)*YYM
AAM3 =ZMUM*A3(I,JM1)*YYM
AAM4 =GKCPM*A4(I,JM1)*YYM
IF (JM1.EQ.1) THEN
  CALL SZERO(4,A)
ELSE
  A(1,1) =0.
  A(1,2) =0.
  A(1,3) =0.
  A(1,4) =0.
  A21=(AAM1*URM+AAM2*VRM)*RJ(I,JM1)/Y(I,JM1)
  A(2,1) =A21-1./3.*EXJ*VMRM
  A(2,2) =-AAM1*ORM*RJ(I,JM1)/Y(I,JM1)
  A(2,3) =-AAM2*ORM*RJ(I,JM1)/Y(I,JM1)-1./3.*EXJ*ZRYJM
  A(2,4) =0.
  A31=(AAM2*URM+AAM3*VRM)*RJ(I,JM1)/Y(I,JM1)
  A(3,1) =A31+1./3.*ZMU(I,J)
  *          *EXJ*URYJM
  A(3,2) =-AAM2*ORM*RJ(I,JM1)/Y(I,JM1)+1./3.*ZMU(I,J)*EXJ*ORYJM
  A(3,3) =-AAM3*ORM*RJ(I,JM1)/Y(I,JM1)
  A(3,4) =0.

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FILE: PNSVIS FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STA

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A(4,1) =(-AAM4*(-ER2M+U2RM+V2RM)+AAM1*U2RM+AAM3*V2RM+
+      2.*AAM2*UVRM)*RJ(I,JM1)/Y(I,JM1)-
+      1./3.*EYJ*V2YJM-1./3.*EXJ*UVYJM
A(4,2) =AAM4*URM*RJ(I,JM1)/Y(I,JM1)-A21-1./3.*EXJ*VYJM2
A(4,3) =AAM4*VRM*RJ(I,JM1)/Y(I,JM1)-A31-1./3.*EYJ*VYJM-
*      1./3.*EXJ*UYJM
A(4,4) =-AAM4*ORM*RJ(I,JM1)/Y(I,JM1)
ENDIF
C(1,1) =0.
C(1,2) =0.
C(1,3) =0.
C(1,4) =0.
C21=(AAP1*URP+AAP2*VRP)*RJ(I,JP1)/Y(I,JP1)
C(2,1) =C21+1./3.*EXJ*VMRP
C(2,2) =-AAP1*ORP*RJ(I,JP1)/Y(I,JP1)
C(2,3) =-AAP2*ORP*RJ(I,JP1)/Y(I,JP1)+1./3.*EXJ*ZRYJP
C(2,4) =0.
C31=(AAP2*URP+AAP3*VRP)*RJ(I,JP1)/Y(I,JP1)
C(3,1) =C31-1./3.*ZMU(I,J)
*      *EXJ*URYJP
C(3,2) =-AAP2*ORP*RJ(I,JP1)/Y(I,JP1)-1./3.*ZMU(I,J)*EXJ*ORYJP
C(3,3) =-AAP3*ORP*RJ(I,JP1)/Y(I,JP1)
C(3,4) =0.
C(4,1) =(-AAP4*(-ER2P+U2RP+V2RP)+AAP1*U2RP+AAP3*V2RP+
+      2.*AAP2*UVRP)*RJ(I,JP1)/Y(I,JP1)-
+      1./3.*EYJ*V2YJP+1./3.*EXJ*UVYJP
C(4,2) =AAP4*URP*RJ(I,JP1)/Y(I,JP1)-C21+1./3.*EXJ*VYJP2
C(4,3) =AAP4*VRP*RJ(I,JP1)/Y(I,JP1)-C31+1./3.*EYJ*VYJP-
+      1./3.*EXJ*UYJP
C(4,4) =-AAP4*ORP*RJ(I,JP1)/Y(I,JP1)
AA1 =AAP1+AAM1
AA2 =AAP2+AAM2
AA3 =AAP3+AAM3
AA4 =AAP4+AAM4
B(1,1) =0.
B(1,2) =0.
B(1,3) =0.
B(1,4) =0.
B(2,1) =(-AA1*UR-AA2*VR)*RJ(I,J)/Y(I,J)
B(2,2) =AA1*OR*RJ(I,J)/Y(I,J)
B(2,3) =AA2*OR*RJ(I,J)/Y(I,J)
B(2,4) =0.
B(3,1) =(-AA2*UR-AA3*VR)*RJ(I,J)/Y(I,J)
B(3,2) =AA2*OR*RJ(I,J)/Y(I,J)
B(3,3) =AA3*OR*RJ(I,J)/Y(I,J)
B(3,4) =0.
B(4,1) =(AA4*(-ER2+U2R+V2R)-AA1*U2R-AA3*V2R-
*      2.*AA2*UVR)*RJ(I,J)/Y(I,J)
B(4,2) =-AA4*UR*RJ(I,J)/Y(I,J)-B(2,1)
B(4,3) =-AA4*VR*RJ(I,J)/Y(I,J)-B(3,1)
B(4,4) =AA4*OR*RJ(I,J)/Y(I,J)
RETURN
END
```

C-----
SUBROUTINE EIGMTX

```

C*
C* SUBROUTINE FOR EIGENVECTOR MATRIX CALCULATION
C* IF IA=1 L FOR ACAP
C* IF IA=2 L FOR BCAP
C*
C*****IMPLICIT REAL*8(A-H,O-Z)
C*****PARAMETER (IZ=150,JZ=80)
C*****COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
C*****P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
C*****COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
C*****ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
C*****AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
C*****COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
C*****CFL1,PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF
C*****BIOT,TW1
C*****COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
C*****COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
C*****IWBC,IFLOW
C*****DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
C*****EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
C*****      (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****DIMENSION A(4,4)
C*****ENTRY EIGEN(IA,A,I,J)
C*****IF(IA.EQ.2)GO TO 10
C*****CX=SAIX(I,J)
C*****CY=SAIY(I,J)
C*****GO TO 20
10 CX=ETAX(I,J)
CY=ETAY(I,J)
20 CONTINUE
SQ2=DSQRT(2.D0)
C=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
C1=CX/DSQRT(CX**2+CY**2)
C2=CY/DSQRT(CX**2+CY**2)
A(1,1)=1.-0.5*GM1(I,J)*(U(I,J)**2+V(I,J)**2)/C**2
A(1,2)=GM1(I,J)*U(I,J)/C**2
A(1,3)=GM1(I,J)*V(I,J)/C**2
A(1,4)=-GM1(I,J)/C**2
A(2,1)=(-C2*U(I,J)+C1*V(I,J))/RHO(I,J)
A(2,2)=C2/RHO(I,J)
A(2,3)=-C1/RHO(I,J)
A(2,4)=0.
A(3,1)=-(C1*U(I,J)+C2*V(I,J))/SQ2/RHO(I,J) +
          0.5/SQ2*GM1(I,J)*(U(I,J)**2+V(I,J)**2)/RHO(I,J)/C
A(3,2)=C1/SQ2/RHO(I,J)-GM1(I,J)/SQ2*U(I,J)/RHO(I,J)/C
A(3,3)=C2/SQ2/RHO(I,J)-GM1(I,J)/SQ2*V(I,J)/RHO(I,J)/C
A(3,4)=GM1(I,J)/SQ2/RHO(I,J)/C
A(4,1)=(C1*U(I,J)+C2*V(I,J))/SQ2/RHO(I,J)+0.5/SQ2*GM1(I,J)*
          (U(I,J)**2+V(I,J)**2)/RHO(I,J)/C
A(4,2)=-C1/SQ2/RHO(I,J)-GM1(I,J)/SQ2*U(I,J)/RHO(I,J)/C
A(4,3)=-C2/SQ2/RHO(I,J)-GM1(I,J)/SQ2*V(I,J)/RHO(I,J)/C
A(4,4)=GM1(I,J)/SQ2/RHO(I,J)/C

```

```

      RETURN
C*
C* LEFT & RIGHT EIGENMATRIX FOR XI DIRECTION
C*
      ENTRY EIGAR(A,I,J)
      CX=SAIX(I,J)
      CY=SAIY(I,J)
      SQ2=1./DSQRT(2.D0)
      C=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
      CXCY=1./DSQRT(CX**2+CY**2)
      C1=CX*CXY
      C2=CY*CXY
      A(1,1)=1.
      A(1,2)=0.
      A(1,3)=RHO(I,J)*SQ2/C
      A(1,4)=A(1,3)
      A(2,1)=U(I,J)
      A(2,2)=RHO(I,J)*C2
      A(2,3)=SQ2*RHO(I,J)*(U(I,J)/C+C1)
      A(2,4)=SQ2*RHO(I,J)*(U(I,J)/C-C1)
      A(3,1)=V(I,J)
      A(3,2)=-RHO(I,J)*C1
      A(3,3)=SQ2*RHO(I,J)*(V(I,J)/C+C2)
      A(3,4)=SQ2*RHO(I,J)*(V(I,J)/C-C2)
      A(4,1)=0.5*(U(I,J)**2+V(I,J)**2)
      A(4,2)=RHO(I,J)*(U(I,J)*C2-V(I,J)*C1)
      TEMP=0.5*SQ2*RHO(I,J)*(U(I,J)**2+V(I,J)**2)/C
      +           +RHO(I,J)*SQ2*C/GM1(I,J)
      RUC=SQ2*RHO(I,J)*(U(I,J)*C1+V(I,J)*C2)
      A(4,3)=TEMP+RUC
      A(4,4)=TEMP-RUC
      RETURN
      END

C-----  

C-----  

      SUBROUTINE COEFY(I)
C*
C*   SETTING COEFFICIENTS FOR LY-OPERATOR
C*
*****  

      IMPLICIT REAL*8(A-H,O-Z)
      PARAMETER (IZ=150,JZ=80)
      COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),E(IZ,JZ,4),G(IZ,JZ,4),
      >          P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
      COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
      >          ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
      >          ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
      COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
      >CFL1,PRNT,PB,RM1,SUM(4),ZMU0,REN,PRN,TWALL,TREF
      >,BIOT,TW1
      COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
      COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
      >          ,IWBC,IFLOW
      DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
      EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),

```

```

>          (Q(1,1,3),RH0V(1,1)),(Q(1,1,4),E(1,1))
C*****DIMENSION AM(4,4,JZ),BM(4,4,JZ),CM(4,4,JZ),DM(4,JZ)
C*****DIMENSION DTEMP(4),ISUB(JZ)
C*****DIMENSION B(4,4),BL1(4,4),D(4,4),A(4,4),AJM(4,4)
CHOIBEGIN
    DIMENSION AMIL1(4,4),BMIL1(4,4),CMIL1(4,4),DMIL1(4)
    DIMENSION BJ2(4,4),BJ1(4,4),DD(4,4)
    DIMENSION AMIL(4,4),BMIL(4,4),CMIL(4,4),DMIL(4)
    DIMENSION AMINV(4,4)
    DIMENSION AB1(4,4),AB2(4,4),AB3(4,4),AB4(4,4)
    DIMENSION D1(4),D2(4),D3(4),D4(4)
CHOIEND
    DATA ISUB/JZ*0/
C*****C* CHECK THE SONIC POINT AT DOWNSTREAM END
C* IF(IVISC.NE.1)GOTO 15
    IF(I.NE.IL)GOTO 15
    DO 5 J=1,JL
        CO=DSQRT(GAMMA(I,J)*P(I,J)/RHO(I,J))
        CONTRA=UN(I,J)-DSQRT(SAIX(I,J)**2+SAIY(I,J)**2)*CO
        IF(CONTRA.LT.0.DO)THEN
            ISUB(J)=1
        ELSE
            ISUB(J)=0
        ENDIF
        IF(UN(I,J).LT.0.DO)ISUB(J)=2
        IF(FB.EQ.0.DO)ISUB(J)=0
        IF(NADV.EQ.1)ISUB(J)=0
5     CONTINUE
15    CONTINUE
C*
C* ON THE CENTER LINE OF THE NOZZLE AT J=1
C*
J=1
CALL SZERO(4,AM(1,1,J))
CALL SZERO(4,BM(1,1,J))
DO 20 M=1,4
    DM(M,J)=0.
    BM(M,M,J)=BM(M,M,J)+1.0
20    CONTINUE
    CALL SZERO(4,CM(1,1,J))
C*
C* INTERIOR NODS
C*
DO 80 J=2,JL1
    TAUD=0.5DO*DELTAU(I,J)*THETA/EYI
    TAUD2=2.*TAUD
    JM1=J-1
    JP1=J+1
    CALL JACOB(2,B,I,JM1)
    CALL SMM(4,-TAUD,B,AM(1,1,J))
    CALL SZERO(4,BM(1,1,J))
    DO 60 M=1,4
60    BM(M,M,J)=BM(M,M,J)+1.

```

```

IF(I.EQ.II.AND.ISUB(J).NE.0)THEN
  CALL AJACOB(1,A,I,J)
  CALL SZERO(4,AJM)
ELSE
  CALL TRUEJ(1,A,I,J)
  CALL TRUEJ(2,AJM,I,J)
ENDIF
CALL DHDQ(D,I,J)
DO 65 M=1,4
DO 65 N=1,4
  BM(M,N,J)=BM(M,N,J)-TAUD2*(D(M,N)-A(M,N)+AJM(M,N))
  IF(I.NE.2.AND.I.LT.II1)BM(M,N,J)=BM(M,N,J)+NORD*TAUD*
*      (A(M,N)-AJM(M,N))
65 CONTINUE
  CALL JACOB(2,B,I,JP1)
  CALL SMM(4,TAUD,B,CM(1,1,J))

C*
C*  INSERT VISCOUS JACOBIAN LHS HERE
C*
  IF(IVISC.EQ.1)THEN
    CALL VJACOB(A,B,D,I,J)
    DO 68 M=1,4
    DO 68 N=1,4
      AM(M,N,J)=AM(M,N,J)+DELTAU(I,J)*A(M,N)
      BM(M,N,J)=BM(M,N,J)+DELTAU(I,J)*B(M,N)
    68 CM(M,N,J)=CM(M,N,J)+DELTAU(I,J)*D(M,N)
    ELSE
    END IF
    DO 70 K=1,4
  70 DM(K,J)=DQ(I,J,K)

C  SUBSONIC REGION KEEP BACK PRESSURE
C
  IF(IVISC.EQ.1.AND.(I.EQ.II.AND.ISUB(J).EQ.1))THEN
    CALL EIGEN(1,BL1,I,J)
    DO 72 K=1,4
  72 BL1(4,K)=0.
    CALL MMM(4,BL1,AM(1,1,J),A)
    CALL MMM(4,BL1,BM(1,1,J),B)
    CALL MMM(4,BL1,CM(1,1,J),D)
    DO 74 M=1,4
    DO 74 N=1,4
      AM(M,N,J)=A(M,N)
      BM(M,N,J)=B(M,N)
    74 CM(M,N,J)=D(M,N)
    DO 76 M=1,4
    DTEMP(M)=0.
    DO 76 K=1,4
    DTEMP(M)=DTEMP(M)+BL1(M,K)*DM(K,J)
  76 CONTINUE
    DO 78 M=1,4
  78 DM(M,J)=DTEMP(M)
    BM(4,1,J)=0.5*GM1(I,J)*(U(I,J)**2+V(I,J)**2)/Y(I,J)
    BM(4,2,J)=-GM1(I,J)*U(I,J)/Y(I,J)
    BM(4,3,J)=-GM1(I,J)*V(I,J)/Y(I,J)

```

```

BM(4,4,J)=GM1(I,J)/Y(I,J)
1F(PB.NE.0.DO)THEN
DM(4,J)=(PB-P(I,J))/RJ(I,J)
ELSE
DM(4,J)=0.
ENDIF
ELSE
END IF

```

```

C
C REVERSE FLOW REGION
C
IF(IVISCR.EQ.1.AND.(I.EQ.IL.AND.ISUB(J).EQ.2))THEN
CALL EIGEN(1,BL1,I,J)
DO 73 K=1,4
BL1(1,K)=0.
BL1(2,K)=0.
73 BL1(4,K)=0.
CALL MMM(4,BL1,AM(1,1,J),A)
CALL MMM(4,BL1,BM(1,1,J),B)
CALL MMM(4,BL1,CM(1,1,J),D)
DO 75 M=1,4
DO 75 N=1,4
AM(M,N,J)=A(M,N)
BM(M,N,J)=B(M,N)
75 CM(M,N,J)=D(M,N)
DO 77 M=1,4
DTEMP(M)=0.
DO 77 K=1,4
DTEMP(M)=DTEMP(M)+BL1(M,K)*DM(K,J)
77 CONTINUE
DO 79 M=1,4
79 DM(M,J)=DTEMP(M)
RJYY=RJ(I,J)/Y(I,J)
RCV=RHO(I,J)*CV(I,J)
RJRCV=RJYY/RCV
BM(1,1,J)=(-E(I,J)/RHO(I,J)+GM1(I,J)/GAMMA(I,J)*(U(I,J)**2
> +V(I,J)**2))*RJRCV
BM(1,2,J)=-GM1(I,J)/GAMMA(I,J)*U(I,J)*RJRCV
BM(1,3,J)=-GM1(I,J)/GAMMA(I,J)*V(I,J)*RJRCV
BM(1,4,J)=RJRCV
C1=(RHO(I,J)*E(I,J)-0.5*RHO(I,J)**2*(U(I,J)**2+V(I,J)**2))
C2=(RHO(I,J)*E(I,J)-0.5*GM1(I,J)/GAMMA(I,J)*RHO(I,J)**2*(U(I,J)**2
> +V(I,J)**2))
C3=(C2/C1)**(GAMMA(I,J)/GM1(I,J))
C4=GAMMA(I,J)/GM1(I,J)/C1*(C2/C1)**(1.D0/GM1(I,J))
BM(2,1,J)=(0.5*(U(I,J)**2+V(I,J)**2)*C3+C4*E(I,J)*(C1-C2)/RHO(I,J)
> )*GM1(I,J)*RJYY
BM(2,2,J)=(-U(I,J)*C3+C4*U(I,J)*(C2-GM1(I,J)/GAMMA(I,J)*C1))
> *GM1(I,J)*RJYY
BM(2,3,J)=(-V(I,J)*C3+C4*V(I,J)*(C2-GM1(I,J)/GAMMA(I,J)*C1))
> *GM1(I,J)*RJYY
BM(2,4,J)=(C3+C4*(C1-C2))*GM1(I,J)*RJYY
BM(4,1,J)=-VN(I,J)*RJYY/RHO(I,J)
BM(4,2,J)=ETAX(I,J)*RJYY/RHO(I,J)
BM(4,3,J)=ETAY(I,J)*RJYY/RHO(I,J)

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```
BM(4,4,J)=0.
TON=(E(I,J)/RHO(I,J)-0.5*GM1(I,J)/GAMMA(I,J)*(U(I,J)**2
> +V(I,J)**2))/CV(I,J)
TT =(E(I,J)/RHO(I,J)-0.5*(U(I,J)**2+V(I,J)**2))/CV(I,J)
PON=P(I,J)*(TON/TT)**(GAMMA(I,J)/GM1(I,J))
DM(1,J)=(TWALL-TON)
DM(2,J)=(PB-PON)
DM(4,J)=-VN(I,J)
END IF

C
CHOI
CHOI
    IF(IVISC.EQ.0.AND.J.EQ.JL1) GOTO 8001
    GO TO 80
8001 DO 8002 M=1,4
    DO 8002 N=1,4
        AMIL1(M,N)=AM(M,N,JL1)
8002 CONTINUE
    DO 8003 M=1,4
    DO 8003 N=1,4
        BMIL1(M,N)=BM(M,N,JL1)
8003 CONTINUE
    DO 8004 M=1,4
    DO 8004 N=1,4
        CMIL1(M,N)=CM(M,N,JL1)
8004 CONTINUE
    DO 8005 M=1,4
        DMIL1(M)=DM(M,JL1)
8005 CONTINUE
CHOI
CHOI
    80 CONTINUE
C*
C* WALL BOUNDARY CONDITION
C*
CHOI      J=JL
CHOI      TAUD=THETA*DELTAU(I,J)/EYI
CHOI      IF(IVISC.EQ.1)GOTO 111
CHOI      CALL SZERO(4,AM(1,1,J))
CHOI      CALL JACOB(2,B,I,J-1)
CHOI      CALL AJACOB(1,A,I,J)
CHOI      CALL AJACOB(2,AJM,I,J)
CHOI      CALL EIGEN(2,BL1,I,J)
CHOI      DO 90 M=1,3
CHOI      DO 90 N=1,4
CHOI      DO 90 K=1,4
CHOI 90  AM(M,N,J)=AM(M,N,J)-TAUD*BL1(M,K)*B(K,N)
CHOI      CALL SZERO(4,BM(1,1,J))
CHOI      CALL JACOB(2,B,I,J)
CHOI      CALL DHDQ(D,I,J)
CHOI      DO 100 M=1,3
CHOI      DO 100 N=1,4
CHOI      BM(M,N,J)=BM(M,N,J)+BL1(M,N)
CHOI      DO 100 K=1,4
CHOI      BM(M,N,J)=BM(M,N,J)+TAUD*BL1(M,K)*(B(K,N)+A(K,N)-D(K,N)-AJM(K,N))
```

```

CHOI      IF(I.NE.2.AND.I.LT.II1) BM(M,N,J)=BM(M,N,J)+NORD*0.5*TAUD*
CHOI      *     BL1(M,K)*(A(K,N)-AJM(K,N))
CHOI 100  CONTINUE
CHOI
CHOIBEG
J=JL
TAUD=THETA*DELTAU(I,J)/EYI
IF(IVISC.EQ.1) GOTO 111
CALL JACOB(2,BJ2,I,J-2)
CALL JACOB(2,BJ1,I,J-1)
CALL JACOB(2,B,I,J)
CALL AJACOB(1,A,I,J)
CALL AJACOB(2,AJM,I,J)
CALL EIGEN(2,BL1,I,J)
DO 899 N=1,4
899 BL1(4,N)=0.D0
CALL HJAC(DD,J)
DO 90 M=1,4
DO 90 N=1,4
AMIL(M,N)=0.5D0*BJ2(M,N)*TAUD
90 CONTINUE
DO 91 M=1,4
DO 91 N=1,4
BMIL(M,N)=-2.D0*BJ1(M,N)*TAUD
91 CONTINUE
CALL JACOB(2,B,I,J)
CALL DHDQ(D,I,J)
DO 100 M=1,4
DO 100 N=1,4
CMIL(M,N)=DD(M,N)+TAUD*(1.5D0*B(M,N)+A(M,N)-D(M,N)-AJM(M,N))
IF(I.NE.2.AND.I.LT.II1) CMIL(M,N)=CMIL(M,N)+NORD*0.5D0*TAUD*
> (A(M,N)-AJM(M,N))
100 CONTINUE
DO 1001 M=1,4
1001 DMIL(M)=DQ(I,JL,M)
C DO 2001 M=1,4
CC WRITE(6,2002) I,(AMIL1(M,N),N=1,4)
C2001 CONTINUE
C2002 FORMAT(2X,I5,2X,4D14.5)
CALL INVER(4,AMIL1,AMINV)
CALL MMM(4,AMINV,BMIL1,AB1)
CALL MMM(4,AMIL,AB1,AB2)
DO 101 M=1,4
DO 101 N=1,4
101 AB3(M,N)=AB2(M,N)-BMIL(M,N)
CALL MMM(4,BL1,AB3,AB4)
DO 102 M=1,4
DO 102 N=1,4
102 AM(M,N,J)=AB4(M,N)
CALL MMM(4,AMINV,CMIL1,AB1)
CALL MMM(4,AMIL,AB1,AB2)
DO 103 M=1,4
DO 103 N=1,4
103 AB3(M,N)=AB2(M,N)-CMIL(M,N)
CALL MMM(4,BL1,AB3,AB4)

```

```

DO 104 M=1,4
DO 104 N=1,4
104 BM(M,N,J)=AB4(M,N)
CALL MMV(4,AMINV,DMIL1,D1)
CALL MMV(4,AMIL,D1,D2)
DO 105 M=1,4
105 D3(M)=D2(M)-DMIL(M)
CALL MMV(4,BL1,D3,D4)
DO 106 M=1,4
106 DM(M,J)=D4(M)
CHOI
CHOIEND
      BM(4,1,J)=-VN(I,J)
      BM(4,2,J)=ETAX(I,J)
      BM(4,3,J)=ETAY(I,J)
      BM(4,4,J)=0.
      CALL SZERO(4,CM(1,1,J))
CHOI      DO 110 M=1,3
CHOI      DM(M,J)=0.
CHOI      DO 110 K=1,4
CHOI      DM(M,J)=DM(M,J)+BL1(M,K)*DQ(I,J,K)
CHOI 110 CONTINUE
C      WRITE(6,*) I,J,BM(4,1,J)
      DM(4,J)=0.
      GOTO 119
111  CONTINUE
      CALL SZERO(4,AM(1,1,J))
      CALL SZERO(4,CM(1,1,J))
      CALL SZERO(4,BM(1,1,J))
      DO 112 M=1,4
      DM(M,J)=0.
112  BM(M,M,J)=1.0
      IF(IWBC.EQ.1)THEN
      OR=1./RHO(I,J)
      ORCV=OR/CV(I,J)
      U2V2=U(I,J)**2+V(I,J)**2
      U2V21=U(I,JL1)**2+V(I,JL1)**2
      YJJL=RJ(I,JL)/Y(I,JL)
      YJJL1=RJ(I,JL1)/Y(I,JL1)
      BM(1,1,J)=(-E(I,J)*OR+U2V2)*YJJL*ORCV
      BM(1,2,J)=-U(I,J)*YJJL*ORCV
      BM(1,3,J)=-V(I,J)*YJJL*ORCV
      BM(1,4,J)=YJJL*ORCV
      BM(2,1,J)=0.
      BM(2,2,J)=YJJL
      BM(2,3,J)=0.
      BM(2,4,J)=0.
      BM(3,1,J)=0.
      BM(3,3,J)=YJJL
      BM(3,4,J)=0.
      C1=SAIX(I,J)*ETAX(I,J)+SAIY(I,J)*ETAY(I,J)
      C2=ETAX(I,J)**2+ETAY(I,J)**2
      CB=C1+C2
      IF(I.GT.2) CB=CB+0.5*FLOAT(NORD)*C1
      CD=C1*P(I-1,J)

```

```

IF(I.GT.2) CD=CD+NORD*C1*(P(I-1,J)-0.5*P(I-2,J))
BM(4,1,J)=0.5*U2V2*YJJL*GM1(I,J)*CB
BM(4,2,J)=-U(I,J)*YJJL*GM1(I,J)*CB
BM(4,3,J)=-V(I,J)*YJJL*GM1(I,J)*CB
BM(4,4,J)=YJJL*GM1(I,J)*CB
AM(4,1,J)=-0.5*U2V21*YJJL1*GM1(I,J)*C2
AM(4,2,J)=U(I,J-1)*YJJL1*GM1(I,J)*C2
AM(4,3,J)=V(I,J-1)*YJJL1*GM1(I,J)*C2
AM(4,4,J)=-YJJL1*GM1(I,J)*C2
DO 113 M=1,3
113 DM(M,J)=0.
TJJ=P(I,J)/RHO(I,J)/RGAS
DM(1,J)=TWALL-TJJ
DM(4,J)=CD+C2*P(I,JL1)-CB*P(I,JL)
C
C ADIABATIC WALL
C
IF(IWALL.EQ.0)THEN
ORCV=1./RHO(I,J)/CV(I,J)
ORCV1=1./RHO(I,J-1)/CV(I,J-1)
RUU=RGAS
TIM1=P(I-1,J)/RHO(I-1,J)/RUU
CD=C1*TIM1
IF(I.GT.2) THEN
TIM2=P(I-2,J)/RHO(I-2,J)/RUU
CD=CD+NORD*C1*(TIM1-0.5*TIM2)
ENDIF
BM(1,1,J)=(-E(I,J)*OR+U2V2)*YJJL*ORCV*CB
BM(1,2,J)=-U(I,J)*YJJL*ORCV*CB
BM(1,3,J)=-V(I,J)*YJJL*ORCV*CB
BM(1,4,J)=YJJL*ORCV*CB
AM(1,1,J)=-(-E(I,J-1)*OR+U2V21)*YJJL1*ORCV1*C2
AM(1,2,J)=U(I,J-1)*YJJL1*ORCV1*C2
AM(1,3,J)=V(I,J-1)*YJJL1*ORCV1*C2
AM(1,4,J)=-YJJL1*ORCV1*C2
TJM1=P(I,J-1)/RHO(I,J-1)/RUU
TJJ=P(I,J)/RHO(I,J)/RUU
DM(1,J)=CD+C2*TJM1-CB*TJJ
ENDIF
C
C WALL COOLING (FROM UPSTREAM TO DOWNSTREAM
C
IF(IWALL.EQ.2.AND.IFLOW.EQ.1)THEN
C1=C1/RJ(I,J)
C2=C2/RJ(I,J)
C3=BIOT/Y(I,J)
CB=C1+C2+C3
IF(I.GT.2) CB=CB+0.5*FLCAT(NORD)*(C1+C3)
ORCV=1./RHO(I,J)/CV(I,J)
ORCV1=1./RHO(I,J-1)/CV(I,J-1)
RUU=RGAS
TIM1=P(I-1,J)/RHO(I-1,J)/RUU
CD=(C1+C3)*TIM1
IF(I.GT.2) THEN
TIM2=P(I-2,J)/RHO(I-2,J)/RUU

```

```

CD=CD+NORD*(C1+C3)*(TIM1-0.5*TIM2)
ENDIF
BM(1,1,J)=(-E(I,J)*OR+U2V2)*YJJL*ORCV*CB
BM(1,2,J)=-U(I,J)*YJJL*ORCV*CB
BM(1,3,J)=-V(I,J)*YJJL*ORCV*CB
BM(1,4,J)=YJJL*ORCV*CB
AM(1,1,J)=-(-E(I,J-1)*OR+U2V21)*YJJL1*ORCV1*C2
AM(1,2,J)=U(I,J-1)*YJJL1*ORCV1*C2
AM(1,3,J)=V(I,J-1)*YJJL1*ORCV1*C2
AM(1,4,J)=-YJJL1*ORCV1*C2
TJM1=P(I,J-1)/RHO(I,J-1)/RUU
TJJ=P(I,J)/RHO(I,J)/RUU
DM(1,J)=CD+C2*TJM1-CB*TJJ
ENDIF

C   INVERSE COOLING FLOW
C
IF(IWALL.EQ.2.AND.IFLOW.EQ.-1)THEN
  IF(I.EQ.IL)THEN
    DM(1,J)= TW1-TJJ
    GOTO 119
  ENDIF
  C1=C1/RJ(I,J)
  C2=C2/RJ(I,J)
  C3=-BIOT/Y(I,J)
  CB=C2-(C1+C3)
  IF(I.LT.IL1) CB=CB-0.5*FLOAT(NORD)*(C1+C3)
  ORCV=1./RHO(I,J)/CV(I,J)
  ORCV1=1./RHO(I,J-1)/CV(I,J-1)
  RUU=RGAS
  TIM1=P(I+1,J)/RHO(I+1,J)/RUU
  CD=-(C1+C3)*TIM1
  IF(I.LT.IL1) THEN
    TIM2=P(I+2,J)/RHO(I+2,J)/RUU
    CD=CD+NORD*(C1+C3)*(-TIM1+0.5*TIM2)
  ENDIF
  BM(1,1,J)=(-E(I,J)*OR+U2V2)*YJJL*ORCV*CB
  BM(1,2,J)=-U(I,J)*YJJL*ORCV*CB
  BM(1,3,J)=-V(I,J)*YJJL*ORCV*CB
  BM(1,4,J)=YJJL*ORCV*CB
  AM(1,1,J)=-(-E(I,J-1)*OR+U2V21)*YJJL1*ORCV1*C2
  AM(1,2,J)=U(I,J-1)*YJJL1*ORCV1*C2
  AM(1,3,J)=V(I,J-1)*YJJL1*ORCV1*C2
  AM(1,4,J)=-YJJL1*ORCV1*C2
  TJM1=P(I,J-1)/RHO(I,J-1)/RUU
  TJJ=P(I,J)/RHO(I,J)/RUU
  DM(1,J)=CD+C2*TJM1-CB*TJJ
ENDIF

C
ENDIF
119  CONTINUE
C*
C* SOLVE 4*4 BLOCK TRIDIAGONAL MATRICS
C*
CALL NBTRIP(AM,BM,CM,DM,1,JL,4)

```

```

DO 120 J=1,JL
DO 120 K=1,4
DQ(I,J,K)=DM(K,J)
120 CONTINUE
RETURN
END
C-----
C----- SUBROUTINE FLUXCL
C*
C* SUBROUTINE FOR FLUX VECTOR CALCULATION
C*
C***** IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=80)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
> P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
> ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
> ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
> CFL1,PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF
>,BIOT,TW1
COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
> ,IWBC,IFLOW
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C***** DIMENSION A(4,4)
ENTRY FLUX(II)
I=II
C*
C* COMPUTE CONVECTIVE TERMS
C*
DO 10 J=1,JL
C F(I,J,1)=RHO(I,J)*UN(I,J)/RJ(I,J)*Y(I,J)
C F(I,J,2)=(-OU(I,J)*UN(I,J)+SAIX(I,J)*P(I,J))/RJ(I,J)*Y(I,J)
C F(I,J,3)=(RHOV(I,J)*UN(I,J)+SAIY(I,J)*P(I,J))/RJ(I,J)*Y(I,J)
C F(I,J,4)=(E(I,J)+P(I,J))*UN(I,J)/RJ(I,J)*Y(I,J)
CALL AJACOB(1,A,I,J)
DO 3 K=1,4
F(I,J,K)=0.
DO 3 JJ=1,4
3 F(I,J,K)=F(I,J,K)+A(K,JJ)*Q(I,J,JJ)*Y(I,J)/RJ(I,J)
G(I,J,1)=RHO(I,J)*VN(I,J)/RJ(I,J)*Y(I,J)
G(I,J,2)=(RHOU(I,J)*VN(I,J)+ETAX(I,J)*P(I,J))/RJ(I,J)*Y(I,J)
G(I,J,3)=(RHOV(I,J)*VN(I,J)+ETAY(I,J)*P(I,J))/RJ(I,J)*Y(I,J)
G(I,J,4)=(E(I,J)+P(I,J))*VN(I,J)/RJ(I,J)*Y(I,J)
10 CONTINUE
RETURN
C*
C* E MINUS FLUX VECTOR
C*
ENTRY FLUXM(II)

```

```

I=II
DO 20 J=1,JL
CALL AJACOB(2,A,I,J)
DO 17 K=1,4
G(I,J,K)=0.
DO 17 JJ=1,4
17 G(I,J,K)=G(I,J,K)+A(K,JJ)*Q(I,J,JJ)/RJ(I,J)*Y(I,J)
20 CONTINUE
RETURN

C*
C* VISCOUS FLUX VECTOR
C*
ENTRY VFLUX(II)
I=II
DO 30 J=2,JL1
JP1=J+1
JM1=J-1
ZMUP=0.5*(ZMU(I,J)+ZMU(I,JP1))
ZMUM=0.5*(ZMU(I,J)+ZMU(I,JM1))
IF(PRNT.EQ.0.DO)THEN
GAMP=0.5*(GAMMA(I,JP1)+GAMMA(I,J))
GAMM=0.5*(GAMMA(I,JM1)+GAMMA(I,J))
GKCPP=ZMUP*GAMP/PRN
GKCPM=ZMUM*GAMM/PRN
ELSE
ZMUTP = 0.5*(ZMUT(JP1)+ZMUT(J))
ZMUTM = 0.5*(ZMUT(JM1)+ZMUT(J))
ZMULP = ZMUP - ZMUTP
ZMULM = ZMUM - ZMUTM
GAMP=0.5*(GAMMA(I,JP1)+GAMMA(I,J))
GAMM=0.5*(GAMMA(I,JM1)+GAMMA(I,J))
GKCPP = GAMP*(ZMULP/PRN+ZMUTP/PRNT)
GKCPM = GAMM*(ZMULM/PRN+ZMUTM/PRNT)
ENDIF
YYP=0.5*(Y(I,J)+Y(I,JP1))
YYM=0.5*(Y(I,J)+Y(I,JM1))
YZP=YYP*ZMUP
YZM=YYM*ZMUM
AAP1=A1(I,J)*YZP
AAM1=A1(I,JM1)*YZM
AAP2=A2(I,J)*YZP
AAM2=A2(I,JM1)*YZM
AAP3=A3(I,J)*YZP
AAM3=A3(I,JM1)*YZM
AAP4=A4(I,J)*YYP*GKCPP
AAM4=A4(I,JM1)*YYM*GKCPM
UP=U(I,JP1)-U(I,J)
UM=-U(I,JM1)+U(I,J)
VP=V(I,JP1)-V(I,J)
VM=V(I,J)-V(I,JM1)
ERP=E(I,JP1)/RHO(I,JP1)-E(I,J)/RHO(I,J)
ERM=E(I,J)/RHO(I,J)-E(I,JM1)/RHO(I,JM1)
U2P=U(I,JP1)**2-U(I,J)**2
U2M=U(I,J)**2-U(I,JM1)**2
V2P=V(I,JP1)**2-V(I,J)**2

```

```

V2M=V(I,J)**2-V(I,JM1)**2
UVF=U(I,JP1)*V(I,JP1)-U(I,J)*V(I,J)
UVM=U(I,J)*V(I,J)-U(I,JM1)*V(I,JM1)
G(I,J,1)=0.
G(I,J,2)=(AAP1*UP-AAM1*UM)+(AAP2*VF-AAM2*VM)
G(I,J,3)=(AAP2*UP-AAM2*UM)+(AAP3*VP-AAM3*VM)
G(I,J,4)=(AAP4*ERP-AAM4*ERM)+0.5*((AAP1-AAP4)*U2P-
    (AAM1-AAM4)*U2M)+0.5*((AAP3-AAP4)*V2P-(AAM3-AAM4)*V2M)+
    (AAP2*UVF-AAM2*UVM)

```

```

C*
C* INSERT THE EXTRA FIRST ORDER TERMS IN CYLINDRICAL COORDINATE
C* SYSTEMS
C*

```

```

EYJ=ETAY(I,J)/RJ(I,J)
EXJ=ETAX(I,J)/RJ(I,J)
DMUV=0.5*(ZMU(I,JP1)*V(I,JP1)-ZMU(I,JM1)*V(I,JM1))
DDV=0.5*(V(I,JP1)-V(I,JM1))
DMUV2=0.5*(ZMU(I,JP1)*V(I,JP1)**2-ZMU(I,JM1)*V(I,JM1)**2)
DMUUV=0.5*(ZMU(I,JP1)*U(I,JP1)*V(I,JP1)-
    *ZMU(I,JM1)*U(I,JM1)*V(I,JM1))
DDU=0.5*(U(I,JP1)-U(I,JM1))
DDMU=0.5*(ZMU(I,JP1)-ZMU(I,JM1))
G(I,J,2)=G(I,J,2)-2./3.*EXJ*DMUV
G(I,J,3)=G(I,J,3)+2./3.*ZMU(I,J)*EXJ*DDU-V(I,J)*EYJ*DDMU)
G(I,J,4)=G(I,J,4)-2./3.*EYJ*DMUV2+EXJ*DMUUV)

```

30 CONTINUE

RETURN

END

```

C-----  

C ** RIGHT HAND SIDE CALCULATION  

C-----
```

SUBROUTINE RHSCL

```
C *****
```

```

IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=80)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
    P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ),
    ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
    ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CEL,THETA,PO,TO,
    ,CEL1,PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF
    ,BIOT,TW1
COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
    ,IWBC,IFLOW
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
    ,(Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))

```

```
C*****
```

ENTRY RHS(I)

I=II

CALL FLUX(I-1)

```
C    IF((I.NE.2.AND.I.NE.II).AND.NORD.EQ.1)CALL FLUX(I-2)
    CALL FLUX(I)
```

```

EXII=2.*EXI
EYII=EYI*2.
DO 10 J=1,JL
DO 10 K=1,4
10 DQ(I,J,K)=0.
J=JL
JM1=J-1
IM1=I-1
DO 20 K=1,4
DQ(I,J,K)=DQ(I,J,K)+F(I,J,K)-F(I-1,J,K) +
CHOI *           G(I,J,K)-G(I,JM1,K)
CHOI > (3.D0*G(I,J,K)-4.D0*G(I,J-1,K)+G(I,J-2,K))*0.5D0
CHOI
20 CONTINUE
DO 100 J=2,JL1
JP1=J+1
JM1=J-1
DO 100 K=1,4
IF(I.NE.1)THEN
DQ(I,J,K)=DQ(I,J,K)+F(I,J,K)-F(I-1,J,K) +
>           (G(I,JP1,K)-G(I,JM1,K))*0.5
ELSE
DQ(I,J,K)=DQ(I,J,K)+0.5*(G(I,JP1,K)-G(I,JM1,K))
ENDIF
100 CONTINUE
IF(I.EQ.IL) GOTO 120
IF(I.NE.2.AND.I.NE.IL1)THEN
DO 110 J=1,JL
DO 110 K=1,4
DQ(I,J,K)=DQ(I,J,K)+NORD*0.5*(F(I,J,K)-2.*F(I-1,J,K) +
*                           F(I-2,J,K))
110 CONTINUE
ENDIF
120 CONTINUE
IF(I.EQ.IL)GOTO 180
IP1=I+1
CALL FLUXM(IP1)
CALL FLUXM(I)
IF((I.NE.IL1.AND.I.NE.2).AND.NORD.EQ.1)CALL FLUXM(I+2)
DO 170 J=2,JL
DO 170 K=1,4
DQ(I,J,K)=DQ(I,J,K)+G(IP1,J,K)-G(I,J,K)
IF(I.NE.IL1.AND.I.NE.2)DQ(I,J,K)=DQ(I,J,K)-NORD*0.5*
*           (G(I+2,J,K)-2.*G(I+1,J,K)+G(I,J,K))
170 CONTINUE
180 CONTINUE
DO 200 J=2,JL
DQ(I,J,3)=DQ(I,J,3)-P(I,J)/RJ(I,J)
200 CONTINUE
RETURN
C*
C* VISCOUS RIGHT HAND SIDE
C*
ENTRY VRHS(II)

```

```

I=II
CALL VFLUX(I)
DO 300 J=2,JL1
DO 300 K=2,4
300 DQ(I,J,K)=DQ(I,J,K)-G(I,J,K)
DO 400 J=2,JL
DQ(I,J,3)=DQ(I,J,3)+4./3.*ZMU(I,J)*V(I,J)/(RJ(I,J)*Y(I,J))
400 CONTINUE
RETURN
END
C ****
C SERVICE SUBROUTINE
C ****
SUBROUTINE SUPPLY
IMPLICIT REAL*8(A-H,O-Z)
PARAMETER (IZ=150,JZ=80)
COMMON/VECTOR/DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),G(IZ,JZ,4),
> P(IZ,JZ),U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ)
COMMON/COORD/SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),ETAY(IZ,JZ)
> ,ZMUT(JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),DELTAU(IZ,JZ)
> ,AREA(IZ),ZMU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),A4(IZ,JZ)
COMMON/CONST/AIN,AEX,RL,EXI,EYI,OMEGAX,OMEGAY,CFL,THETA,PO,TO,
> CFL1,PRNT,PB,RM1,SUM(4),ZMUO,REN,PRN,TWALL,TREF
>,BIOT,TW1
COMMON/CONST1/GAMMA(IZ,JZ),GM1(IZ,JZ),CP(IZ,JZ),CV(IZ,JZ),RGAS
COMMON/INTEG/IL,JL,IL1,JL1,NEND,NBEG,NADV,ITIME,IVISC,NORD,IWALL
> ,IWBC,IFLOW
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),E(IZ,JZ)
EQUIVALENCE(Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),E(1,1))
C*****
DIMENSION SS(4)
DATA GO,PATM/9.8067,101325./
ENTRY CHECK
DO 10 K=1,4
10 SS(K)=0.
DO 20 I=2,IL
DO 20 J=2,JL
DO 20 K=1,4
QQ=Q(I,J,K)
IE(QQ.EQ.0.D0)GO TO 20
SS(K)=SS(K)+(DQ(I,J,K)*RJ(I,J)/Y(I,J)/QQ)**2
20 CONTINUE
DO 30 K=1,4
30 SS(K)=DSQRT(SS(K))/(IL*JL)
WRITE(19,500)NADV,(SS(K),K=1,4)
500 FORMAT(I5,3X,4(1X,E14.7))
RETURN
ENTRY MASS
C
C MASS FLOW RATE
C
PPI=DARCOS(-1.D0)
DO 80 I=1,IL
FLRT=0.

```

```

DO 75 J=1,JL1
DELR=DSQRT((X(I,J+1)-X(I,J))**2+(Y(I,J+1)-Y(I,J))**2)
CXCY=DSQRT(SAIX(I,J)**2+SAIY(I,J)**2)
CXCY1=DSQRT(SAIX(I,J+1)**2+SAIY(I,J+1)**2)
FLRT=FLRT+0.5*PPI*(Y(I,J+1)+Y(I,J))*DELR
+      *(RHO(I,J+1)*UN(I,J+1),CXCY1+RHO(I,J)*UN(I,J)/CXCY)
75  CONTINUE
      WRITE(18,789)I,FLRT
80  CONTINUE
789  FORMAT(1X,I8,E14.7)

C
C THRUST AND ISP CALCULATIONS
C
      I=IL
      THRUST=0.
      DO 85 J=1,JL1
      DELR=DSQRT((X(I,J+1)-X(I,J))**2+(Y(I,J+1)-Y(I,J))**2)
      THRUST=THRUST+0.5*PPI*(Y(I,J+1)+Y(I,J))*DELR*
>      (RHO(I,J+1)*U(I,J+1)**2+P(I,J+1)-PATM+
>      RHO(I,J) *U(I,J)**2+P(I,J)-PATM)
85  CONTINUE
      CCC=THRUST/FLRT
      SPI=CCC/G0
      WRITE(18,788) THRUST,SPI
788  FORMAT(//,'*** THRUST=',E14.7,//,'*** ISP =',E14.7)

C
      RETURN
      ENTRY OUTPUT
      WRITE(18,550)NADV
550  FORMAT(//10(1H*)/'    NADV=',I5//)
      DO 50 I=1,IL
      DO 50 J=1,JL
      ST=(E(I,J)/RHO(I,J)-GM1(I,J)*0.5/GAMMA(I,J)*(U(I,J)**2+
>      V(I,J)**2))/CV(I,J)
      TT=(E(I,J)/RHO(I,J)-0.5*(U(I,J)**2+V(I,J)**2))/CV(I,J)
      RMA=DSQRT((U(I,J)*U(I,J)+V(I,J)*V(I,J))/GAMMA(I,J)
>      *RHO(I,J)/P(I,J))
      SP=P(I,J)*(ST/TT)**(GAMMA(I,J)/GM1(I,J))
      WRITE(18,607)X(I,J),Y(I,J),P(I,J),RMA,TT,V(I,J)
      WRITE(66) (Q(I,J,K),K=1,4),DELTAU(I,J)
607  FORMAT(6(1X,E14.7))
C      WRITE(6,600)I,J,RHO(I,J),U(I,J),V(I,J),E(I,J),ST
C      WRITE(6,650)P(I,J),UN(I,J),VN(I,J),SP,TT
600  FORMAT(1X,'#',I2,',',I2,3X,5(1X,E10.3))
650  FORMAT(10X,5(1X,E10.3))
50  CONTINUE

C
C WRITE THE LAST TWO LINES
C
C      DO 70 I=IL1,IL
C      DO 70 J=1,JL
C70  WRITE(68) (Q(I,J,K),K=1,4)
C
      RETURN
      END

```

C ****

C*

C* LIBRARY SUBROUTINES

C*

```

SUBROUTINE NBTRIP(A,B,C,D,ILO,IU,ORDER)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(1),B(1),C(1),D(1),IPS(5),X(5)
INTEGER ORDER,ORDSQ
ORDSQ=ORDER**2
I=ILO
IOMAT=1+(I-1)*ORDSQ
IOVEC=1+(I-1)*ORDER
CALL LUDPVT(B(IOMAT),ORDER,IPS)
CALL LUSPVT(B(IOMAT),D(IOVEC),D(IOVEC),X,ORDER,IPS)
DO 100 J=1,ORDER
IOMATJ=IOMAT+(J-1)*ORDER
CALL LUSPVT(B(IOMAT),C(IOMATJ),C(IOMATJ),X,ORDER,IPS)
100 CONTINUE
200 CONTINUE
I=I+1
IOMAT=1+(I-1)*ORDSQ
IOVEC=1+(I-1)*ORDER
I1MAT=IOMAT-ORDSQ
I1VEC=IOVEC-ORDER
CALL MULPUT(A(IOMAT),D(I1VEC),D(IOVEC),ORDER)
DO 300 J=1,ORDER
IOMATJ=IOMAT+(J-1)*ORDER
I1MATJ=I1MAT+(J-1)*ORDER
CALL MULPUT(A(IOMAT),C(I1MATJ),B(IOMATJ),ORDER)
300 CONTINUE
IF(I.EQ.IU) GO TO 500
CALL LUDECO(B(IOMAT),ORDER)
CALL LUSOLV(B(IOMAT),D(IOVEC),D(IOVEC),ORDER)
DO 400 J=1,ORDER
IOMATJ=IOMAT+(J-1)*ORDER
CALL LUSOLV(B(IOMAT),C(IOMATJ),C(IOMATJ),ORDER)
400 CONTINUE
GO TO 200
500 CONTINUE
CALL LUDPVT(B(IOMAT),ORDER,IPS)
CALL LUSPVT(B(IOMAT),D(IOVEC),D(IOVEC),X,ORDER,IPS)
600 CONTINUE
I=I-1
IOMAT=1+(I-1)*ORDSQ
IOVEC=1+(I-1)*ORDER
I1VEC=IOVEC+ORDER
CALL MULPUT(C(IOMAT),D(I1VEC),D(IOVEC),ORDER)
IF(I.GT.ILO) GO TO 600
RETURN
END

```

C-----

```

SUBROUTINE LUDPVT(A,ORDER,IPS)
IMPLICIT REAL*8 (A-H,O-Z)
INTEGER ORDER
DIMENSION A(ORDER,1),IPS(ORDER)

```

```

DO 5 I=1,ORDER
IPS(I)=I
5 CONTINUE
NM1=ORDER-1
DO 17 K=1,NM1
BIG=0.ODO
DO 11 I=K,ORDER
IP=IFS(I)
SIZE=DABS(A(IP,K))
IF(SIZE-BIG)11,11,10
10 BIG=SIZE
IDXPIV=I
11 CONTINUE
IF(IDXPIV-K)14,15,14
14 J=IPS(K)
IPS(K)=IPS(IDXPIV)
IPS(IDXPIV)=J
15 KP=IPS(K)
PIVOT=A(KP,K)
KP1=K+1
DO 16 I=KP1,ORDER
IP=IPS(I)
EM=-A(IP,K)/PIVOT
A(IP,K)=-EM
DO 16 J=KP1,ORDER
A(IP,J)=A(IP,J)+EM*A(KP,J)
16 CONTINUE
17 CONTINUE
RETURN
END

```

C-----

```

SUBROUTINE MULPUT(A,B,C,ORDER)
IMPLICIT REAL*8(A-H,O-Z)
INTEGER ORDER
DIMENSION A(1),B(1),C(1)
DO 200 JR=1,ORDER
SUM=0.0
DO 100 JC=1,ORDER
IA=JR+(JC-1)*ORDER
100 SUM=SUM+A(IA)*B(JC)
200 C(JR)=C(JR)-SUM
RETURN
END

```

C-----

```

SUBROUTINE LUSPVT(A,B,C,X,ORDER,IPS)
IMPLICIT REAL*8 (A-H,O-Z)
INTEGER ORDER
DIMENSION A(ORDER,1),B(1),C(1),X(1),IPS(1)
NP1=ORDER+1
IP=IPS(1)
X(1)=B(IP)
DO 2 I=2,ORDER
IP=IPS(I)
IM1=I-1
SUM=0.ODO

```

```

DO 1 J=1,IM1
1 SUM=SUM+A(IP,J)*X(J)
2 X(I)=B(IP)-SUM
IP=IPS(ORDER)
C(ORDER)=X(ORDER)/A(IP,ORDER)
DO 4 IBACK=2,ORDER
I=NP1-IBACK
IP=IPS(I)
IP1=I+1
SUM=0.0D0
DO 3 J=IP1,ORDER
3 SUM=SUM+A(IP,J)*C(J)
4 C(I)=(X(I)-SUM)/A(IP,I)
RETURN
END

```

C-----

```

SUBROUTINE LUDECO(A,ORDER)
IMPLICIT REAL*8(A-H,O-Z)
INTEGER ORDER
DIMENSION A(ORDER,1)
DO 8 JC=2,ORDER
8 A(1,JC)=A(1,JC)/A(1,1)
JRJC=1
10 CONTINUE
JRJC=JRJC+1
JRJCM1=JRJC-1
JRJCP1=JRJC+1
DO 14 JR=JRJC,ORDER
SUM=A(JR,JRJC)
DO 12 JM=1,JRJCM1
12 SUM=SUM-A(JR,JM)*A(JM,JRJC)
A(JR,JRJC)=SUM
IF(JRJC.EQ.ORDER) RETURN
DO 18 JC=JRJCP1,ORDER
SUM=A(JRJC,JC)
DO 16 JM=1,JRJCM1
16 SUM=SUM-A(JRJC,JM)*A(JM,JC)
18 A(JRJC,JC)=SUM/A(JRJC,JRJC)
GO TO 10
END

```

C-----

```

SUBROUTINE LUSOLV(A,B,C,ORDER)
IMPLICIT REAL*8(A-H,O-Z)
INTEGER ORDER
DIMENSION A(ORDER,1),B(1),C(1)
C(1)=C(1)/A(1,1)
DO 14 JR=2,ORDER
JRM1=JR-1
SUM=B(JR)
DO 12 JM=1,JRM1
12 SUM=SUM-A(JR,JM)*C(JM)
C(JR)=SUM/A(JR,JR)
DO 18 JRJR=2,ORDER
JR=ORDER-JRJR+1
JRP1=JR+1

```

```

SUM=C(JR)
DO 16 JMJM=JRP1,ORDER
JM=ORDER-JMJM+JRP1
16 SUM=SUM-A(JR,JM)*C(JM)
18 C(JR)=SUM
RETURN
END
C-----
C   SET ZERO FOR MATRIC (M,M)
SUBROUTINE SZERO(M,A)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(M,M)
DO 10 I=1,M
DO 10 J=1,M
A(I,J)=0.ODO
10 CONTINUE
RETURN
END
C-----
C   SCALAR*METRIC (M,M)
SUBROUTINE SMM(M,C,A,B)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(M,M),B(M,M)
DO 10 I=1,M
DO 10 J=1,M
B(I,J)=C*A(I,J)
10 CONTINUE
RETURN
END
C-----
C   METRIX*METRIX (M*M)
SUBROUTINE MMM(M,A,B,C)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(M,M),B(M,M),C(M,M)
DO 10 I=1,M
DO 10 J=1,M
C(I,J)=0.ODO
DO 10 K=1,M
C(I,J)=C(I,J)+A(I,K)*B(K,J)
10 CONTINUE
RETURN
END
C*****
SUBROUTINE HJAC(A,J)
C*****
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(4,4)
CALL SZERO(4,A)
A(1,1)=1.DO
A(2,2)=1.DO
A(3,3)=1.DO
A(4,4)=1.DO
RETURN
END
C*****

```

```

SUBROUTINE MMV(M,A,B,C)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(M,M),B(M),C(M)
DO 10 I=1,M
C(I)=0.D0
DO 10 K=1,M
C(I)=C(I)+A(I,K)*B(K)
10 CONTINUE
RETURN
END
C***** ****
SUBROUTINE INVER(M,A,AINV)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(4,4),B(4,4),AINV(4,4),COF(4,4)
A11=A(1,1)
A12=A(1,2)
A13=A(1,3)
A14=A(1,4)
A21=A(2,1)
A22=A(2,2)
A23=A(2,3)
A24=A(2,4)
A31=A(3,1)
A32=A(3,2)
A33=A(3,3)
A34=A(3,4)
A41=A(4,1)
A42=A(4,2)
A43=A(4,3)
A44=A(4,4)
DET=A11*(A22*A33*A44+A23*A34*A42+A24*A43*A32-A24*A33*A42
> -A23*A32*A44-A22*A43*A34)-  

> A12*(A21*A33*A44+A23*A34*A41+A24*A43*A31-A24*A33*A41  

> -A23*A31*A44-A21*A43*A34)+  

> A13*(A21*A32*A44+A22*A34*A41+A24*A42*A31-A24*A32*A41  

> -A22*A31*A44-A21*A42*A34)-  

> A14*(A21*A32*A43+A22*A33*A41+A23*A42*A31-A23*A32*A41  

-> -A22*A31*A43-A21*A42*A33)
COF(1,1)=A22*A33*A44+A23*A34*A42+A24*A43*A32-A24*A33*A42
> -A23*A32*A44-A22*A43*A34
COF(1,2)=-(A21*A33*A44+A23*A34*A41+A24*A43*A31-A24*A33*A41
> -A23*A31*A44-A21*A43*A34)
COF(1,3)=A21*A32*A44+A22*A34*A41+A24*A42*A31-A24*A32*A41
> -A22*A31*A44-A21*A42*A34
COF(1,4)=-(A21*A32*A43+A22*A33*A41+A23*A42*A31-A23*A32*A41
> -A22*A31*A43-A21*A42*A33)
COF(2,1)=-(A12*A33*A44+A13*A34*A42+A14*A32*A43-A14*A33*A42
> -A13*A32*A44-A12*A43*A34)
COF(2,2)=A11*A33*A44+A13*A34*A41+A14*A31*A43-A14*A33*A41
> -A13*A31*A44-A11*A43*A34
COF(2,3)=-(A11*A32*A44+A12*A34*A41+A14*A31*A42-A14*A32*A41
> -A12*A31*A44-A11*A42*A34)
COF(2,4)=A11*A32*A43+A12*A33*A41+A13*A31*A42-A13*A32*A41
> -A12*A31*A43-A11*A42*A33
COF(3,1)=A12*A23*A44+A13*A24*A42+A14*A22*A43-A14*A23*A42

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```

> -A13*A22*A44-A12*A43*A24
COF(3, 2)=-(A11*A23*A44+A13*A24*A41+A14*A21*A43-A14*A23*A41
> -A13*A21*A44-A11*A43*A24)
COF(3, 3)=A11*A22*A44+A12*A24*A41+A14*A21*A42-A14*A22*A41
> -A12*A21*A44-A11*A42*A24
COF(3, 4)=-(A11*A22*A43+A12*A23*A41+A13*A21*A42-A13*A22*A41
> -A12*A21*A43-A11*A42*A23)
COF(4, 1)=-(A12*A23*A34+A13*A24*A32+A14*A22*A33-A14*A23*A32
> -A13*A22*A34-A12*A33*A24)
COF(4, 2)=A11*A23*A34+A13*A24*A31+A14*A21*A33-A14*A23*A31
> -A13*A21*A34-A11*A33*A24
COF(4, 3)=-(A11*A22*A34+A12*A24*A31+A14*A21*A32-A14*A22*A31
> -A12*A21*A34-A11*A32*A24)
COF(4, 4)=A11*A22*A33+A12*A23*A31+A13*A21*A32-A13*A22*A31
> -A12*A21*A33-A11*A32*A23
AINV(1, 1)=COF(1, 1)/DET
AINV(1, 2)=COF(2, 1)/DET
AINV(1, 3)=COF(3, 1)/DET
AINV(1, 4)=COF(4, 1)/DET
AINV(2, 1)=COF(1, 2)/DET
AINV(2, 2)=COF(2, 2)/DET
AINV(2, 3)=COF(3, 2)/DET
AINV(2, 4)=COF(4, 2)/DET
AINV(3, 1)=COF(1, 3)/DET
AINV(3, 2)=COF(2, 3)/DET
AINV(3, 3)=COF(3, 3)/DET
AINV(3, 4)=COF(4, 3)/DET
AINV(4, 1)=COF(1, 4)/DET
AINV(4, 2)=COF(2, 4)/DET
AINV(4, 3)=COF(3, 4)/DET
AINV(4, 4)=COF(4, 4)/DET
C CALL MMM(4,A,AINV,B)
C DO 1 MM=1, 4
C WRITE(6,10) (B(MM,NN),NN=1,4)
C 1 CONTINUE
10 FORMAT(4D16.7)
RETURN
END
*****
SUBROUTINE CPGAM(CP,CV,GAMMA,GM1,R,I,J,
> RHO,RHOU,RHOV,E,TCP)
*****
PARAMETER(IZ=150,JZ=100)
IMPLICIT REAL*8 (A-H,O-Z)
COMMON/CPCOFF/ CPA1,CPA2,CPA3,CPA4,CPA5,CPA6,CPA7
> ,CPA8,CPA9,CPA10,ENE(101)
=====
IF(TCP.NE.0.0) GOTO 20
UU=RHOU/RHO
VV=RHOV/RHO
EE=E/RHO-0.5*(UU**2+VV**2)
TT=300.0
IF(EE.LE.ENE(1)) GO TO 20
DO 10 MM=1,101
EA= EE - ENE(MM)

```

```

    EB= EE - ENE(MM+1)
    ESIGN= EA*EB
    IF(ESIGN.LE.0.DO)THEN
        T1=300.0+27.611*DFLOAT(MM-1)
        T2=300.0+27.611*DFLOAT(MM)
        TT=(T2*EA-T1*EB)/(EA-EB)
        GO TO 20
    ELSE
    END IF
10   CONTINUE
    TT=3061.1DO
20   CONTINUE
    IF(TCP.NE.0.0) TT=TCP
C*
    IF(TT.LE.1000.0)THEN
        CP=(CPA6+CPA7*TT+CPA8*TT**2+CPA9*TT**3+CPA10*TT**4)
        CV=CP-R
    ELSE
        CP=(CPA1+CPA2*TT+CPA3*TT**2+CPA4*TT**3+CPA5*TT**4)
        CV=CP-R
    END IF
    GAMMA=CP/CV
    GM1=GAMMA-1.0
    RETURN
    END
C*****SUBROUTINE CPCOEF*****
C*****IMPLICIT REAL*8 (A-H,O-Z)
COMMON/CPCOFF/ CPA1,CPA2,CPA3,CPA4,CPA5,CPA6,CPA7
>           ,CPA8,CPA9,CPA10,ENE(101)
DIMENSION Y(10),A1(10),A2(10),A3(10),A4(10),A5(10)
>           ,A6(10),A7(10),A8(10),A9(10),A10(10),WM(10)
DATA RU,WMMIX/8314.3,20.405/
C=====
C CO
    WM(1)=28.010
    Y(1)= 0.13108
C CO2
    WM(2)=44.0
    Y(2)= 0.03636
C H
    WM(3)=1.0
    Y(3)= 0.02387
C H2
    WM(4)=2.0
    Y(4)= 0.15802
C H2O
    WM(5)=18.0
    Y(5)= 0.32366
C NO
    WM(6)=30.0
    Y(6)= 0.00260
C N2
    WM(7)=28.0

```

Y(7)= 0.30407

C O

WM(8)=16.0

Y(8)= 0.00158

C OH

WM(9)=17.0

Y(9)= 0.01744

C O2

WM(10)=32.0

Y(10)= 0.00129

C-----CO

A1(1)= 0.29840696E+01

A2(1)= 0.14891390E-02

A3(1)=-0.57899684E-06

A4(1)= 0.10364577E-09

A5(1)=-0.69353550E-14

C

A6(1)= 0.37100928E+01

A7(1)=-0.16190964E-02

A8(1)= 0.36923594E-05

A9(1)=-0.20319674E-08

A10(1)= 0.23953344E-12

C-----CO2

A1(2)= 0.44608041E+01

A2(2)= 0.30981719E-02

A3(2)=-0.12392571E-05

A4(2)= 0.22741325E-09

A5(2)=-0.15525954E-13

C

A6(2)= 0.24007797E+01

A7(2)= 0.87350957E-02

A8(2)=-0.66070878E-05

A9(2)= 0.20021861E-08

A10(2)= 0.63274039E-15

C-----H

A1(3)= 0.25000000E+01

A2(3)= 0.00000000

A3(3)= 0.00000000

A4(3)= 0.00000000

A5(3)= 0.00000000

C

A6(3)= 0.25000000E+01

A7(3)= 0.00000000

A8(3)= 0.00000000

A9(3)= 0.00000000

A10(3)= 0.00000000

C-----H2

A1(4)= 0.30558123E+01

A2(4)= 0.59740400E-03

A3(4)=-0.16747471E-08

A4(4)=-0.21247544E-10

A5(4)= 0.25195487E-14

C

A6(4)= 0.29432327E+01

A7(4)= 0.34815509E-02

A8(4)=-0.77713819E-05
A9(4)= 0.74997496E-08
A10(4)=-0.25203379E-11
C-----H2O
A1(5)= 0.26340654E+01
A2(5)= 0.31121899E-02
A3(5)=-0.90278449E-06
A4(5)= 0.12673054E-09
A5(5)=-0.69164732E-14
C
A6(5)= 0.41675564E+01
A7(5)=-0.18106868E-02
A8(5)= 0.59450878E-05
A9(5)=-0.48670871E-08
A10(5)= 0.15284144E-11
C-----NO
A1(6)= 0.31486543E+01
A2(6)= 0.14151823E-02
A3(6)=-0.57574881E-06
A4(6)= 0.10738529E-09
A5(6)=-0.73900199E-14
C
A6(6)= 0.42484931E+01
A7(6)=-0.48661106E-02
A8(6)= 0.11634155E-04
A9(6)=-0.99768494E-08
A10(6)= 0.30483948E-11
C-----N2
A1(7)= 0.28536374E+01
A2(7)= 0.16014368E-02
A3(7)=-0.62888336E-06
A4(7)= 0.11428932E-09
A5(7)=-0.77953822E-14
C
A6(7)= 0.37034288E+01
A7(7)=-0.14179405E-02
A8(7)= 0.28625094E-05
A9(7)=-0.12018374E-08
A10(7)=-0.13475522E-13
C-----O
A1(8)= 0.25342961E+01
A2(8)=-0.12478170E-04
A3(8)=-0.12562724E-07
A4(8)= 0.69029862E-11
A5(8)=-0.63797095E-15
C
A6(8)= 0.30309401E+01
A7(8)=-0.22525853E-02
A8(8)= 0.39824540E-05
A9(8)=-0.32604921E-08
A10(8)= 0.10152035E-11
C-----OH
A1(9)= 0.28897814E+01
A2(9)= 0.10005879E-02
A3(9)=-0.22048807E-06

FILE: PNSVIS FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STA

A4(9)= 0.20191288E-10
A5(9)=-0.39409831E-15

C

A6(9)= 0.38737300E+01
A7(9)=-0.13393772E-02
A8(9)= 0.16348351E-05
A9(9)=-0.52133639E-09
A10(9)= 0.41826974E-13

C-----O2

A1(10)= 0.36122139E+01
A2(10)= 0.74853166E-03
A3(10)=-0.19820647E-06
A4(10)= 0.33749008E-10
A5(10)=-0.23907374E-14

C

A6(10)= 0.37837135E+01
A7(10)=-0.30233634E-02
A8(10)= 0.99492751E-05
A9(10)=-0.98189101E-08
A10(10)= 0.33031825E-11

C=====

CPA1=0.DO
CPA2=0.DO
CPA3=0.DO
CPA4=0.DO
CPA5=0.DO
CPA6=0.DO
CPA7=0.DO
CPA8=0.DO
CPA9=0.DO
CPA10=0.DO

DO 10 J=1,10

CPA1=CPA1+Y(J)*A1(J)*RU/WMMIX
CPA2=CPA2+Y(J)*A2(J)*RU/WMMIX
CPA3=CPA3+Y(J)*A3(J)*RU/WMMIX
CPA4=CPA4+Y(J)*A4(J)*RU/WMMIX
CPA5=CPA5+Y(J)*A5(J)*RU/WMMIX
CPA6=CPA6+Y(J)*A6(J)*RU/WMMIX
CPA7=CPA7+Y(J)*A7(J)*RU/WMMIX
CPA8=CPA8+Y(J)*A8(J)*RU/WMMIX
CPA9=CPA9+Y(J)*A9(J)*RU/WMMIX
CPA10=CPA10+Y(J)*A10(J)*RU/WMMIX

10 CONTINUE

C...

R=RU/WMMIX
DO 20 MM=1,101
TT=300.0+27.611*DFLOAT(MM-1)
IF(TT.LE.1000.0)THEN
 CP=(CPA6+CPA7*TT+CPA8*TT**2+CPA9*TT**3+CPA10*TT**4)
 CV=CP-R
 ENE(MM)=CV*TT
ELSE
 CP=(CPA1+CPA2*TT+CPA3*TT**2+CPA4*TT**3+CPA5*TT**4)
 CV=CP-R
 ENE(MM)=CV*TT

```

END IF
20 CONTINUE
RETURN
END

DATA.INPUT DD *
&INPUT IL=135, JI=80, NREG=1, NEND=1, NITER=1, PO=1 D+06, TO=3061.1D0,
      CFL1=0.5D+04, CFL=100., OMEGAX=0., OMEGAY=0.5, RM1=1.2, RM2=4.0, NORD=1,
      AIN=0.05, AEX=.236, RL=.695, THETA=1.0, CPO=7152.4853, GAMMA0=1.17,
      ITIME=1, IREAD=1, FST=0.00, TWALL=3000., FSTY=0.9, PB=0., PRNT=0.7,
      IVISC=1, IWALL=0, PRN=0.7, REN=1.D5, TREF=3000., ZMU0=8.5D-03,
      IWBC=1 BIOT=15., TW1=500., IFLOW=1

&END

DATA.FT38F001 DD DSN=STU.I19500.MYH100.HERMES.DIF.H135M80.VIS,
DISP=(OLD,KEEP),VOL=REF=STU.I19500.MYH100.LIB,
DCB=(RECFM=VBS,LRECL=80,BLKSIZE=3120),
SPACE=(TRK,(9,5),RLSE)

DATA.FT66F001 DD DSN=STU.I19500.MYH100.HERMES2.DIF.RERUN.VIS,
DISP=(NEW,KEEP),VOL=REF=STU.I19500.MYH100.LIB,
DCB=(RECFM=VBS,LRECL=80,BLKSIZE=3120),
SPACE=(TRK,(9,5),RLSE)

DATA.FT19F001 DD DSN=STU.I19500.MYH100.HERMES2.DIF.DQ.VIS,
DISP=(NEW,KEEP),VOL=REF=STU.I19500.MYH100.LIB,
DCB=(RECFM=FB,LRECL=80,BLKSIZE=3120),
SPACE=(TRK,(9,5),RLSE)

//DATA.FT18F001 DD DSN=STU.I19500.MYH100.HERMES2.DIF.SOLU.VIS,
//DISP=(NEW,KEEP),VOL=REF=STU.I19500.MYH100.LIB,
//DCB=(RECFM=FB,LRECL=130,BLKSIZE=3120),
//SPACE=(TRK,(9,5),RLSE)

//DATA.FT68F001 DD DSN=STU.I19500.MYH100.HERMES.CONV.LINE.VIS,
//DISP=(OLD,KEEP),VOL=REF=STU.I19500.MYH100.LIB,
//DCB=(RECFM=VBS,LRECL=80,BLKSIZE=3120),
//SPACE=(TRK,(9,5),RLSE)

// EXEC PROMPTME

```

X14140

USERID: V19 ORIGIN: PSUVM CREATED: 06/20/89 15:48:19
FILENAME: NPROG11 FOR CLASS: A FORMAT: J
SPOOLID: 2822 RECS: 3707 COPY: 1 DUPLICATE: 1

PRINTED AT: PSUVM ID: \$PPCBP01 AT: 06/20/89 15:48:27

*

* THIS FILE WAS SENT BY THE COMMAND:

* PRT3812 NPROG11 FOR A1 (PPCB1 COPIES 1 ORIENT N FONT 11

*

```

PROGRAM NOZZLE(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,
> TAPE1,TAPE2,TAPE3,TAPE4,TAPE7,TAPE8,TAPE9,TAPE10,
> TAPE11,TAPE12)
*****
* PROGRAM NAME: NOZZLE
* AXISYMMETRIC SUPERSONIC NOZZLE FLOW
* IN GENERAL COORDINATE SYSTEM
* USING TIME ITERATIVE UW/CD DDADI METHOD
* WITH THIN-LAYER APPROXIMATED NAVIER-STOKES' Eqs.
*****
*
* MAIN PROGRAM
*
*****
* TAPE1 - READ NAMELIST /INPUT/
* TAPE2 - WRITE NAMELIST /INPUT/
* TAPE3 - READ X(I,J), Y(I,J)
* TAPE4 - WRITE FLRT
* TAPE5 - READ INPUT DATA
* TAPE6 - WRITE OUTPUT DATA
* TAPE7 - READ DELTAU(I,J), Q(I,J,K)
* TAPE8 - WRITE DELTAU(I,J), Q(I,J,K)
* TAPE9 - READ NEND, SS(K) (=DQ/Q)
* TAPE10 - WRITE NEND, SS(K) (=DQ/Q)
* TAPE11 - READ NAMELIST /DINPL/
* TAPE12 - WRITE NAMELIST /DINPL/
PARAMETER (IZ=60,JZ=40)
COMMON /VECTOR/ DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),
> G(IZ,JZ,4), P(IZ,JZ),T(IZ,JZ),E(IZ,JZ),AMW(IZ,JZ),
> U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ),
> ZMU(JZ),ZMUT(JZ),ZK(JZ)
COMMON /COORD/ SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),
> ETAY(IZ,JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),
> DELTAU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),
> A4(IZ,JZ)
COMMON /CONS/ EXI,EYI,THETA,CFL,CFL1,OMEGAX,OMEGAY,AIN,AEX,
> RL,RG,AMWO,GAMMAO,REN,PRN,PRNT,TREF,ZMUO,OMEGA,
> PO,TO,TWALL,PB,SUM(4)
COMMON /INTEG/ IL,JL,IL1,JL1,NBEG,NEND,NADV,NORD,ITIME,
> IVISC,IWALL,IWRT
COMMON /INPL/ X1(9),Y1(9),F1(9,9),X2(9),Y2(9),F2(9,9),
> X3(9),Y3(9),F3(9,9),X4(9),Y4(9),F4(9,9),
> X5(9),Y5(9),F5(9,9),X6(9),Y6(9),F6(9,9),
> X7(9),Y7(9),F7(9,9)
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),EO(IZ,JZ)
EQUIVALENCE (Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),EO(1,1))
*****
CALL INITIA
WRITE (6,500)
500 FORMAT(1H1//)
DO 10 NADV=NBEG,NEND
CALL SOLVE
CALL CHECK

```

```

10 CONTINUE
  WRITE (6,500)
  CALL MASS
  WRITE (6,500)
  CALL OUTPUT
  STOP
  END
  SUBROUTINE INITIA
*****
*
*      SET UP INITIAL CONDITIONS
*
*****
PARAMETER (IZ=60,JZ=40)
COMMON /VECTOR/ DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),
>          G(IZ,JZ,4), P(IZ,JZ),T(IZ,JZ),E(IZ,JZ),AMW(IZ,JZ),
>          U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ),
>          ZMU(JZ),ZMUT(JZ),ZK(JZ)
COMMON /COORD/ SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),
>          ETAY(IZ,JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),
>          DELTAU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),
>          A4(IZ,JZ)
COMMON /CONS/ EXI,EYI,THETA,CFL,CFL1,OMEGAX,OMEGAY,AIN,AEX,
>          RL,RG,AMWO,GAMMAO,REN,PRN,PRNT,TREF,ZMU0,OMEGA,
>          PC,TO,TWALL,PB,SUM(4)
COMMON /INTEG/ IL,JL,IL1,JL1,NBEG,NEND,NADV,NORD,ITIME,
>          IVISC,IWALL,IWRT
COMMON /INPL/ X1(9),Y1(9),F1(9,9),X2(9),Y2(9),F2(9,9),
>          X3(9),Y3(9),F3(9,9),X4(9),Y4(9),F4(9,9),
>          X5(9),Y5(9),F5(9,9),X6(9),Y6(9),F6(9,9),
>          X7(9),Y7(9),F7(9,9)
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),EO(IZ,JZ)
EQUIVALENCE (Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
>          (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),EO(1,1))
DIMENSION SS(4)
NAMELIST /INPUT/ IL,JL,NBEG,NEND,NITER,THETA,NORD,CFL,CFL1,
>          ITIME,OMEGAX,OMEGAY,AIN,AEX,RL,FST,FSTY,RM1,RM2,
>          IVISC,IWALL,RG,AMWO,GAMMAO,CP,REN,PRN,PRNT,TREF,
>          ZMU0,OMEGA,PO,TO,TWALL,PB,IREAD,IWRT,IRUN
NAMELIST /DINPL/ X1,Y1,F1,X2,Y2,F2,X3,Y3,F3,
>          X4,Y4,F4,X5,Y5,F5,X6,Y6,F6,
>          X7,Y7,F7
*****
*
*      IF THE DIMENSION IN COMMON BLOCK MUST BE CHANGED
*      PLEASE CHANGE THE PARAMETER STATEMENT
*
... IL=TOTAL GRID NUMBER IN XI DIRECTION
... JL=TOTAL GRID NUMBER IN ETA DIRECTION
... NBEG=COUNTING INDEX OF ITERATION STEP
    =1 FOR THE FIRST RUN
    =ANY NUMBER EXCEPT 1 FOR RERUN
... NEND=NUMBER OF ITERATIONS FOR THE FIRST RUN ONLY
... NITER=NUMBER OF ITERATIONS TO BE RUN WHEN RERUN (NBEG.NE.1)
... THETA=ALWAYS EQUALS 1

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... NORD=IN USE IN PNS, NOT IN USE IN TLNS
... CFL=CFL NUMBER
... CFL1=CFL NUMBER FOR PNS MARCHING
... ITIME=0 FOR CONSTANT DT
 =1 FOR CONSTANT CFL
... OMEGAX=ARTIFICIAL DISSIPATION CONSTANT IN XI DIRECTION
... OMEGAY=ARTIFICIAL DISSIPATION CONSTANT IN ETA DIRECTION
... AIN=THE INLET RADIUS FOR CONICAL NOZZLE (IGNORED IN IREAD=1)
... AEX=THE EXIT RADIUS FOR CONICAL NOZZLE (IGNORED IF IREAD=1)
... RL=TOTAL LENGTH OF CONICAL NOZZLE (IGNORED IF IREAD=1)
... FST=STRETCHING FACTOR IN XI DIRECTION (0 FOR UNIFORM GRID)
 (IGNORED IN IREAD=1) (NOT IN USE IN TLNS)
... FSTY=STRETCHING FACTOR IN ETA DIRECTION (0 FOR UNIFORM GRID)
 (IGNORED IN IREAD=1) (NOT IN USE IN TLNS)
... RM1=THE INITIAL GUESS FOR INLET MACH NUMBER
 (IGNORED IN IREAD=1)
... RM2=THE INITIAL GUESS FOR EXIT MACH NUMBER
 (IGNORED IN IREAD=1)
... IVISC=0 INVISCID FLOW
 =1 VISCOUS FLOW
... IWALL=0 FOR ADIABATIC WALL
 =1 FOR CONSTANT WALL TEMPERATURE
... RG=UNIVERSAL GAS CONSTANT (NOT IN USE IN PNS SOLUTION)
... AMWO=MOLECULAR WEIGHT IN STAGNATION CHAMBER
 (NOT IN USE IN PNS)
... GAMMAO=SPECIFIC HEAT RATIO (STAGNATION CHAMBER VALUE WHEN
 USED FOR REAL CASES IN TLNS)
... CP=CONSTANT PRESSURE SPECIFIC HEAT (NOT IN USE IN TLNS)
... REN=REYNOLDS NUMBER
 (CAN BE SWITCH ON OR OFF IN THIS SUBROUTINE)
... PRN=PRANDTL NUMBER
... PRNT=TURBULENT PRANDTL NUMBER
 =0. FOR LAMINAR FLOW
 =0.9 FOR TURBULENT FLOW
... TREF=THE REFERENCE TEMPERATURE FOR VISCOSITY CALCULATION
... ZMUO=THE VISCOSITY AT T=TREF
... OMEGA=EXPONENTIAL VISCOSITY LAW
... PO=STAGNATION PRESSURE
... TO=STAGNATION TEMPERATURE
... TWALL=GIVEN WALL TEMPERATURE FOR IWALL=1
... PB=THE BACK PRESSURE AT THE EXIT OF NOZZLE
 =0. (SUBSONIC FLOW EXTRAPOLATED FROM INTERIOR)
 =THE SPECIFIED BACK PRESSURE (FIXED THE PRESSURE FOR
 SUBSONIC PORTION AT EXIT)
... IREAD=0 FOR DEFAULT CONICAL NOZZLE
 =1 READ GRID FROM DATA FILE
... IWRT=1 PRINTING OF FLOWFIELD RESULTS
 =0 NO PRINTING OF FLOWFIELD RESULTS
... IRUN=0 FOR 1ST RUN
*
* READ INPUT DATA
*
 READ (1,INPUT)
 READ (11,DINPL)
 IRUN=IRUN+1

```

    IL1=IL-1
    JL1=JL-1
*
*      READ GRID FROM DATA FILE
*
      IF(IREAD.EQ.1) THEN
        READ (3,501) ((X(I,J),Y(I,J),I=1,IL),J=1,JL)
501    FORMAT(E17.9,4E16.9)
      ELSE
      END IF
*
*      COORDINATE TRANSFORMATION
*
      EXI=1.0
      EYI=1.0
      DO 30 I=1,IL
      IP1=I+1
      IM1=I-1
      IF(I.EQ.1) IM1=1
      IF(I.EQ.IL) IP1=IL
      DSAI=2.*EXI
      IF(I.EQ.1.OR.I.EQ.IL) DSAI=EXI
      DO 30 J=1,JL
      JP1=J+1
      JM1=J-1
      IF(J.EQ.1) JM1=1
      IF(J.EQ.JL) JP1=JL
      DETA=2.*EYI
      IF(J.EQ.1.OR.J.EQ.JL) DETA=EYI
      XSAI=(X(IP1,J)-X(IM1,J))/DSAI
      YSAI=(Y(IP1,J)-Y(IM1,J))/DSAI
      XETA=(X(I,JP1)-X(I,JM1))/DETA
      YETA=(Y(I,JP1)-Y(I,JM1))/DETA
      IF(J.EQ.1) THEN
        XETA=XETA-0.5*(X(I,J)-2.*X(I,J+1)+X(I,J+2))
        YETA=YETA-0.5*(Y(I,J)-2.*Y(I,J+1)+Y(I,J+2))
      ELSE
      END IF
*
*      JACOBIAN IS DEFINED AS -
*
*          -1
*      J=(X   *Y   -X   *Y   )
*          SAI   ETA   ETA   SAI
*
      RJP=XSAI*YETA-XETA*YSAI
      RJ(I,J)=1./RJP
      SAIX(I,J)=YETA/RJP
      SAIY(I,J)=-XETA/RJP
      ETAX(I,J)=-YSAI/RJP
      ETAY(I,J)=XSAI/RJP
30 CONTINUE
*
*      CALCULATE METRIC TERMS AT MID POINTS
*

```

```

CALL MCONST
*
* INITIALIZATION - COMPUTE Q(I,J,K)
*
*
* GIVE THE INITIAL VALUE OF VISCOSTY
* IF THE VISCOSITY AT T=TREF IS GIVEN FROM INPUT
* THE CALCULATION FOR ZMUO MUST BE SWITCHED OFF
*
GM1=GAMMA0-1.
R=RG/AMWO
CV=CP/GAMMA0
TIN=TO/(1.+0.5*GM1*RM1**2)
UIN=RM1*SQRT(GAMMA0*R*TIN)
PIN=PO*(TIN/TO)**(GAMMA0/GM1)
RIN=PIN/(R*TIN)
ZMUO=(RIN*UIN*Y(1)*2.)/REN
*
* SKIP TO RERUN THE CODE
*
IF(IRUN.NE.1) GO TO 100
DO 40 I=1,IL
  IF(I.EQ.1) THEN
    AMWS=AMWO
    GAMMA=GAMMA0
    GM1=GAMMA-1.
    RO=PO/(RG/AMWS)/TO
  END IF
42 RM=RM1+FLOAT(I-1)/FLOAT(IL1)*(RM2-RM1)
GMM=1.+0.5*GM1*RM**2
TS=TO/GMM
PS=PO/GMM** (GAMMA/GM1)
RS=PS/(RG/AMWS)/TS
  IF(I.EQ.1) THEN
    WRITE(6,504) TS,PS,RS,AMWS,GAMMA
504 FORMAT(//1X,' TS=',E11.5,' PS=',E11.5,' RS=',E11.5,
>           ' AMW=',E11.5,' GAMMA=',E11.5)
41  TS1=TS
  PS1=PS
  RS1=RS
  ES=FE(RS,TS)
  AMWS=FAMW(RS,TS)
  GAMMA=1.+(RG/AMWS)/(ES/TS)
  GM1=GAMMA-1.
  GMM=1.+0.5*GM1*RM**2
  TS=TO/GMM
  PS=PO/GMM** (GAMMA/GM1)
  RS=PS/(RG/AMWS)/TS
  WRITE(6,503) TS,PS,RS,ES,AMWS,GAMMA
503 FORMAT(1X,' TS=',E11.5,' PS=',E11.5,' RS=',E11.5,
>           ' ES=',E11.5,' AMW=',E11.5,' GAMMA=',E11.5)
  IF(ABS(TS-TS1).GT.1.E-5.OR.ABS(PS-PS1).GT.1.E-5.OR.
>           ABS(RS-RS1).GT.1.E-5) GO TO 41
  END IF
  ES=FE(RS,TS)

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```

CO=SQRT(FC02(PS,RS,TS,ES,AMWS))
UU=RM*CO
DO 40 J=1,JL
IF(I.EQ.1.OR.I.EQ.IL) THEN
  IF(I.EQ.1) SLOPE=(Y(I+1,J)-Y(I,J))/(X(I+1,J)-X(I,J))
  IF(I.EQ.IL) SLOPE=(Y(I,J)-Y(I-1,J))/(X(I,J)-X(I-1,J))
ELSE
  SLOPE=(Y(I+1,J)-Y(I-1,J))/(X(I+1,J)-X(I-1,J))
END IF
DENOM=SQRT(1.+SLOPE*SLOPE)
U(I,J)=UU/DENOM
V(I,J)=UU*SLOPE/DENOM
UN(I,J)=SAIX(I,J)*U(I,J)+SAIY(I,J)*V(I,J)
VN(I,J)=ETAX(I,J)*U(I,J)+ETAY(I,J)*V(I,J)
*
* SLIP INITIAL CONDITION, IVISC=0
*
IF(J.EQ.JL.AND.IVISC.EQ.0) THEN
  U(I,J)=UU/DENOM
  V(I,J)=-ETAX(I,J)/ETAY(I,J)*U(I,J)
  UN(I,J)=U(I,J)*SAIX(I,J)+V(I,J)*SAIY(I,J)
  VN(I,J)=0.
END IF
*
* NO-SLIP INITIAL CONDITION, IVISC=1
*
IF(J.EQ.JL.AND.IVISC.EQ.1) THEN
  U(I,J)=0.
  V(I,J)=0.
  UN(I,J)=0.
  VN(I,J)=0.
END IF
AMW(I,J)=AMWS
E(I,J)=ES
T(I,J)=TS
P(I,J)=PO/(TO/T(I,J))**((GAMMA/GM1))
IF(J.EQ.JL.AND.IVISC.EQ.1) THEN
  IF(IWALL.EQ.1) T(I,J)=TWALL
  P(I,J)=P(I,J-1)
  IF(I.EQ.IL.AND.PB.NE.0.0) P(I,J)=PB
ELSE
END IF
RHO(I,J)=P(I,J)/(RG/AMW(I,J))/T(I,J)
RHOU(I,J)=RHO(I,J)*U(I,J)
RHOV(I,J)=RHO(I,J)*V(I,J)
EO(I,J)=RHO(I,J)*(E(I,J)+0.5*(U(I,J)**2+V(I,J)**2))
40 CONTINUE
*
* INITIALIZATION - COMPUTE DELTAU(I,J)
*
EIGMAX=0.
DO 50 I=1,IL
DO 50 J=1,JL
CO=SQRT(FC02(P(I,J),RHO(I,J),T(I,J),E(I,J),AMW(I,J)))
CX=SQRT(SAIX(I,J)**2+SAIY(I,J)**2)

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CY=SQRT(ETAX(I,J)**2+ETAY(I,J)**2)
CX=(UN(I,J)+CX*CO)/EXI
CY=(VN(I,J)+CY*CO)/EYI
EIGNN=ABS(CX)
IF(EIGNN.LE.ABS(CY)) EIGNN=ABS(CY)
IF(ITIME.EQ.1) GO TO 55
IF(CX.GE.EIGMAX) EIGMAX=CX
IF(CY.GT.EIGMAX) EIGMAX=CY
55 DELTAU(I,J)=CFL/EIGNN
50 CONTINUE
WRITE (6,INPUT)
WRITE (2,INPUT)
WRITE (6,DINPL)
IF(ITIME.EQ.1) RETURN
DO 60 I=1,IL
DO 60 J=1,JL
DELTAU(I,J)=CFL/EIGMAX
60 CONTINUE
RETURN
100 CONTINUE
*
*      READ FLOWFIELD DATA, (NBEG, NEND ARE DETERMINED BY NDUM)
*
70 READ (9,502,END=65) NDUM,(SS(K),K=1,4)
502 FORMAT(I5,3X,4(1X,E14.7))
WRITE (10,502) NDUM,(SS(K),K=1,4)
GO TO 70
65 CONTINUE
NBEG=NDUM+1
NEND=NBEG+NITER-1
READ (7) ((DELTAU(I,J),I=1,IL),J=1,JL)
READ (7) ((RHO(I,J),RHOU(I,J),RHOV(I,J),EO(I,J),
>           I=1,IL),J=1,JL)
DO 80 I=1,IL
DO 80 J=1,JL
U(I,J)=RHOU(I,J)/RHO(I,J)
V(I,J)=RHOV(I,J)/RHO(I,J)
UN(I,J)=U(I,J)*SAIX(I,J)+V(I,J)*SAIY(I,J)
VN(I,J)=U(I,J)*ETAX(I,J)+V(I,J)*ETAY(I,J)
E(I,J)=EO(I,J)/RHO(I,J)-0.5*(U(I,J)**2+V(I,J)**2)
T(I,J)=FT(RHO(I,J),E(I,J))
AMW(I,J)=FAMW(RHO(I,J),T(I,J))
P(I,J)=RHO(I,J)*(RG/AMW(I,J))*T(I,J)
80 CONTINUE
*
*      CHANGES IN /INPUT/ PUT HERE AND ADD - WRITE (2,INPUT)
*
WRITE (6,INPUT)
WRITE (6,DINPL)
RETURN
END
SUBROUTINE SOLVE
*****
*
*      SOLVE SUBROUTINE

```

```

*
*****PARAMETER (IZ=60,JZ=40)
COMMON /VECTOR/ DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),
>      G(IZ,JZ,4), P(IZ,JZ),T(IZ,JZ),E(IZ,JZ),AMW(IZ,JZ),
>      U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ),
>      ZMU(JZ),ZMUT(JZ),ZK(JZ)
COMMON /COORD/ SAI(X(IZ,JZ),SAI(Y(IZ,JZ),ETAX(IZ,JZ),
>      ETAY(IZ,JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),
>      DELTAU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),
>      A4(IZ,JZ)
COMMON /CONS/ EXI,EYI,THETA,CFL,CFL1,OMEGAX,OMEGAY,AIN,AEX,
>      RL,RG,AMWO,GAMMAO,REN,PRN,PRNT,TREF,ZMUO,OMEGA,
>      PO,TO,TWALL,PB,SUM(4)
COMMON /INTEG/ IL,JL,IL1,JL1,NBEG,NEND,NADV,NORD,ITIME,
>      IVISC,IWALL,IWRT
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),EO(IZ,JZ)
EQUIVALENCE (Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
>      (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),EC(1,1))
*****
JEND=JL
IF(IVISC.EQ.1) JEND=JL1
*
* FORWARD SWEEP
*
*
* RHS CALCULATIONS
*
DO 20 I=2,IL
CALL RHSEF(I)
IF(IVISC.EQ.1) THEN
  CALL MULAM(I)
  IF(PRNT.NE.0.0) CALL MUTUR(I)
  CALL KLAM(I)
  IF(PRNT.NE.0.0) CALL KTUR(I)
  CALL RHSVS(I)
END IF
CALL RSHH(I)
*
* CALCULATE RESIDUAL
*
DO 20 J=1,JL
DO 20 K=1,4
DQ(I,J,K)=-DELTAU(I,J)*DQ(I,J,K)
20 CONTINUE
*
* ADD SAI DIRECTION 4TH ORDER ARITFICIAL VISCOSITY
*
IF(OMEGAX.NE.0.0) CALL ADDX
*
* ADD ETA DIRECTION 4TH ORDER ARITFICIAL VISCOSITY
*
IF(OMEGAY.NE.0.0) CALL ADDY
DO 30 I=2,IL
*
```

```

*      SOLVE L-ETA OPERATOR
*
*      CALL COEFY(I)
*
*      UPDATE VARIABLES FORWARD SWEPT
*
        DO 40 J=2,JEND
        RJJ=RJ(I,J)/Y(I,J)
        DO 45 K=1,4
        Q(I,J,K)=Q(I,J,K)+DQ(I,J,K)*RJJ
45    CONTINUE
        U(I,J)=RHOU(I,J)/RHO(I,J)
        V(I,J)=RHOV(I,J)/RHO(I,J)
        UN(I,J)=SAIX(I,J)*U(I,J)+SAIY(I,J)*V(I,J)
        VN(I,J)=U(I,J)*ETAX(I,J)+ETAY(I,J)*V(I,J)
        E(I,J)=EO(I,J)/RHO(I,J)-0.5*(U(I,J)**2+V(I,J)**2)
        T(I,J)=FT(RHO(I,J),E(I,J))
        AMW(I,J)=FAMW(RHO(I,J),T(I,J))
        P(I,J)=RHO(I,J)*(RG/AMW(I,J))*T(I,J)
40    CONTINUE
        CALL MULAM(I)
*
*      CENTERLINE BOUNDARY CONDITIONS
*
*      CALL CLBC(I)
*
*      WALL BOUNDARY CONDITIONS
*
*      IF(IVISC.EQ.1) CALL WALLBC(I)
30    CONTINUE
*
*      BACKWARD SWEPT
*
*
*      RHS CALCULATIONS
*
        DO 70 IB=2,IL1
        I=IL1-IB+2
        CALL RHSEF(I)
        IF(IVISC.EQ.1) THEN
          CALL MULAM(I)
          IF(PRNT.NE.0.0) CALL MUTUR(I)
          CALL KLAM(I)
          IF(PRNT.NE.0.0) CALL KTUR(I)
          CALL RHSVS(I)
        END IF
        CALL RHSH(I)
*
*      CALCULATE RESIDUAL
*
        DO 70 J=1,JL
        DO 70 K=1,4
        DQ(I,J,K)=-DELTAU(I,J)*DQ(I,J,K)
70    CONTINUE
*
*      ADD SAI DIRECTION 4TH ORDER ARTIFICIAL VISCOSITY

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```

*
* IF(OMEGAX.NE.0.0) CALL ADDX
*
* ADD ETA DIRECTION 4TH ORDER ARTIFICIAL VISCOSITY
*
IF(OMEGAY.NE.0.0) CALL ADDY
DO 80 IB=2,IL1
I=IL1-IB+2
*
SOLVE L-ETA OPERATOR
*
CALL COEFY(I)
*
UPDATING VARIABLES BACKWARD SWEEP
*
DO 90 J=2,JEND
RJJ=RJ(I,J)/Y(I,J)
DO 95 K=1,4
Q(I,J,K)=Q(I,J,K)+DQ(I,J,K)*RJJ
95 CONTINUE
U(I,J)=RHOU(I,J)/RHO(I,J)
V(I,J)=RHOV(I,J)/RHO(I,J)
UN(I,J)=U(I,J)*SAIX(I,J)+V(I,J)*SAIY(I,J)
VN(I,J)=U(I,J)*ETAX(I,J)+V(I,J)*ETAY(I,J)
E(I,J)=EO(I,J)/RHO(I,J)-0.5*(U(I,J)**2+V(I,J)**2)
T(I,J)=FT(RHO(I,J),E(I,J))
AMW(I,J)=FAMW(RHO(I,J),T(I,J))
P(I,J)=RHO(I,J)*(RG/AMW(I,J))*T(I,J)
*
UPDATING DELTAU(I,J)
*
CC=SQRT(FC02(P(I,J),RHO(I,J),T(I,J),E(I,J),AMW(I,J)))
CX=SQRT(SAIX(I,J)**2+SAIY(I,J)**2)
CY=SQRT(ETAX(I,J)**2+ETAY(I,J)**2)
CX=(UN(I,J)+CX*CO)
CY=(VN(I,J)+CY*CO)
EIGNN=ABS(CX)
IF(EIGNN.LE.ABS(CY)) EIGNN=ABS(CY)
DELTAU(I,J)=ITIME*CFL/EIGNN+(1-ITIME)*DELTAU(I,J)
90 CONTINUE
*
* CENTERLINE BOUNDARY CONDITIONS
*
CALL CLBC(I)
*
* WALL BOUNDARY CONDITIONS
*
IF(IVISC.EQ.1) CALL WALLBC(I)
80 CONTINUE
RETURN
END
SUBROUTINE COEFY(I)
*****
* SETTING COEFFICIENTS FOR LY-OPERATOR

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```

*
*****PARAMETER (IZ=60,JZ=40)
COMMON /VECTOR/ DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),
> G(IZ,JZ,4), P(IZ,JZ),T(IZ,JZ),E(IZ,JZ),AMW(IZ,JZ),
> U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ),
> ZMU(JZ),ZMUT(JZ),ZK(JZ)
COMMON /COORD/ SAI(X(IZ,JZ),SAI(Y(IZ,JZ),ETAX(IZ,JZ),
> ETAY(IZ,JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),
> DELTAU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),
> A4(IZ,JZ)
COMMON /CONS/ EXI,EYI,THETA,CFL,CELI,OMEGAX,OMEGAY,AIN,AEX,
> RL,RG,AMWO,GAMMAO,REN,PRN,PRNT,TREF,ZM0,OMEGA,
> PO,TO,TWALL,PB,SUM(4)
COMMON /INTEG/ IL,JL,IL1,JL1,NBEG,NEND,NADV,NORD,ITIME,
> IVISC,IWALL,IWRT
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RH0V(IZ,JZ),EO(IZ,JZ)
EQUIVALENCE (Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RH0V(1,1)),(Q(1,1,4),EO(1,1))
DIMENSION IN(4),EE(4,4,JZ),EL(4,JZ),W(4,JZ)
DIMENSION AM(4,4),BM(4,4),CM(4,4),DM(4)
DIMENSION AL(4,4),BE(4),DTEMP(4),ISUB(JZ)
DIMENSION B(4,4),BL1(4,4),D(4,4),A(4,4),AJM(4,4)
DATA ISUB /JZ*0/
*****
*
* CHECK THE SONIC POINT AT DOWNSTREAM END
*
IF(IVISC.NE.1) GO TO 5
IF(I.NE.IL) GO TO 5
DO 10 J=1,JL
CO=SQRT(FC02(P(I,J),RHO(I,J),T(I,J),E(I,J),AMW(I,J)))
CONTRA=UN(I,J)-SQRT(SAI(X(I,J)**2+SAI(Y(I,J)**2)*CO
IF(CONTRA.LT.0.0) THEN
  ISUB(J)=1
ELSE
  ISUB(J)=0
END IF
IF(PB.EQ.0.0) ISUB(J)=0
10 CONTINUE
5 CONTINUE
*
* ON THE CENTER LINE OF THE NOZZLE AT J=1
*
J=1
CALL SZERO(4,AM)
CALL SZERO(4,BM)
DO 15 M=1,4
DM(M)=0.
BM(M,M)=BM(M,M)+1.0
15 CONTINUE
CALL SZERO(4,CM)
CALL EEL(J,4,JL,EE,EL,AM,BM,CM,DM,IN,AL,BE)
*
* INTERIOR NODS

```

```

*
DO 20 J=2,JL1
TAUD=0.50*DELTAU(I,J)*THETA/EYI
TAUD2=2.*TAUD
JM1=J-1
JP1=J+1
CALL JCBAB(2,0,B,I,JM1)
CALL SMM(4,TAUD,B,AM)
CALL SZERO(4,BM)
DO 25 M=1,4
BM(M,M)=BM(M,M)+1.
25 CONTINUE
CALL JCBABFM(1,1,0,A,I,J)
CALL JCBABPM(1,2,0,AJM,I,J)
CALL JCBD(D,I,J)
DO 30 M=1,4
DO 30 N=1,4
BM(M,N)=BM(M,N)-TAUD2*(D(M,N)-A(M,N)+AJM(M,N))
30 CONTINUE
CALL JCBAB(2,0,B,I,JP1)
CALL SMM(4,-TAUD,B,CM)
*
*
* INSERT VISCOUS JACOBIAN LHS HERE
*
IF (IVISC.EQ.1) THEN
  CALL JCBMVS(A,B,D,I,J)
  DO 35 M=1,4
  DO 35 N=1,4
    AM(M,N)=AM(M,N)-DELTAU(I,J)*A(M,N)
    BM(M,N)=BM(M,N)+DELTAU(I,J)*B(M,N)
    CM(M,N)=CM(M,N)-DELTAU(I,J)*D(M,N)
35 CONTINUE
ELSE
END IF
DO 40 K=1,4
DM(K)=DQ(I,J,K)
40 CONTINUE
*
*
* DOWNSTREAM BOUNDARY CONDITIONS FOR VISCOUS FLOW
*
IF (IVISC.EQ.1.AND.(I.EQ.IL.AND.ISUB(J).EQ.1)) THEN
  CALL TMPM(1,0,BL1,I,J)
  DO 45 K=1,4
  BL1(4,K)=0.
45 CONTINUE
CALL MMM(4,BL1,AM,A)
CALL MMM(4,BL1,BM,B)
CALL MMM(4,BL1,CM,D)
DO 50 M=1,4
DO 50 N=1,4
AM(M,N)=A(M,N)
BM(M,N)=B(M,N)
CM(M,N)=D(M,N)
50 CONTINUE
DO 55 M=1,4

```

```

        DTEMP(M)=0.
        DO 55 K=1,4
        DTEMP(M)=DTEMP(M)+BL1(M,K)*DM(K)
55      CONTINUE
        DO 60 M=1,4
        DM(M)=DTEMP(M)
60      CONTINUE
        AR=FAR(P(I,J),RHO(I,J),T(I,J),E(I,J),AMW(I,J))
        AE=FAE(P(I,J),RHO(I,J),T(I,J),E(I,J),AMW(I,J))
        AER=AE/RHO(I,J)
        DFDR=AR+AER*(-EO(I,J)/RHO(I,J)+(U(I,J)**2+V(I,J)**2))
        DPDU=-AER*U(I,J)
        DPDV=-AER*V(I,J)
        DPDE=AER
        BM(4,1)=DPDR/Y(I,J)
        BM(4,2)=DPDU/Y(I,J)
        BM(4,3)=DPDV/Y(I,J)
        BM(4,4)=DPDE/Y(I,J)
        IF(PB.NE.0.0) THEN
            DM(4)=(PB-P(I,J))/RJ(I,J)
        ELSE
            DM(4)=0.
        END IF
    ELSE
    END IF
    CALL EEL(J,4,JL,EE,EL,AM,BM,CM,DM,IN,AL,BE)
20  CONTINUE
*
*      WALL BOUNDARY CONDITIONS FOR INVISCID FLOW, EULER EQS.
*
        J=JL
        TAUD=THETA*DELTAU(I,J)/EYI
        IF(IVISC.EQ.1) GO TO 65
        CALL SZERO(4,AM)
        CALL JCBAB(2,0,B,I,J-1)
        CALL JCBABPM(1,1,0,A,I,J)
        CALL JCBABPM(1,2,0,AJM,I,J)
        CALL TMFP(2,0,BL1,I,J)
        DO 70 M=1,3
        DO 70 N=1,4
        DO 70 K=1,4
        AM(M,N)=AM(M,N)+TAUD*BL1(M,K)*B(K,N)
70      CONTINUE
        CALL SZERO(4,BM)
        CALL JCBAB(2,0,B,I,J)
        CALL JCBD(D,I,J)
        DO 75 M=1,3
        DO 75 N=1,4
        BM(M,N)=BM(M,N)+BL1(M,N)
        DO 75 K=1,4
        BM(M,N)=BM(M,N)
        >           +TAUD*BL1(M,K)*(B(K,N)+A(K,N)-D(K,N)-AJM(K,N))
75      CONTINUE
        BM(4,1)=-VN(I,J)
        BM(4,2)=ETAX(I,J)

```

```

BM(4,3)=ETAY(I,J)
BM(4,4)=0.
CALL SZERO(4,CM)
DO 80 M=1,3
DM(M)=0.
DO 80 K=1,4
DM(M)=DM(M)+BL1(M,K)*DQ(I,J,K)
80 CONTINUE
DM(4)=0.
GO TO 85
65 CONTINUE
CALL SZERO(4,AM)
CALL SZERO(4,BM)
CALL SZERO(4,CM)
DO 90 M=1,4
DM(M)=0.
90 BM(M,M)=1.0
85 CONTINUE
CALL EEL(J,4,JL,EE,EL,AM,BM,CM,DM,IN,AL,BE)
*
```

* SOLVE 4x4 BLOCK TRIDIAGONAL MATRICES

```

CALL SOLU(W,JL,4,EE,EL)
DO 95 J=1,JL
DO 95 K=1,4
DQ(I,J,K)=W(K,J)
95 CONTINUE
RETURN
END
SUBROUTINE BC
*****
```

* SUBROUTINE FOR BOUNDARY CONDITIONS

```

*****  

PARAMETER (IZ=60,JZ=40)
COMMON /VECTOR/ DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),
> G(IZ,JZ,4), P(IZ,JZ),T(IZ,JZ),E(IZ,JZ),AMW(IZ,JZ),
> U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ),
> ZMU(JZ),ZMUT(JZ),ZK(JZ)
COMMON /COORD/ SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),
> ETAY(IZ,JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),
> DELTAU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),
> A4(IZ,JZ)
COMMON /CONS/ EXI,EYI,THETA,CFL,CFL1,OMEGAX,OMEGAY,AIN,AEX,
> RL,RG,AMWO,GAMMAO,REN,PRN,PRNT,TREF,ZMUO,OMEGA,
> PO,TO,TWALL,PB,SUM(4)
COMMON /INTEG/ IL,JL,IL1,JL1,NBEG,NEND,NADV,NORD,ITIME,
> IVISC,IWALL,IWRT
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),EO(IZ,JZ)
EQUIVALENCE (Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),EO(1,1))
*****
```

ENTRY CLBC(II)

```

*
* CENTER LINE BOUNDARY CONDITIONS
*
I=II
*
* THE QUANTITIES EXTRAPOLATED ARE U, RHO, EO AND LET V=0
*
SY=SAIY(I,1)
EY=ETAY(I,1)
DENOM=SY-1.5*EY
IF(I.EQ.1) THEN
  UIM1=0.
  RHOIM1=0.
  EOIM1=0.
ELSE
  UIM1=U(I-1,1)
  RHOIM1=RHO(I-1,1)
  EOIM1=EO(I-1,1)
END IF
U(I,1)=(SY*UIM1-0.5*EY*(4.*U(I,2)-U(I,3)))/DENOM
V(I,1)=0.
UN(I,1)=SAIX(I,1)*U(I,1)
VN(I,1)=ETAX(I,1)*U(I,1)
RHO(I,1)=(SY*RHOIM1-0.5*EY*(4.*RHO(I,2)-RHO(I,3)))/DENOM
EO(I,1)=(SY*EOIM1-0.5*EY*(4.*EO(I,2)-EO(I,3)))/DENOM
E(I,1)=EO(I,1)/RHO(I,1)-0.5*(U(I,1)**2+V(I,1)**2)
T(I,1)=FT(RHO(I,1),E(I,1))
AMW(I,1)=FAMW(RHO(I,1),T(I,1))
P(I,1)=RHO(I,1)*(RG/AMW(I,1))*T(I,1)
RHOU(I,1)=RHO(I,1)*U(I,1)
RHOV(I,1)=RHO(I,1)*V(I,1)
RETURN
*****
ENTRY WALLBC(IL)
*****
*
* WALL BOUNDARY CONDITIONS FOR VISCOUS FLOW
*
I=II
J=JL
CC1=ETAX(I,J)*SAIX(I,J)+ETAY(I,J)*SAIY(I,J)
CC2=ETAX(I,J)**2+ETAY(I,J)**2
IF(I.NE.IL) THEN
  AM=-0.5*CC1
  BM=1.5*CC2
  CM=0.5*CC1
  DM=CC2*(2.*P(I,J-1)-0.5*P(I,J-2))
ELSE
  AM=-CC1
  BM=CC1+1.5*CC2
  CM=0.
  DM=CC2*(2.*P(I,J-1)-0.5*P(I,J-2))
END IF
IP1=I+1
IF(I.EQ.IL) IP1=IL

```

```
*****
* LAMINAR VISCOSITY CALCULATION
*
I=II
*
USE SUTHELAND LAW
*
DO 10 J=1,JL
TOS=TREF+SCONST
TT=T(I,J)
TTS=TT+SCONST
ZMU(J)=ZMU0*TOS/TTS*(TT/TREF)**1.5
*
USE CONSTANT VISCOSITY
*
ZMU(J)=ZMU0
*
USE EXPONENTIAL VISCOSITY LAW
*
ZMU(J)=ZMU0*(TT/TREF)**OMEGA
*
USE DATA
*
ZMU(J)=FZMU(RHO(I,J),E(I,J))
10 CONTINUE
RETURN
*****
ENTRY MUTUR(II)
*****
*
BALDWIN - LOMAX TURBULENCE MODEL
*
I=II
FYMAX=0.0
YMAX=0.0
UDIF=0.
YVERT(JL)=0.0
TAUW=ZMU(JL)*ABS(ETAY(I,JL)*(U(I,JL)-U(I,JL-1))
> -ETAX(I,JL)*(V(I,JL)-V(I,JL-1)))
CYP=SQRT(RHO(I,JL)*TAUW)/ZMU(JL)
*
DO 20 KK=2,JL1
K=JL+1-KK
YVER=YVERT(K+1)+1.0/SQRT(ETAX(I,K)**2+ETAY(I,K)**2)
OMG=ABS(ETAY(I,K)*(U(I,K+1)-U(I,K-1)).5
> +SAIY(I,K)*(U(I,K)-U(I-1,K))
> -ETAX(I,K)*(V(I,K+1)-V(I,K-1)).5
> -SAIX(I,K)*(V(I,K)-V(I-1,K)))
YPLUS=CYP*YVER
CEXP=YPLUS/AP
IF(CEXP.GT.500.) CEXP=500.
TURLEN=VKCON*YVER*(1.00-EXP(-CEXP))
ZMUI(K)=RHO(I,K)*OMG*TURLEN**2
FY=TURLEN/VKCON*OMG
```

```
UTOTAL=SQRT(U(I,K)**2+V(I,K)**2)
IF(UTOTAL.GE.UDIF) UDIF=UTOTAL
IF(FY.LT.FYMAX) GO TO 20
FYMAX=FY
YMAX=YVER
20 YVERT(K)=YVER
*
VXDIF=UDIF
FWAKE1=YMAX*FYMAX
FWAKE2=CKW*YMAX*VXDIF**2/FYMAX
FWAKE=AMIN1(FWAKE1,FWAKE2)
*
DO 30 KK=2, JL1
K=JL+1-KK
FKLEB=(CKLEB*YVERT(K)/YMAX)**6
FKLEB=1./(1.0+5.5*FKLEB)
ZMUO=XK*CCP*RHO(I,K)*FWAKE*FKLEB
IF(ZMUI(K).GT.ZMUO) THEN
  ZMUTUR=ZMUO
ELSE
  ZMUTUR=ZMUI(K)
END IF
ZMUT(K)=ZMUTUR
ZMU(K)=ZMU(K)+ZMUTUR
WRITE (77,500) K,Y(I,K),YVERT(K),U(I,K),ZMUI(K),ZMUO,ZMU(K)
500 FORMAT(2X,I3,6(2X,D13.6))
30 CONTINUE
*
ZMUT(1)=0.
ZMUT(JL)=0.
RETURN
*****
ENTRY KLAM(II)
*****
I=II
DO 40 J=1,JL
ZK(J)=FZK(RHO(I,J),E(I,J))
40 CONTINUE
RETURN
*****
ENTRY KTUR(II)
*****
I=II
DO 50 J=1,JL
CPT=RG/AMW(I,J)+E(I,J)/T(I,J)
ZKT=CPT/PRNT*ZMUT(J)
ZK(J)=ZK(J)+ZKT
50 CONTINUE
RETURN
END
SUBROUTINE MCONST
*****
*
*      SUBROUTINE FOR CALCULATING METRIC TERMS AT THE MIDPOINT
*      (I,J+1/2), (FOR THE VISCOUS VECTOR DMVS/DETA)
```

```

*
*          4      2      2
*      A1(I,J)=(-ETA    +ETA   )
*                  3      X      Y
*
*          1
*      A2(I,J)=-ETA *ETA
*                  3      X      Y
*
*          2      4      2
*      A3(I,J)=(ETA    +-ETA   )
*                  X      3      Y
*
*          2      2
*      A4(I,J)=(ETA    +ETA   )
*                  X      Y
*
*****
PARAMETER (IZ=60,JZ=40)
COMMON /VECTOR/ DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),
>           G(IZ,JZ,4), P(IZ,JZ),T(IZ,JZ),E(IZ,JZ),AMW(IZ,JZ),
>           U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ),
>           ZMU(JZ),ZMUT(JZ),ZK(JZ)
COMMON /COORD/ SAI(X(IZ,JZ),SAI(Y(IZ,JZ),ETAX(IZ,JZ),
>           ETAY(IZ,JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),
>           DELTAU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),
>           A4(IZ,JZ)
COMMON /CONS/ EXI,EYI,THETA,CFL,CFL1,OMEGAX,OMEGAY,AIN,AEX,
>           RL,RG,AMWO,GAMMAO,REN,PRN,PRNT,TREF,ZMUO,OMEGA,
>           PO,TO,TWALL,PB,SUM(4)
COMMON /INTEG/ IL,JL,IL1,JL1,NBEG,NEND,NADV,NORD,ITIME,
>           IVISC,IWALL,IWRT
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),EO(IZ,JZ)
EQUIVALENCE (Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
>           (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),EO(1,1))
DATA FD3,OD3 /1.333333333333,0.333333333333/
*****
DO 10 I=2,IL
DO 10 J=1,JL1
IF(I.EQ.IL) THEN
  XSAI=0.5*(X(I,J)+X(I,J+1)-X(I-1,J)-X(I-1,J+1))
  YSAI=0.5*(Y(I,J)+Y(I,J+1)-Y(I-1,J)-Y(I-1,J+1))
ELSE
  YSAI=0.25*(Y(I+1,J+1)+Y(I+1,J)-Y(I-1,J+1)-Y(I-1,J))
  XSAI=0.25*(X(I+1,J+1)+X(I+1,J)-X(I-1,J+1)-X(I-1,J))
END IF
YETA=Y(I,J+1)-Y(I,J)
XETA=X(I,J+1)-X(I,J)
RJJ=1./(XSAI*YETA-XETA*YSAI)
A1(I,J)=RJJ*RJJ*(FD3*YSAI**2+XSAI**2)
A2(I,J)=-RJJ*RJJ*OD3*XSAI*YSAI
A3(I,J)=RJJ*RJJ*(YSAI**2+FD3*XSAI**2)
A4(I,J)=RJJ*RJJ*(XSAI**2+YSAI**2)
10 CONTINUE

```

```

RETURN
END
SUBROUTINE AVERAGE( IA, IROE, CXM, CYM, RHOM, UM, VM, EOM, PM, UCNM,
> EM, TM, AMWM, I, J)
*****
*
* SUBROUTINE FOR AVERAGING FLOW PROPERTIES
*
* IF IA=1, AVERAGING OF Q FOR A MATRIX
* IF IA=2, AVERAGING OF Q FOR B MATRIX
* IF IROE=0, MEAN VALUE AVERAGING
* IF IROE=1, ROE AVERAGING
*
*****PARAMETER (IZ=60,JZ=40)
COMMON /VECTOR/ DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),
> G(IZ,JZ,4), P(IZ,JZ),T(IZ,JZ),E(IZ,JZ),AMW(IZ,JZ),
> U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ),
> ZMU(JZ),ZMUT(JZ),ZK(JZ)
COMMON /COORD/ SAI(X(IZ,JZ),SAI(Y(IZ,JZ),ETAX(IZ,JZ),
> ETAY(IZ,JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),
> DELTAU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),
> A4(IZ,JZ)
COMMON /CONS/ EXI,EYI,THETA,CFL,CFL1,OMEGAX,OMEGAY,AIN,AEX,
> RL,RG,AMWO,GAMMAO,REN,PRN,PRNT,TREF,ZMUO,OMEGA,
> PO,TO,TWALL,PB,SUM(4)
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),EO(IZ,JZ)
EQUIVALENCE (Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),EO(1,1))
*****
IROE=1
IF( IA.EQ.1) THEN
  I1=I
  J1=J
  I2=I+1
  J2=J
  CXM=0.5*(SAIX(I1,J1)+SAIX(I2,J2))
  CYM=0.5*(SAIY(I1,J1)+SAIY(I2,J2))
END IF
IF( IA.EQ.2) THEN
  I1=I
  J1=J
  I2=I
  J2=J+1
  CXM=0.5*(ETAX(I1,J1)+ETAX(I2,J2))
  CYM=0.5*(ETAY(I1,J1)+ETAY(I2,J2))
END IF
IF( IROE.EQ.0) THEN
  RHOM=0.5*(RHO(I1,J1)+RHO(I2,J2))
  UM=0.5*(U(I1,J1)+U(I2,J2))
  VM=0.5*(V(I1,J1)+V(I2,J2))
  EOM=0.5*(EO(I1,J1)+EO(I2,J2))
  PM=0.5*(P(I1,J1)+P(I2,J2))
  IF( IA.EQ.1) UCNM=0.5*(UN(I1,J1)+UN(I2,J2))
  IF( IA.EQ.2) UCNM=0.5*(VN(I1,J1)+VN(I2,J2))

```

```

UCNM=CXM*UM+CYM*VM
EM=EOM/RHOM-0.5*(UM**2+VM**2)
TM=FT(RHOM, EM)
AMWM=FAMW(RHOM, TM)
END IF
IF(IROE.EQ.1) THEN
  SQRHO1=SQRT(RHO(I1,J1))
  SQRHO2=SQRT(RHO(I2,J2))
  DENOM=SQRHO1+SQRHO2
  RHOM=(RHO(I1,J1)*SQRHO1+RHO(I2,J2)*SQRHO2)/DENOM
  UM=(U(I1,J1)*SQRHO1+U(I2,J2)*SQRHO2)/DENOM
  VM=(V(I1,J1)*SQRHO1+V(I2,J2)*SQRHO2)/DENOM
  HT1=(EO(I1,J1)+P(I1,J1))/RHO(I1,J1)
  HT2=(EO(I2,J2)+P(I2,J2))/RHO(I2,J2)
  HTM=(HT1*SQRHO1+HT2*SQRHO2)/DENOM
* ARITHMETIC AVERAGING OF "REAL GAS GAMMA"
  G1=1.+ (RG/AMW(I1,J1))/(E(I1,J1)/T(I1,J1))
  G2=1.+ (RG/AMW(I2,J2))/(E(I2,J2)/T(I2,J2))
  GM=0.5*(G1+G2)
  PM=(GM-1.)/GM*(RHOM*HTM-0.5*RHOM*(UM**2+VM**2))
  EOM=RHOM*HTM-PM
  UCNM=CXM*UM+CYM*VM
  EM=EOM/RHOM-0.5*(UM**2+VM**2)
  TM=FT(RHOM, EM)
  AMWM=FAMW(RHOM, TM)
END IF
RETURN
END
SUBROUTINE JCBCL
*****
```

```

* SUBROUTINE FOR JACOBIANS CALCULATIONS
*
```

```

*****  

PARAMETER (IZ=60, JZ=40)  

COMMON /VECTOR/ DQ(IZ,JZ,4), Q(IZ,JZ,4), F(IZ,JZ,4),  

>           G(IZ,JZ,4), P(IZ,JZ), T(IZ,JZ), E(IZ,JZ), AMW(IZ,JZ),  

>           U(IZ,JZ), V(IZ,JZ), UN(IZ,JZ), VN(IZ,JZ),  

>           ZMU(JZ), ZMUT(JZ), ZK(JZ)  

COMMON /COORD/ SAIX(IZ,JZ), SAIY(IZ,JZ), ETAX(IZ,JZ),  

>           ETAY(IZ,JZ), RJ(IZ,JZ), X(IZ,JZ), Y(IZ,JZ),  

>           DELTAU(IZ,JZ), A1(IZ,JZ), A2(IZ,JZ), A3(IZ,JZ),  

>           A4(IZ,JZ)  

COMMON /CONS/ EXI, EYI, THETA, CFL, CFL1, OMEGAX, OMEGAY, AIN, AEX,  

>           RL, RG, AMWO, GAMMAO, REN, PRN, PRNT, TREF, ZMUO, OMEGA,  

>           PO, TO, TWALL, PB, SUM(4)  

COMMON /INTEG/ IL, JL, IL1, JL1, NBEG, NEND, NADV, NORD, ITIME,  

>           IVISC, IWALL, IWRT  

DIMENSION RHO(IZ,JZ), RHOU(IZ,JZ), RHOV(IZ,JZ), EO(IZ,JZ)  

EQUIVALENCE (Q(1,1,1), RHO(1,1)), (Q(1,1,2), RHOU(1,1)),  

>           (Q(1,1,3), RHOV(1,1)), (Q(1,1,4), EO(1,1))  

DIMENSION A(4,4), B(4,4), C(4,4), AA(4,4), BB(4,4), DIAG(4),  

>           D(4,4)
*****
```

```

ENTRY JCBAB(IA, IMID, A, I, J)
```

```
*****
*      JACOBIAN A OR B MATRIX CALCULATIONS
*      A=DE/DQ, B=DF/DQ
*
*      IF IA=1, ACAP MATRIX
*      IF IA=2, BCAP MATRIX
*****
IF((IA.EQ.1.AND.IMID.EQ.0).OR.
>   (IA.EQ.1.AND.IMID.EQ.1.AND.I.EQ.IL)) THEN
  CX=SAIX(I,J)
  CY=SAIY(I,J)
  QRHO=RHO(I,J)
  QU=U(I,J)
  QV=V(I,J)
  QEO=EO(I,J)
  QP=P(I,J)
  QCN=UN(I,J)
  QE=E(I,J)
  QT=T(I,J)
  QAMW=AMW(I,J)
END IF
IF((IA.EQ.2.AND.IMID.EQ.0).OR.
>   (IA.EQ.2.AND.IMID.EQ.1.AND.J.EQ.JL)) THEN
  CX=ETAX(I,J)
  CY=ETAY(I,J)
  QRHO=RHO(I,J)
  QU=U(I,J)
  QV=V(I,J)
  QEO=EO(I,J)
  QP=P(I,J)
  QCN=VN(I,J)
  QE=E(I,J)
  QT=T(I,J)
  QAMW=AMW(I,J)
END IF
IF(IA.EQ.1.AND.IMID.EQ.1.AND.I.NE.IL) THEN
  CALL AVERAGE(IA,IROE,CX,CY,QRHO,QU,QV,QEO,QP,QCN,
>             QE,QT,QAMW,I,J)
END IF
IF(IA.EQ.2.AND.IMID.EQ.1.AND.J.NE.JL) THEN
  CALL AVERAGE(IA,IROE,CX,CY,QRHO,QU,QV,QEO,QP,QCN,
>             QE,QT,QAMW,I,J)
END IF
AR=FAR(QP,QRHO,QT,QE,QAMW)
AE=FAE(QP,QRHO,QT,QE,QAMW)
AER=AE/QRHO
DPDR=AR+AER*(-QEO/QRHO+(QU**2+QV**2))
DPDU=-AER*QU
DPDV=-AER*QV
DPDE=AER
A(1,1)=0.0
A(1,2)=CX
A(1,3)=CY
```

```

A(1,4)=0.0
A(2,1)=-QU*QCN+CX*DPDR
A(2,2)=QCN+CX*(QU+DPDU)
A(2,3)=CY*QU+CX*DPDV
A(2,4)=CX*DPDE
A(3,1)=-QV*QCN+CY*DPDR
A(3,2)=CX*QV+CY*DPDU
A(3,3)=QCN+CY*(QV+DPDV)
A(3,4)=CY*DPDE
A(4,1)=QCN*(DPDR-(QEO+QP)/QRHO)
A(4,2)=QCN*DPDU+CX*(QEO+QP)/QRHO
A(4,3)=QCN*DPDV+CY*(QEO+QP)/QRHO
A(4,4)=QCN*(1.+DPDE)
RETURN
*****
```

```
ENTRY JCBABPM(IA,IB,IMID,A,I,J)
```

```

* SPLITTED JACOBIAN A-PLUS, A-MINUS, B-PLUS, OR B-MINUS
* + -1 -1 + -1 -1 -
* A =T *P *(LAMBDA) *P*T, A =T *P *(LAMBDA) *P*T
```

```

* + -1 -1 + -1 -1 -
* B =T *P *(LAMBDA) *P*T, B =T *P *(LAMBDA) *P*T
```

```

* IF IA=1 IB=1 - A-PLUS MATRIX
* IF IA=1 IB=2 - A-MINUS MATRIX
* IF IA=2 IB=1 - B-PLUS MATRIX
* IF IA=2 IB=2 - B-MINUS MATRIX
* IF IMID=0 - JACOBIAN CALCULATED IN POINT (I,J)
* IF IMID=1 IA=1 - JACOBIAN CALCULATED IN POINT (I+1/2,J)
* IF IMID=1 IA=2 - JACOBIAN CALCULATED IN POINT (I,J+1/2)
```

```

* IF((IA.EQ.1.AND.IMID.EQ.0).OR.
> (IA.EQ.1.AND.IMID.EQ.1.AND.I.EQ.IL)) THEN
```

```
CX=SAIX(I,J)
```

```
CY=SAIY(I,J)
```

```
QRHO=RHO(I,J)
```

```
QU=U(I,J)
```

```
QV=V(I,J)
```

```
QEO=EO(I,J)
```

```
QP=P(I,J)
```

```
QCN=UN(I,J)
```

```
QE=E(I,J)
```

```
QT=T(I,J)
```

```
QAMW=AMW(I,J)
```

```
END IF
```

```
IF((IA.EQ.2.AND.IMID.EQ.0).OR.
```

```
> (IA.EQ.2.AND.IMID.EQ.1.AND.J.EQ.JL)) THEN
```

```
CX=ETAX(I,J)
```

```
CY=ETAY(I,J)
```

```
QRHO=RHO(I,J)
```

```
QU=U(I,J)
```

```
QV=V(I,J)
```

```

QEO=EO(I,J)
QF=P(I,J)
QCN=VN(I,J)
QE=E(I,J)
QT=T(I,J)
QAMW=AMW(I,J)
END IF
IF(IA.EQ.1.AND.IMID.EQ.1.AND.I.NE.IL) THEN
  CALL AVERAGE(IA,IROE,CX,CY,QRHO,QU,QV,QEO,QP,QCN,
>           QE,QT,QAMW,I,J)
END IF
IF(IA.EQ.2.AND.IMID.EQ.1.AND.J.NE.JL) THEN
  CALL AVERAGE(IA,IROE,CX,CY,QRHO,QU,QV,QEO,QP,QCN,
>           QE,QT,QAMW,I,J)
END IF
C0=SQRT(FC02(QP,QRHO,QT,QE,QAMW))
CQ=SQRT(CX**2+CY**2)
CQCO=CQ*C0
EIG4=QCN-CQCO
IF(IB.EQ.1) THEN
  DIAG(1)=QCN
  DIAG(2)=QCN
  DIAG(3)=QCN+CQCO
  DIAG(4)=0.
  IF(EIG4.GE.0.0) DIAG(4)=EIG4
END IF
IF(IB.EQ.2) THEN
  DIAG(1)=0.
  DIAG(2)=0.
  DIAG(3)=0.
  DIAG(4)=0.
  IF(EIG4.LT.0.0) DIAG(4)=EIG4
END IF
CALL TMPM(IA,IMID,AA,I,J)
DO 30 II=1,4
DO 30 JJ=1,4
BB(JJ,II)=DIAG(II)*AA(II,JJ)
30 CONTINUE
CALL PPTP(IA,IMID,AA,I,J)
CALL MMM(4,AA,BB,A)
RETURN
*****
ENTRY JCBD(D,I,J)
*****
*
* SOURCE TERM JACOBIAN MATRIX, D=DH'/DQ
*
* H(1)=0.
* H(2)=0.
* H(3)=(P-4./3.*MU*V/Y)/J
* H(4)=0.
*
*****CALL SZERO(4,D)
IF(IVISC.EQ.0) THEN

```

```

ZMU(J)=0.
DMUDR=0.
DMUDU=0.
DMUDV=0.
DMUDE=0.
ELSE
  CR=FDMUDRE(RHO(I,J),E(I,J))
  CE=FDMUDER(RHO(I,J),E(I,J))
  CER=CE/RHO(I,J)
  DMUDR=CR+CER*(-EO(I,J)/RHO(I,J)+(U(I,J)**2+V(I,J)**2))
  DMUDU=-CER*U(I,J)
  DMUDV=-CER*V(I,J)
  DMUDE=CER
END IF
AR=FAR(P(I,J),RHO(I,J),T(I,J),E(I,J),AMW(I,J))
AE=FAE(P(I,J),RHO(I,J),T(I,J),E(I,J),AMW(I,J))
AER=AE/RHO(I,J)
DPDR=AR+AER*(-EO(I,J)/RHO(I,J)+(U(I,J)**2+V(I,J)**2))
DPDU=-AER*U(I,J)
DPDV=-AER*V(I,J)
DPDE=AER
RY=4./3./Y(I,J)**2
D(3,1)=DPDR/Y(I,J)
>      +IVISC*(-V(I,J)*DMUDR+ZMU(J)*V(I,J)/RHO(I,J))*RY
D(3,2)=DPDU/Y(I,J)
>      +IVISC*(-V(I,J)*DMUDU)*RY
D(3,3)=DPDV/Y(I,J)
>      +IVISC*(-V(I,J)*DMUDV-ZMU(J)/RHO(I,J))*RY
D(3,4)=DPDE/Y(I,J)
>      +IVISC*(-V(I,J)*DMUDE)*RY
RETURN
*****
***** ENTRY JCBMVS(A,B,C,I,J)
*****
*
*   VISCOUS JACOBIAN MATRIX, MVS=-D(DSVS'/DETA+H'')/DQ
*
*   H(1)=0.
*
*   H(2)=-*(-*ETA *D(MU*V)/DETA)
*           1   2
*           J   3   X
*
*   H(3)=-*(*ETA *MU*DU/DETA--*ETA *V*D(MU)/DETA)
*           1   2   2
*           J   3   X   3   Y
*
*   H(4)=-*(*ETA *D(MU*U*V)/DETA--*ETA *D(MU*V*V)/DETA)
*           1   2   2
*           J   3   X   3   Y
*
*****
JP1=J+1
JM1=J-1
YJP1 = Y(I,JP1)/RJ(I,JP1)

```

```

YJP      = 0.5*(Y(I,J)/RJ(I,J)+Y(I,JP1)/RJ(I,JP1))
YJ      = Y(I,J)/RJ(I,J)
YJM     = 0.5*(Y(I,J)/RJ(I,J)+Y(I,JM1)/RJ(I,JM1))
YJM1    = Y(I,JM1)/RJ(I,JM1)
EXJ      = 1./3.*ETAX(I,J)/RJ(I,J)
EYJ      = 1./3.*ETAY(I,J)/RJ(I,J)
RHOP     = 0.5*(RHO(I,J)+RHO(I,JP1))
RHOM     = 0.5*(RHO(I,J)+RHO(I,JM1))
UP      = 0.5*(U(I,J)+U(I,JP1))
UM      = 0.5*(U(I,J)+U(I,JM1))
VP      = 0.5*(V(I,J)+V(I,JP1))
VM      = 0.5*(V(I,J)+V(I,JM1))
EP      = 0.5*(E(I,J)+E(I,JP1))
EM      = 0.5*(E(I,J)+E(I,JM1))
ORP1    = 1./RHO(I,JP1)
OR      = 1./RHO(I,J)
ORM1    = 1./RHO(I,JM1)
UORP1   = U(I,JP1)/RHO(I,JP1)
UOR     = U(I,J)/RHO(I,J)
UORM1   = U(I,JM1)/RHO(I,JM1)
VORP1   = V(I,JP1)/RHO(I,JP1)
VOR     = V(I,J)/RHO(I,J)
VORM1   = V(I,JM1)/RHO(I,JM1)
U2P1    = U(I,JP1)**2
U2P     = (0.5*(U(I,J)+U(I,JP1)))**2
U2      = U(I,J)**2
U2M     = (0.5*(U(I,J)+U(I,JM1)))**2
U2M1    = U(I,JM1)**2
V2P1    = V(I,JP1)**2
V2P     = (0.5*(V(I,J)+V(I,JP1)))**2
V2      = V(I,J)**2
V2M     = (0.5*(V(I,J)+V(I,JM1)))**2
V2M1    = V(I,JM1)**2
UVP1    = U(I,JP1)*V(I,JP1)
UV      = U(I,J)*V(I,J)
UVM1   = U(I,JM1)*V(I,JM1)
U2ORP1  = U2P1*ORP1
U2OR    = U2*OR
U2ORM1  = U2M1*ORM1
V2ORP1  = V2P1*ORP1
V2OR    = V2*OR
V2ORM1  = V2M1*ORM1
UVORP1  = UVP1*ORP1
UVOR    = UV*OR
UVORM1  = UVM1*ORM1
ZMUP    = 0.5*(ZMU(J)+ZMU(JP1))
ZMUM    = 0.5*(ZMU(J)+ZMU(JM1))
YJZMUP  = YJP*ZMUP
YJZMUM  = YJM*ZMUM
ZKP     = 0.5*(ZK(J)+ZK(JP1))
ZKM     = 0.5*(ZK(J)+ZK(JM1))
YJZKP   = YJP*ZKP
YJZKM   = YJM*ZKM
EOORP1  = EO(I,JP1)/RHO(I,JP1)
EOORP   = 0.5*(EO(I,J)/RHO(I,J)+EO(I,JP1)/RHO(I,JP1))

```

```

EOOR    = EO(I,J)/RHO(I,J)
EOORM   = 0.5*(EO(I,J)/RHO(I,J)+EO(I,JM1)/RHO(I,JM1))
EOORM1 = EO(I,JM1)/RHO(I,JM1)

*
BR=FDTDRE(RHO(I,JP1),E(I,JP1))
BE=FDTDER(RHO(I,JP1),E(I,JP1))
BER=BE/RHO(I,JP1)
DTDRP1=BR+BER*(-EOORP1+(U2P1+V2P1))
DTDUP1=-BER*U(I,JP1)
DTDVP1=-BER*V(I,JP1)
DTDEP1=BER
BR=FDTDRE(RHO(I,J),E(I,J))
BE=FDTDER(RHO(I,J),E(I,J))
BER=BE/RHO(I,J)
DTDR=BR+BER*(-EOOR+(U2+V2))
DTDU=-BER*U(I,J)
DTDV=-BER*V(I,J)
DTDE=BER
BR=FDTDRE(RHO(I,JM1),E(I,JM1))
BE=FDTDER(RHO(I,JM1),E(I,JM1))
BER=BE/RHO(I,JM1)
DTDRM1=BR+BER*(-EOORM1+(U2M1+V2M1))
DTDUM1=-BER*U(I,JM1)
DTDVM1=-BER*V(I,JM1)
DTDEM1=BER

*
CR=FDMUDRE(RHO(I,JP1),E(I,JP1))
CE=FDMUDER(RHO(I,JP1),E(I,JP1))
CER=CE/RHO(I,JP1)
DMUDRP1=CR+CER*(-EOORP1+(U2P1+V2P1))
DMUDUP1=-CER*U(I,JP1)
DMUDVP1=-CER*V(I,JP1)
DMUDEP1=CER
CR=FDMUDRE(RHOP,EP)
CE=FDMUDER(RHOP,EP)
CER=CE/RHOP
DMUDRP=CR+CER*(-EOORP+(U2P+V2P))
DMUDUP=-CER*UP
DMUDVP=-CER*VP
DMUDEP=CER
CR=FDMUDRE(RHO(I,J),E(I,J))
CE=FDMUDER(RHO(I,J),E(I,J))
CER=CE/RHO(I,J)
DMUDR=CR+CER*(-EOOR+(U2+V2))
DMUDU=-CER*U(I,J)
DMUDV=-CER*V(I,J)
DMUDE=CER
CR=FDMUDRE(RHOM,EM)
CE=FDMUDER(RHOM,EM)
CER=CE/RHOM
DMUDRM=CR+CER*(-EOORM+(U2M+V2M))
DMUDUM=-CER*UM
DMUDVM=-CER*VM
DMUDEM=CER
CR=FDMUDRE(RHO(I,JM1),E(I,JM1))

```

```

CE=FDMUDER(RHO(I,JM1),E(I,JM1))
CER=CE/RHO(I,JM1)
DMUDRM1=CR+CER*(-EOORM1+(U2M1+V2M1))
DMUDUM1=-CER*U(I,JM1)
DMUDVM1=-CER*V(I,JM1)
DMUDEM1=CER
*
DR=FDKDRE(RHOP,EP)
DE=FDKDER(RHOP,EP)
DER=DE/RHOP
DKDRP=DR+DER*(-EOORP+(U2F+V2P))
DKDUP=-DER*UP
DKDVP=-DER*VP
DKDEP=DER
DR=FDKDRE(RHOM,EM)
DE=FDKDER(RHOM,EM)
DER=DE/RHOM
DKDRM=DR+DER*(-EOORM+(U2M+V2M))
DKDUM=-DER*UM
DKDVM=-DER*VM
DKDEM=DER
*
* COMPUTE -M=-(DSVS'/DQ)/DETA
*
IF(JM1.EQ.1) THEN
  CALL SZERO(4,A)
ELSE
  A(1,1)=0.
  A(1,2)=0.
  A(1,3)=0.
  A(1,4)=0.
  A(2,1)=-DMUDRM*(A1(I,JM1)*U(I,JM1)+A2(I,JM1)*V(I,JM1))
  >      +YJZMUM*(A1(I,JM1)*UORM1+A2(I,JM1)*VORM1)/YJM1
  A(2,2)=-DMUDUM*(A1(I,JM1)*U(I,JM1)+A2(I,JM1)*V(I,JM1))
  >      -YJZMUM*A1(I,JM1)*ORM1/YJM1
  A(2,3)=-DMUDVM*(A1(I,JM1)*U(I,JM1)+A2(I,JM1)*V(I,JM1))
  >      -YJZMUM*A2(I,JM1)*ORM1/YJM1
  A(2,4)=-DMUDEM*(A1(I,JM1)*U(I,JM1)+A2(I,JM1)*V(I,JM1))
  A(3,1)=-DMUDRM*(A3(I,JM1)*V(I,JM1)+A2(I,JM1)*U(I,JM1))
  >      +YJZMUM*(A3(I,JM1)*VORM1+A2(I,JM1)*UORM1)/YJM1
  A(3,2)=-DMUDUM*(A3(I,JM1)*V(I,JM1)+A2(I,JM1)*U(I,JM1))
  >      -YJZMUM*A2(I,JM1)*ORM1/YJM1
  A(3,3)=-DMUDVM*(A3(I,JM1)*V(I,JM1)+A2(I,JM1)*U(I,JM1))
  >      -YJZMUM*A3(I,JM1)*ORM1/YJM1
  A(3,4)=-DMUDEM*(A3(I,JM1)*V(I,JM1)+A2(I,JM1)*U(I,JM1))
  A(4,1)=-DMUDRM*(0.5*A1(I,JM1)*U2M1+A2(I,JM1)*UVML
  >      +0.5*A3(I,JM1)*V2M1)
  >      +YJZMUM*(A1(I,JM1)*U2ORM1+2.0*A2(I,JM1)*UVORM1
  >      +A3(I,JM1)*V2ORM1)/YJM1
  >      -DKDRM*A4(I,JM1)*T(I,JM1)
  >      -YJZKM*A4(I,JM1)*DTDRM1/YJM1
  A(4,2)=-DMUDUM*(0.5*A1(I,JM1)*U2M1+A2(I,JM1)*UVML
  >      +0.5*A3(I,JM1)*V2M1)
  >      -YJZMUM*(A1(I,JM1)*UORM1+A2(I,JM1)*VORM1)/YJM1
  >      -DKDUM*A4(I,JM1)*T(I,JM1)

```

```

> -YJZKM*A4(I,JM1)*DTDUM1/YJM1
A(4,3)=-DMUDVM*(0.5*A1(I,JM1)*U2M1+A2(I,JM1)*UVM1
> +0.5*A3(I,JM1)*V2M1)
> -YJZMUM*(A2(I,JM1)*UORM1+A3(I,JM1)*VORM1)/YJM1
> -DKDVM*A4(I,JM1)*T(I,JM1)
> -YJZKM*A4(I,JM1)*DTDVM1/YJM1
A(4,4)=-DMUDEM*(0.5*A1(I,JM1)*U2M1+A2(I,JM1)*UVM1
> +0.5*A3(I,JM1)*V2M1)
> -DKDEM*A4(I,JM1)*T(I,JM1)
> -YJZKM*A4(I,JM1)*DTDEM1/YJM1
END IF
C(1,1)=0.
C(1,2)=0.
C(1,3)=0.
C(1,4)=0.
C(2,1)=-DMUDRP*(A1(I,J)*U(I,JP1)+A2(I,J)*V(I,JP1))
> +YJZMUP*(A1(I,J)*UORP1+A2(I,J)*VORP1)/YJP1
C(2,2)=-DMUDUP*(A1(I,J)*U(I,JP1)+A2(I,J)*V(I,JP1))
> -YJZMUP*A1(I,J)*ORP1/YJP1
C(2,3)=-DMUDVP*(A1(I,J)*U(I,JP1)+A2(I,J)*V(I,JP1))
> -YJZMUP*A2(I,J)*ORP1/YJP1
C(2,4)=-DMUDEP*(A1(I,J)*U(I,JP1)+A2(I,J)*V(I,JP1))
C(3,1)=-DMUDRP*(A3(I,J)*V(I,JP1)+A2(I,J)*U(I,JP1))
> +YJZMUP*(A3(I,J)*VORP1+A2(I,J)*UORP1)/YJP1
C(3,2)=-DMUDUP*(A3(I,J)*V(I,JP1)+A2(I,J)*U(I,JP1))
> -YJZMUP*A2(I,J)*ORP1/YJP1
C(3,3)=-DMUDVP*(A3(I,J)*V(I,JP1)+A2(I,J)*U(I,JP1))
> -YJZMUP*A3(I,J)*ORP1/YJP1
C(3,4)=-DMUDEP*(A3(I,J)*V(I,JP1)+A2(I,J)*U(I,JP1))
C(4,1)=-DMUDRP*(0.5*A1(I,J)*U2P1+A2(I,J)*UVP1
> +0.5*A3(I,J)*V2P1)
> +YJZMUP*(A1(I,J)*U2ORP1+2.0*A2(I,J)*UVORP1
> +A3(I,J)*V2ORP1)/YJP1
> -DKDRP*A4(I,J)*T(I,JP1)
> -YJZKP*A4(I,J)*DTDRP1/YJP1
C(4,2)=-DMUDUP*(0.5*A1(I,J)*U2P1+A2(I,J)*UVP1
> +0.5*A3(I,J)*V2P1)
> -YJZMUP*(A1(I,J)*UORP1+A2(I,J)*VORP1)/YJP1
> -DKDUP*A4(I,J)*T(I,JP1)
> -YJZKP*A4(I,J)*DTDUP1/YJP1
C(4,3)=-DMUDVP*(0.5*A1(I,J)*U2P1+A2(I,J)*UVP1
> +0.5*A3(I,J)*V2P1)
> -YJZMUP*(A2(I,J)*UORP1+A3(I,J)*VORP1)/YJP1
> -DKDVP*A4(I,J)*T(I,JP1)
> -YJZKP*A4(I,J)*DTDVP1/YJP1
C(4,4)=-DMUDEP*(0.5*A1(I,J)*U2P1+A2(I,J)*UVP1
> +0.5*A3(I,J)*V2P1)
> -DKDEP*A4(I,J)*T(I,JP1)
> -YJZKP*A4(I,J)*DTDEP1/YJP1
B(1,1)=0.
B(1,2)=0.
B(1,3)=0.
B(1,4)=0.
B(2,1)=(DMUDRP*A1(I,J)+DMUDRM*A1(I,JM1))*U(I,J)
> +(DMUDRP*A2(I,J)+DMUDRM*A2(I,JM1))*V(I,J)

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```

>      - (YJZMUP*A1(I,J)+YJZMUM*A1(I,JM1))*UOR/YJ
>      - (YJZMUP*A2(I,J)+YJZMUM*A2(I,JM1))*VOR/YJ
B(2,2)=(DMUDUP*A1(I,J)+DMUDUM*A1(I,JM1))*U(I,J)
>      + (DMUDUP*A2(I,J)+DMUDUM*A2(I,JM1))*V(I,J)
>      + (YJZMUP*A1(I,J)+YJZMUM*A1(I,JM1))*OR/YJ
B(2,3)=(DMUDVP*A1(I,J)+DMUDVM*A1(I,JM1))*U(I,J)
>      + (DMUDVF*A2(I,J)+DMUDVM*A2(I,JM1))*V(I,J)
>      + (YJZMUF*A2(I,J)+YJZMUM*A2(I,JM1))*OR/YJ
B(2,4)=(DMUDEP*A1(I,J)+DMUDEM*A1(I,JM1))*U(I,J)
>      + (DMUDEF*A2(I,J)+DMUDEM*A2(I,JM1))*V(I,J)
B(3,1)=(DMUDRP*A3(I,J)+DMUDRM*A3(I,JM1))*V(I,J)
>      + (DMUDRP*A2(I,J)+DMUDRM*A2(I,JM1))*U(I,J)
>      - (YJZMUP*A3(I,J)+YJZMUM*A3(I,JM1))*VOR/YJ
>      - (YJZMUP*A2(I,J)+YJZMUM*A2(I,JM1))*UOR/YJ
B(3,2)=(DMUDUP*A3(I,J)+DMUDUM*A3(I,JM1))*V(I,J)
>      + (DMUDUP*A2(I,J)+DMUDUM*A2(I,JM1))*U(I,J)
>      + (YJZMUF*A2(I,J)+YJZMUM*A2(I,JM1))*OR/YJ
B(3,3)=(DMUDVP*A3(I,J)+DMUDVM*A3(I,JM1))*V(I,J)
>      + (DMUDVP*A2(I,J)+DMUDVM*A2(I,JM1))*U(I,J)
>      + (YJZMUP*A3(I,J)+YJZMUM*A3(I,JM1))*OR/YJ
B(3,4)=(DMUDEP*A3(I,J)+DMUDEM*A3(I,JM1))*V(I,J)
>      + (DMUDEF*A2(I,J)+DMUDEM*A2(I,JM1))*U(I,J)
B(4,1)=0.5*(DMUDRP*A1(I,J)+DMUDRM*A1(I,JM1))*U2
>      + (DMUDRP*A2(I,J)+DMUDRM*A2(I,JM1))*UV
>      + 0.5*(DMUDRP*A3(I,J)+DMUDRM*A3(I,JM1))*V2
>      - (YJZMUP*A1(I,J)+YJZMUM*A1(I,JM1))*U2OR/YJ
>      - 2.0*(YJZMUP*A2(I,J)+YJZMUM*A2(I,JM1))*UVOR/YJ
>      - (YJZMUP*A3(I,J)+YJZMUM*A3(I,JM1))*V2OR/YJ
>      + (DKDRP*A4(I,J)+DKDRM*A4(I,JM1))*T(I,J)
>      + (YJZKP*A4(I,J)+YJZKM*A4(I,JM1))*DTDR/YJ
B(4,2)=0.5*(DMUDUP*A1(I,J)+DMUDUM*A1(I,JM1))*U2
>      + (DMUDUP*A2(I,J)+DMUDUM*A2(I,JM1))*UV
>      + 0.5*(DMUDUP*A3(I,J)+DMUDUM*A3(I,JM1))*V2
>      + (YJZMUP*A1(I,J)+YJZMUM*A1(I,JM1))*UOR/YJ
>      + (YJZMUP*A2(I,J)+YJZMUM*A2(I,JM1))*VOR/YJ
>      + (DKDUP*A4(I,J)+DKDUM*A4(I,JM1))*T(I,J)
>      + (YJZKP*A4(I,J)+YJZKM*A4(I,JM1))*DTDU/YJ
B(4,3)=0.5*(DMUDVP*A1(I,J)+DMUDVM*A1(I,JM1))*U2
>      + (DMUDVP*A2(I,J)+DMUDVM*A2(I,JM1))*UV
>      + 0.5*(DMUDVP*A3(I,J)+DMUDVM*A3(I,JM1))*V2
>      + (YJZMUP*A2(I,J)+YJZMUM*A2(I,JM1))*UOR/YJ
>      + (YJZMUP*A3(I,J)+YJZMUM*A3(I,JM1))*VOR/YJ
>      + (DKDVP*A4(I,J)+DKDVM*A4(I,JM1))*T(I,J)
>      + (YJZKP*A4(I,J)+YJZKM*A4(I,JM1))*DTDV/YJ
B(4,4)=0.5*(DMUDEP*A1(I,J)+DMUDEM*A1(I,JM1))*U2
>      + (DMUDEP*A2(I,J)+DMUDEM*A2(I,JM1))*UV
>      + 0.5*(DMUDEP*A3(I,J)+DMUDEM*A3(I,JM1))*V2
>      + (DKDEP*A4(I,J)+DKDEM*A4(I,JM1))*T(I,J)
>      + (YJZKP*A4(I,J)+YJZKM*A4(I,JM1))*DTDE/YJ

```

*
 * COMPUTE -D'--DH' /DQ
 * AND ADD TO PREVIOUS RESULTS
 *

IF(JM1.EQ.1) THEN
 CALL SZERO(4,A)

```

ELSE
A(2,1)=A(2,1)-EXJ*(V(I,JM1)*DMUDRM1-ZMU(JM1)*VORM1)/YJM1
A(2,2)=A(2,2)-EXJ*V(I,JM1)*DMUDUM1/YJM1
A(2,3)=A(2,3)-EXJ*(V(I,JM1)*DMUDVM1+ZMU(JM1)*ORM1)/YJM1
A(2,4)=A(2,4)-EXJ*V(I,JM1)*DMUDEM1/YJM1
A(3,1)=A(3,1)+EXJ*DMUDR/YJ*U(I,JM1)
>           -EXJ*ZMU(J)*UORM1/YJM1
>           +EYJ*VOR/YJ*ZMU(JM1)
>           -EYJ*V(I,J)*DMUDRM1/YJM1
A(3,2)=A(3,2)+EXJ*DMUDU/YJ*U(I,JM1)
>           +EXJ*ZMU(J)*ORM1/YJM1
>           -EYJ*V(I,J)*DMUDUM1/YJM1
A(3,3)=A(3,3)+EXJ*DMUDV/YJ*U(I,JM1)
>           -EYJ*OR/YJ*ZMU(JM1)
>           -EYJ*V(I,J)*DMUDVM1/YJM1
A(3,4)=A(3,4)+EXJ*DMUDE/YJ*U(I,JM1)
>           -EYJ*V(I,J)*DMUDEM1/YJM1
A(4,1)=A(4,1)-EXJ*(DMUDRM1-2.0*ZMU(JM1)*ORM1)*UVM1/YJM1
>           -EYJ*(DMUDRM1-2.0*ZMU(JM1)*ORM1)*V2M1/YJM1
A(4,2)=A(4,2)-EXJ*(DMUDUM1*UVM1+ZMU(JM1)*VORM1)/YJM1
>           -EYJ*(DMUDUM1*V2M1)/YJM1
A(4,3)=A(4,3)-EXJ*(DMUDVM1*UVM1+ZMU(JM1)*UORM1)/YJM1
>           -EYJ*(DMUDVM1*V2M1+2.0*ZMU(JM1)*VORM1)/YJM1
A(4,4)=A(4,4)-EXJ*DMUDEM1*UVM1/YJM1
>           -EYJ*DMUDEM1*V2M1/YJM1
END IF
C(2,1)=C(2,1)+EXJ*(V(I,JP1)*DMUDRP1-ZMU(JP1)*VORP1)/YJP1
C(2,2)=C(2,2)+EXJ*V(I,JP1)*DMUDUP1/YJP1
C(2,3)=C(2,3)+EXJ*(V(I,JP1)*DMUDVP1+ZMU(JP1)*ORP1)/YJP1
C(2,4)=C(2,4)+EXJ*V(I,JP1)*DMUDEP1/YJP1
C(3,1)=C(3,1)-EXJ*DMUDR/YJ*U(I,JP1)
>           +EXJ*ZMU(J)*UORP1/YJP1
>           -EYJ*VOR/YJ*ZMU(JP1)
>           +EYJ*V(I,J)*DMUDRP1/YJP1
C(3,2)=C(3,2)-EXJ*DMUDU/YJ*U(I,JP1)
>           -EXJ*ZMU(J)*ORP1/YJP1
>           +EYJ*V(I,J)*DMUDUP1/YJP1
C(3,3)=C(3,3)-EXJ*DMUDV/YJ*U(I,JP1)
>           +EYJ*OR/YJ*ZMU(JP1)
>           +EYJ*V(I,J)*DMUDVP1/YJP1
C(3,4)=C(3,4)-EXJ*DMUDE/YJ*U(I,JP1)
>           +EYJ*V(I,J)*DMUDEP1/YJP1
C(4,1)=C(4,1)+EXJ*(DMUDRP1-2.0*ZMU(JP1)*ORP1)*UVP1/YJP1
>           +EYJ*(DMUDRP1-2.0*ZMU(JP1)*ORP1)*V2P1/YJP1
C(4,2)=C(4,2)+EXJ*(DMUDUP1*UVP1+ZMU(JP1)*VORP1)/YJP1
>           +EYJ*DMUDUP1*V2P1/YJP1
C(4,3)=C(4,3)+EXJ*(DMUDVP1*UVP1+ZMU(JP1)*UORP1)/YJP1
>           +EYJ*(DMUDVP1*V2P1+2.0*ZMU(JP1)*VORP1)/YJP1
C(4,4)=C(4,4)+EXJ*DMUDEP1*UVP1/YJP1
>           +EYJ*DMUDEP1*V2P1/YJP1
RETURN
END
SUBROUTINE EIGMTX
*****
*
```

* SUBROUTINE FOR EIGENVECTOR MATRIX CALCULATION

 PARAMETER (IZ=60,JZ=40)
 COMMON /VECTOR/ DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),
 > G(IZ,JZ,4), P(IZ,JZ),T(IZ,JZ),E(IZ,JZ),AMW(IZ,JZ),
 > U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ),
 > ZMU(JZ),ZMUT(JZ),ZK(JZ)
 COMMON /COORD/ SAIX(IZ,JZ),SAIY(IZ,JZ),ETAX(IZ,JZ),
 > ETAY(IZ,JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),
 > DELTAU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),
 > A4(IZ,JZ)
 COMMON /CONS/ EXI,EYI,THETA,CFL,CFL1,OMEGAX,OMEGAY,AIN,AEX,
 > RL,RG,AMWO,GAMMAO,REN,PRN,PRNT,TREF,ZMUO,OMEGA,
 > PO,TO,TWALL,PB,SUM(4)
 COMMON /INTEG/ IL,JL,IL1,JL1,NBEG,NEND,NADV,NORD,ITIME,
 > IVISC,IWALL,IWRT
 DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),EO(IZ,JZ)
 EQUIVALENCE (Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
 > (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),EO(1,1))
 DIMENSION A(4,4)

ENTRY TMPM(IA, IMID, A, I, J)

 *
 *
 * -1 -1
 * CALCULATION OF T *P MATRIX
 *
 * IF IA=1 IMID=0 - XI MATRIX CALCULATED IN POINT (I,J)
 * IF IA=2 IMID=0 - ETA MATRIX CALCULATED IN POINT (I,J)
 * IF IA=1 IMID=1 - XI MATRIX CALCULATED IN POINT (I+1/2,J)
 * IF IA=2 IMID=1 - ETA MATRIX CALCULATED IN POINT (I,J+1/2)
 *

 IF((IA.EQ.1.AND.IMID.EQ.0).OR.
 > (IA.EQ.1.AND.IMID.EQ.1.AND.I.EQ.IL)) THEN
 CX=SAIX(I,J)
 CY=SAIY(I,J)
 QRHO=RHO(I,J)
 QU=U(I,J)
 QV=V(I,J)
 QEO=EO(I,J)
 QP=P(I,J)
 QCN=UN(I,J)
 QE=E(I,J)
 QT=T(I,J)
 QAMW=AMW(I,J)
 END IF
 IF((IA.EQ.2.AND.IMID.EQ.0).OR.
 > (IA.EQ.2.AND.IMID.EQ.1.AND.J.EQ.JL)) THEN
 CX=ETAX(I,J)
 CY=ETAY(I,J)
 QRHO=RHO(I,J)
 QU=U(I,J)
 QV=V(I,J)

```

QEO=EO(I,J)
QP=P(I,J)
QCN=VN(I,J)
QE=E(I,J)
QT=T(I,J)
QAMW=AMW(I,J)
END IF
IF(IA.EQ.1.AND.IMID.EQ.1.AND.I.NE.IL) THEN
  CALL AVERAGE(IA,IROE,CX,CY,QRHO,QU,QV,QEO,QP,QCN,
>           QE,QT,QAMW,I,J)
END IF
IF(IA.EQ.2.AND.IMID.EQ.1.AND.J.NE.JL) THEN
  CALL AVERAGE(IA,IROE,CX,CY,QRHO,QU,QV,QEO,QP,QCN,
>           QE,QT,QAMW,I,J)
END IF
SQ2=SQRT(2.0)
C=SQRT(FC02(QP,QRHO,QT,QE,QAMW))
AR=FAR(QP,QRHO,QT,QE,QAMW)
AE=FAE(QP,QRHO,QT,QE,QAMW)
AER=AE/QRHO
DPDR=AR+AER*(-QEO/QRHO+(QU**2+QV**2))
DPDU=-AER*QU
DPDV=-AER*QV
DPDE=AER
C1=CX/SQRT(CX**2+CY**2)
C2=CY/SQRT(CX**2+CY**2)
A(1,1)=1.-DPDR/C**2
A(1,2)=-DPDU/C**2
A(1,3)=-DPDV/C**2
A(1,4)=-DPDE/C**2
A(2,1)=-(C2*QU-C1*QV)/QRHO
A(2,2)=C2/QRHO
A(2,3)=-C1/QRHO
A(2,4)=0.
A(3,1)=(-(C1*QU+C2*QV)+DPDR/C)/SQ2/QRHO
A(3,2)=(C1+DPDU/C)/SQ2/QRHO
A(3,3)=(C2+DPDV/C)/SQ2/QRHO
A(3,4)=DPDE/C/SQ2/QRHO
A(4,1)=((C1*QU+C2*QV)+DPDR/C)/SQ2/QRHO
A(4,2)=(-C1+DPDU/C)/SQ2/QRHO
A(4,3)=(-C2+DPDV/C)/SQ2/QRHO
A(4,4)=DPDE/C/SQ2/QRHO
RETURN
*****
ENTRY PPTP(IA,IMID,A,I,J)
*****
*
* CALCULATION OF P*T MATRIX
*
* IF IA=1 IMID=0 - XI MATRIX CALCULATED IN POINT (I,J)
* IF IA=2 IMID=0 - ETA MATRIX CALCULATED IN POINT (I,J)
* IF IA=1 IMID=1 - XI MATRIX CALCULATED IN POINT (I+1/2,J)
* IF IA=2 IMID=1 - ETA MATRIX CALCULATED IN POINT (I,J+1/2)
*
*****

```

```

IF((IA.EQ.1.AND.IMID.EQ.0).OR.
>   (IA.EQ.1.AND.IMID.EQ.1.AND.I.EQ.IL)) THEN
CX=SAIX(I,J)
CY=SAIY(I,J)
QRHO=RHO(I,J)
QU=U(I,J)
QV=V(I,J)
QEO=EO(I,J)
QP=P(I,J)
QCN=UN(I,J)
QE=E(I,J)
QT=T(I,J)
QAMW=AMW(I,J)
END IF
IF((IA.EQ.2.AND.IMID.EQ.0).OR.
>   (IA.EQ.2.AND.IMID.EQ.1.AND.J.EQ.JL)) THEN
CX=ETAX(I,J)
CY=ETAY(I,J)
QRHO=RHO(I,J)
QU=U(I,J)
QV=V(I,J)
QEO=EO(I,J)
QP=P(I,J)
QCN=VN(I,J)
QE=E(I,J)
QT=T(I,J)
QAMW=AMW(I,J)
END IF
IF(IA.EQ.1.AND.IMID.EQ.1.AND.I.NE.IL) THEN
  CALL AVERAGE(IA,IROE,CX,CY,QRHO,QU,QV,QEO,QP,QCN,
>             QE,QT,QAMW,I,J)
END IF
IF(IA.EQ.2.AND.IMID.EQ.1.AND.J.NE.JL) THEN
  CALL AVERAGE(IA,IROE,CX,CY,QRHO,QU,QV,QEO,QP,QCN,
>             QE,QT,QAMW,I,J)
END IF
SQ2=1./SQRT(2.0)
C=SQRT(FC02(QP,QRHO,QT,QE,QAMW))
AR=FAR(QP,QRHO,QT,QE,QAMW)
AE=FAE(QP,QRHO,QT,QE,QAMW)
AER=AE/QRHO
DPDR=AR+AER*(-QEO/QRHO+(QU**2+QV**2))
DPDU=-AER*QU
DPDV=-AER*QV
DPDE=AER
CXCY=1./SQRT(CX**2+CY**2)
C1=CX*CXY
C2=CY*CXY
A(1,1)=1.
A(1,2)=0.
A(1,3)=QRHO*SQ2/C
A(1,4)=A(1,3)
A(2,1)=QU
A(2,2)=QRHO*C2
A(2,3)=SQ2*QRHO*(QU/C+C1)

```

```

A(2,4)=SQ2*QRHO*(QU/C-C1)
A(3,1)=QV
A(3,2)=-QRHO*C1
A(3,3)=SQ2*QRHO*(QV/C+C2)
A(3,4)=SQ2*QRHO*(QV/C-C2)
A(4,1)=QEO/QRHO-QRHO*AR/AE
A(4,2)=QRHO*(QU*C2-QV*C1)
TEMP1=SQ2*QRHO**2*C/AE
TEMP2=SQ2*QRHO*(QU*C1+QV*C2)
A(4,3)=A(4,1)*QRHO*SQ2/C+TEMP1+TEMP2
A(4,4)=A(4,1)*QRHO*SQ2/C+TEMP1-TEMP2
RETURN
END
SUBROUTINE FLXCL
*****
```

```

*      SUBROUTINE FOR FLUX VECTOR CALCULATION
*
```

```

*****
```

PARAMETER (IZ=60,JZ=40)

COMMON /VECTOR/ DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),
> G(IZ,JZ,4), P(IZ,JZ),T(IZ,JZ),E(IZ,JZ),AMW(IZ,JZ),
> U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ),
> ZMU(JZ),ZMUT(JZ),ZK(JZ)

COMMON /COORD/ SAI(X(IZ,JZ),SAI(Y(IZ,JZ),ETAX(IZ,JZ),
> ETAY(IZ,JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),
> DELTAU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),
> A4(IZ,JZ)

COMMON /CONS/ EXI,EYI,THETA,CFL,CFL1,OMEGAX,OMEGAY,AIN,AEX,
> RL,RG,AMWO,GAMMAO,REN,PRN,PRNT,TREF,ZMUO,OMEGA,
> PO,TO,TWALL,PB,SUM(4)

COMMON /INTEG/ IL,JL,IL1,JL1,NBEG,NEND,NADV,NORD,ITIME,
> IVISC,IWALL,IWRT

DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),EO(IZ,JZ)

EQUIVALENCE (Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),EO(1,1))

DIMENSION A(4,4)

```

*****
```

```

ENTRY FLXE(II)
*****
```

```

*      COMPUTE CONVECTIVE FLUX VECTOR E
*
```

```

*****
```

I=II
DO 10 J=1,JL
F(I,J,1)=RHO(I,J)*UN(I,J)/RJ(I,J)*Y(I,J)
F(I,J,2)=(RHOU(I,J)*UN(I,J)+SAIX(I,J)*P(I,J))/RJ(I,J)*Y(I,J)
F(I,J,3)=(RHOV(I,J)*UN(I,J)+SAIY(I,J)*P(I,J))/RJ(I,J)*Y(I,J)
F(I,J,4)=(EO(I,J)+P(I,J))*UN(I,J)/RJ(I,J)*Y(I,J)

```

10 CONTINUE
RETURN
*****
```

```

ENTRY FLXF(II)
*****
```

```

*
*      COMPUTE CONVECTIVE FLUX VECTOR F
*
*****+
*I=II
DO 20 J=1,JL
G(I,J,1)=RHO(I,J)*VN(I,J)/RJ(I,J)*Y(I,J)
G(I,J,2)=(RHOU(I,J)*VN(I,J)+ETAX(I,J)*P(I,J))/RJ(I,J)*Y(I,J)
G(I,J,3)=(RHOV(I,J)*VN(I,J)+ETAY(I,J)*P(I,J))/RJ(I,J)*Y(I,J)
G(I,J,4)=(EO(I,J)+P(I,J))*VN(I,J)/RJ(I,J)*Y(I,J)
20 CONTINUE
RETURN
*****+
ENTRY FLXEP(II,IMID)
*****
*
*      +
*      E   FLUX VECTOR ( IMID=0 )
*
*      +  +
*      DE =A ( I+1/2,J)*(Q(I+1,J)-Q(I,J)) ( IMID=1 )
*
*****+
*I=II
IF(IMID.EQ.0) THEN
  DO 30 J=1,JL
    CALL JCBABPM(1,1,0,A,I,J)
    DO 31 K=1,4
      F(I,J,K)=0.
      DO 31 JJ=1,4
        F(I,J,K)=F(I,J,K)+A(K,JJ)*Q(I,J,JJ)/RJ(I,J)*Y(I,J)
31  CONTINUE
30  CONTINUE
END IF
IF(IMID.EQ.1.AND.I.NE.IL) THEN
  DO 35 J=1,JL
    CALL JCBABPM(1,1,1,A,I,J)
    DO 36 K=1,4
      F(I,J,K)=0.
      DO 36 JJ=1,4
        YM=0.5*(Y(I,J)+Y(I+1,J))
        RJM=0.5*(RJ(I,J)+RJ(I+1,J))
        F(I,J,K)=F(I,J,K)+A(K,JJ)*(Q(I+1,J,JJ)-Q(I,J,JJ))/RJM*YM
36  CONTINUE
35  CONTINUE
END IF
IF(IMID.EQ.1.AND.I.EQ.IL) THEN
  DO 37 J=1,JL
    CALL JCBABPM(1,1,0,A,I,J)
    DO 38 K=1,4
      F(I,J,K)=0.
      DO 38 JJ=1,4
        YM=Y(I,J)
        RJM=RJ(I,J)
        F(I,J,K)=F(I,J,K)+A(K,JJ)*(Q(I,J,JJ)-Q(I-1,J,JJ))/RJM*YM

```

```

38    CONTINUE
37    CONTINUE
END IF
RETURN
*****
ENTRY FLXEM(II,IMID)
*****
*
*   -
*   E   FLUX VECTOR (IMID=0)
*
*   - -
*   DE =A (I+1/2,J)*(Q(I+1,J)-Q(I,J)) (IMID=1)
*
*****
I=II
IF(IMID.EQ.0) THEN
  DO 40 J=1,JL
  CALL JCBABPM(1,2,0,A,I,J)
  DO 41 K=1,4
  G(I,J,K)=0.
  DO 41 JJ=1,4
  G(I,J,K)=G(I,J,K)+A(K,JJ)*Q(I,J,JJ)/RJ(I,J)*Y(I,J)
41    CONTINUE
40    CONTINUE
END IF
IF(IMID.EQ.1.AND.I.NE.IL) THEN
  DO 45 J=1,JL
  CALL JCBABPM(1,2,1,A,I,J)
  DO 46 K=1,4
  G(I,J,K)=0.
  DO 46 JJ=1,4
  YM=0.5*(Y(I,J)+Y(I+1,J))
  RJM=0.5*(RJ(I,J)+RJ(I+1,J))
  G(I,J,K)=G(I,J,K)+A(K,JJ)*(Q(I+1,J,JJ)-Q(I,J,JJ))/RJM*YM
46    CONTINUE
45    CONTINUE
END IF
IF(IMID.EQ.1.AND.I.EQ.IL) THEN
  DO 47 J=1,JL
  CALL JCBABPM(1,2,0,A,I,J)
  DO 48 K=1,4
  G(I,J,K)=0.
  DO 48 JJ=1,4
  YM=Y(I,J)
  RJM=RJ(I,J)
  G(I,J,K)=G(I,J,K)+A(K,JJ)*(Q(I,J,JJ)-Q(I-1,J,JJ))/RJM*YM
48    CONTINUE
47    CONTINUE
END IF
RETURN
*****
ENTRY FLXFP(II,IMID)
*****
*
```

```

*      +
*      F  FLUX VECTOR (IMID=0)
*
*      +  +
*      DF =B (I,J+1/2)*(Q(I,J+1)-Q(I,J)) (IMID=1)
*
*****+
I=II
IF(IMID.EQ.0) THEN
  DO 50 J=1,JL
    CALL JCBABPM(2,1,0,A,I,J)
  DO 51 K=1,4
    F(I,J,K)=0.
  DO 51 JJ=1,4
    F(I,J,K)=F(I,J,K)+A(K,JJ)*Q(I,J,JJ)/RJ(I,J)*Y(I,J)
51  CONTINUE
50  CONTINUE
END IF
IF(IMID.EQ.1.AND.J.NE.JL) THEN
  DO 55 J=1,JL1
    CALL JCBABPM(2,1,1,A,I,J)
  DO 56 K=1,4
    F(I,J,K)=0.
  DO 56 JJ=1,4
    YM=0.5*(Y(I,J)+Y(I,J+1))
    RJM=0.5*(RJ(I,J)+RJ(I,J+1))
    F(I,J,K)=F(I,J,K)+A(K,JJ)*(Q(I,J+1,JJ)-Q(I,J,JJ))/RJM*YM
56  CONTINUE
55  CONTINUE
END IF
IF(IMID.EQ.1.AND.J.EQ.JL) THEN
  CALL JCBABPM(2,1,0,A,I,J)
  DO 58 K=1,4
    F(I,J,K)=0.
  DO 58 JJ=1,4
    YM=Y(I,J)
    RJM=RJ(I,J)
    F(I,J,K)=F(I,J,K)+A(K,JJ)*(Q(I,J,JJ)-Q(I,J-1,JJ))/RJM*YM
58  CONTINUE
END IF
RETURN
*****
ENTRY FLXFM(II,IMID)
*****
*
*      -
*      F  FLUX VECTOR (IMID=0)
*
*      -  -
*      DF =B (I,J+1/2)*(Q(I,J+1)-Q(I,J))
*
*****+
I=II
IF(IMID.EQ.0) THEN
  DO 60 J=1,JL

```

```

      CALL JCBABPM(2,2,0,A,I,J)
      DO 61 K=1,4
      C(I,J,K)=0.
      DO 61 JJ=1,4
      G(I,J,K)=G(I,J,K)+A(K,JJ)*Q(I,J,JJ)/RJ(I,J)*Y(I,J)
61    CONTINUE
60    CONTINUE
      END IF
      IF(IMID.EQ.1.AND.J.NE.JL) THEN
      DO 65 J=1,JL1
      CALL JCBABPM(2,2,1,A,I,J)
      DO 66 K=1,4
      G(I,J,K)=0.
      DO 66 JJ=1,4
      YM=0.5*(Y(I,J)+Y(I,J+1))
      RJM=0.5*(RJ(I,J)+RJ(I,J+1))
      G(I,J,K)=C(I,J,K)+A(K,JJ)*(Q(I,J+1,JJ)-Q(I,J,JJ))/RJM*YM
66    CONTINUE
65    CONTINUE
      END IF
      IF(IMID.EQ.1.AND.J.EQ.JL) THEN
      CALL JCBABPM(2,2,0,A,I,J)
      DO 68 K=1,4
      G(I,J,K)=0.
      DO 68 JJ=1,4
      YM=Y(I,J)
      RJM=RJ(I,J)
      G(I,J,K)=G(I,J,K)+A(K,JJ)*(Q(I,J,JJ)-Q(I,J-1,JJ))/RJM*YM
68    CONTINUE
      END IF
      RETURN
*****
```

```

ENTRY FLXSVS(II)
*****
*      VISCOUS FLUX VECTOR, (DSVS'/DETA)+H'
*
*      VISCOUS FLUX VECTOR DSVS'/DETA
*
I=II
DO 70 J=2,JL1
JP1=J+1
JM1=J-1
YJP=0.5*(Y(I,J)/RJ(I,J)+Y(I,JP1)/RJ(I,JP1))
YJM=0.5*(Y(I,J)/RJ(I,J)+Y(I,JM1)/RJ(I,JM1))
ZMUP=0.5*(ZMU(J)+ZMU(JP1))
ZMUM=0.5*(ZMU(J)+ZMU(JM1))
ZKP=0.5*(ZK(J)+ZK(JP1))
ZKM=0.5*(ZK(J)+ZK(JM1))
DUP=U(I,JP1)-U(I,J)
DUM=U(I,J)-U(I,JM1)
DVP=V(I,JP1)-V(I,J)
DVM=V(I,J)-V(I,JM1)
```

```

DU2P=U(I,JP1)**2-U(I,J)**2
DU2M=U(I,J)**2-U(I,JM1)**2
DV2P=V(I,JP1)**2-V(I,J)**2
DV2M=V(I,J)**2-V(I,JM1)**2
DUVP=U(I,JP1)*V(I,JP1)-U(I,J)*V(I,J)
DUVM=U(I,J)*V(I,J)-U(I,JM1)*V(I,JM1)
DTP=T(I,JP1)-T(I,J)
DTM=T(I,J)-T(I,JM1)
ZMUA1P=ZMUP*A1(I,J)
ZMUA1M=ZMUM*A1(I,JM1)
ZMUA2P=ZMUP*A2(I,J)
ZMUA2M=ZMUM*A2(I,JM1)
ZMUA3P=ZMUP*A3(I,J)
ZMUA3M=ZMUM*A3(I,JM1)
ZKA4P=ZKP*A4(I,J)
ZKA4M=ZKM*A4(I,JM1)
G(I,J,1)=0.
G(I,J,2)=YJP*(ZMUA1P*DUP+ZMUA2P*DVP)
> -YJM*(ZMUA1M*DUM+ZMUA2M*DVM)
G(I,J,3)=YJP*(ZMUA3P*DVP+ZMUA2P*DUP)
> -YJM*(ZMUA3M*DVP+ZMUA2M*DUM)
G(I,J,4)=YJP*(0.5*ZMUA1P*DU2P+ZMUA2P*DUVP+0.5*ZMUA3P*DV2P
> +ZKA4P*DTP)
> -YJM*(0.5*ZMUA1M*DU2M+ZMUA2M*DUVM+0.5*ZMUA3M*DV2M
> +ZKA4M*DTM)
*
```

* INSERT THE EXTRA FIRST ORDER TERMS IN CYLINDRICAL
* COORDINATE SYSTEMS, VECTOR H'

H(1)=0.

*
$$H(2) = -\frac{1}{J} \frac{2}{X} * \text{ETA} * D(MU*V) / \text{DETA}$$

*
$$H(3) = -\frac{1}{J} \frac{2}{X} * \text{MU} * DU / \text{DETA} - \frac{2}{3} \frac{1}{Y} * \text{V} * \text{ETA} * DMU / \text{DETA}$$

*
$$H(4) = -\frac{1}{J} \frac{2}{X} * D(MU*U*V) / \text{DETA} - \frac{2}{3} \frac{1}{Y} * \text{ETA} * D(MU*V*V) / \text{DETA}$$

EXJ=1./3.*ETAX(I,J)/RJ(I,J)
EYJ=1./3.*ETAY(I,J)/RJ(I,J)
G(I,J,2)=G(I,J,2)-EXJ*(ZMU(JP1)*V(I,JP1)-ZMU(JM1)*V(I,JM1))
G(I,J,3)=G(I,J,3)+EXJ*ZMU(J)*(U(I,JP1)-U(I,JM1))
> -EYJ*V(I,J)*(ZMU(JP1)-ZMU(JM1))
G(I,J,4)=G(I,J,4)-EXJ*(ZMU(JP1)*U(I,JP1)*V(I,JP1)
> -ZMU(JM1)*U(I,JM1)*V(I,JM1))
> -EYJ*(ZMU(JP1)*V(I,JP1)**2
> -ZMU(JM1)*V(I,JM1)**2)

70 CONTINUE

RETURN

END

SUBROUTINE RHSCL

* RIGHT HAND SIDE CALCULATION

PARAMETER (IZ=60,JZ=40)

COMMON /VECTOR/ DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),
> G(IZ,JZ,4), P(IZ,JZ),T(IZ,JZ),E(IZ,JZ),AMW(IZ,JZ),
> U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ),
> ZMU(JZ),ZMUT(JZ),ZK(JZ)COMMON /COORD/ SAI(X(IZ,JZ),SAI(Y(IZ,JZ),ETAX(IZ,JZ),
> ETAY(IZ,JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),
> DELTAU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),
> A4(IZ,JZ)COMMON /CONS/ EX1,EY1,THETA,CFL,CFL1,OMEGAX,OMEGAY,AIN,AEX,
> RL,RG,AMWO,GAMMAO,REN,PRN,PRNT,TREF,ZMU0,OMEGA,
> PO,TO,TWALL,PB,SUM(4)COMMON /INTEG/ IL,JL,IL1,JL1,NBEG,NEND,NADV,NORD,ITIME,
> IVISC,IWALL,IWRT

DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),EO(IZ,JZ)

EQUIVALENCE (Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
> (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),EO(1,1))

ENTRY RHSEE(II)

*

* RIGHT HAND SIDE CONVECTIVE EULER TERMS E, F

*

* NOTE - SEE ALSO ENTRY RHSH FOR SOURCE CONVECTIVE TERM OF H'

*

I=II
DO 10 J=1,JL
DO 10 K=1,4
DQ(I,J,K)=0.

10 CONTINUE

*

* COMPUTE E(I-1,J), E(I+1,J), F(I,J-1), F(I,J+1) - 1ST ORDER

*

CALL FLXE(I-1)
IF(I.NE.IL) THEN
 CALL FLXE(I+1)
ELSE CALL FLXE(I)
 CALL FLXE(I-2)

END IF

CALL FLXF(I)

DO 20 J=2,JL

DO 20 K=1,4

IF(J.NE.JL) THEN

IF(I.NE.IL) THEN

 DQ(I,J,K)=DQ(I,J,K)+0.5*(F(I+1,J,K)-F(I-1,J,K))
 +0.5*(G(I,J+1,K)-G(I,J-1,K))

ELSE

```

      DQ(I,J,K)=DQ(I,J,K)+(F(I,J,K)-F(I-1,J,K))
      >          +0.5*(G(I,J+1,K)-G(I,J-1,K))
      >          +0.5*(F(I,J,K)-2.0*F(I-1,J,K)+F(I-2,J,K))
      END IF
      ELSE
        IF(I.NE.IL) THEN
          DQ(I,J,K)=DQ(I,J,K)+0.5*(F(I+1,J,K)-F(I-1,J,K))
      >          +(G(I,J,K)-G(I,J-1,K))
      >          +0.5*(G(I,J,K)-2.0*G(I,J-1,K)+G(I,J-2,K))
        ELSE
          DQ(I,J,K)=DQ(I,J,K)+(F(I,J,K)-F(I-1,J,K))
      >          +(G(I,J,K)-G(I,J-1,K))
      >          +0.5*(F(I,J,K)-2.0*F(I-1,J,K)+F(I-2,J,K))
      >          +0.5*(G(I,J,K)-2.0*G(I,J-1,K)+G(I,J-2,K))
        END IF
      END IF
20 CONTINUE
*
* COMPUTE D/E(I-1/2,J)/, D/E(I+1/2,J)/ - 1ST ORDER
*
CALL FLXEP(I-1,1)
CALL FLXEM(I-1,1)
CALL FLXEP(I,1)
CALL FLXEM(I,1)
DO 30 J=2,JL
DO 30 K=1,4
IF(I.NE.IL) THEN
  DQ(I,J,K)=DQ(I,J,K)-0.5*(F(I,J,K)-F(I-1,J,K))
  >          +0.5*(G(I,J,K)-G(I-1,J,K))
ELSE
  DQ(I,J,K)=DQ(I,J,K)-(F(I,J,K)-F(I-1,J,K))
  >          +(G(I,J,K)-G(I-1,J,K))
END IF
30 CONTINUE
*
* COMPUTE D/F(I,J-1/2)/, D/F(I,J+1/2)/ - 1ST ORDER
*
CALL FLXFP(I,1)
CALL FLXFM(I,1)
DO 35 J=2,JL
DO 35 K=1,4
IF(J.NE.JL) THEN
  DQ(I,J,K)=DQ(I,J,K)-0.5*(F(I,J,K)-F(I,J-1,K))
  >          +0.5*(G(I,J,K)-G(I,J-1,K))
ELSE
  DQ(I,J,K)=DQ(I,J,K)-(F(I,J,K)-F(I,J-1,K))
  >          +(G(I,J,K)-G(I,J-1,K))
END IF
35 CONTINUE
*
*           +   -
* COMPUTE DE , DE - 2ND ORDER
*
IF(I.GT.2.AND.I.LT.IL) THEN
  CALL FLXEP(I-2,1)

```

```

    CALL FLXEP(I-1,1)
    CALL FLXEM(I,1)
    CALL FLXEM(I+1,1)
ELSE
END IF
DO 40 J=2,JL
DO 40 K=1,4
IF(I.EQ.2.OR.I.EQ.IL) GO TO 40
IF(I.NE.IL-1) THEN
  DQ(I,J,K)=DQ(I,J,K)+0.5*(F(I-1,J,K)-F(I-2,J,K))
>          -0.5*(G(I+1,J,K)-G(I,J,K))
ELSE
  DQ(I,J,K)=DQ(I,J,K)+0.5*(F(I-1,J,K)-F(I-2,J,K))
>          -(G(I+1,J,K)-G(I,J,K))
END IF
40 CONTINUE
*
```

```

*      +   -
* COMPUTE DF , DF - 2ND ORDER
*
```

```

CALL FLXFP(I,1)
CALL FLXFM(I,1)
DO 45 J=2,JL
DO 45 K=1,4
IF(J.EQ.2.OR.J.EQ.JL) GO TO 45
IF(J.NE.JL-1) THEN
  DQ(I,J,K)=DQ(I,J,K)+0.5*(F(I,J-1,K)-F(I,J-2,K))
>          -0.5*(G(I,J+1,K)-G(I,J,K))
ELSE
  DQ(I,J,K)=DQ(I,J,K)+0.5*(F(I,J-1,K)-F(I,J-2,K))
>          -(G(I,J+1,K)-G(I,J,K))
END IF
45 CONTINUE
RETURN
*****
```

```

***** ENTRY RHSH(II)
*****
```

```

*      SOURCE VECTOR H'
*
*      H(1)=0.
*      H(2)=0.
*      H(3)=(P-4./3.*MU*V/Y)/J
*      H(4)=0.
*
```

```

***** I=II
DO 50 J=2,JL
IF(IVISC.EQ.0) THEN
  R2MY=0.
ELSE
  R2MY=4./3.*ZMU(J)*V(I,J)/(RJ(I,J)*Y(I,J))
END IF
DQ(I,J,3)=DQ(I,J,3)-P(I,J)/RJ(I,J)+IVISC*R2MY
50 CONTINUE
```

```

RETURN
*****
ENTRY RHSVS(II)
*****
*
*      RIGHT HAND SIDE VISCOSUS TERMS
*
*      NOTE - SEE ALSO ENTRY RHSH FOR SOURCE VISCOSUS TERMS OF H'
*****
I=II
CALL FLXSVS(I)
DO 90 J=2,JL1
DO 90 K=2,4
DQ(I,J,K)=DQ(I,J,K)-G(I,J,K)
90 CONTINUE
RETURN
END
SUBROUTINE SMOOTH
*****
*
*      ADD ARTIFICIAL DISSIPATIONAL TERM FOR SAI, ETA - DIRECTION
*****
PARAMETER (IZ=60,JZ=40)
COMMON /VECTOR/ DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),
>           G(IZ,JZ,4), P(IZ,JZ),T(IZ,JZ),E(IZ,JZ),AMW(IZ,JZ),
>           U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ),
>           ZMU(JZ),ZMUT(JZ),ZK(JZ)
COMMON /COORD/ SAI(X(IZ,JZ),SAI(Y(IZ,JZ),ETAX(IZ,JZ),
>           ETAY(IZ,JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),
>           DELTAU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),
>           A4(IZ,JZ)
COMMON /CONS/ EXI,EYI,THETA,CFL,CFL1,OMEGAX,OMEGAY,AIN,AEX,
>           RL,RG,AMWO,GAMMAO,REN,PRN,PRNT,TREF,ZMUO,OMEGA,
>           PO,TO,TWALL,PB,SUM(4)
COMMON /INTEG/ IL,JL,IL1,JL1,NBEG,NEND,NADV,NORD,ITIME,
>           IVISC,IWALL,IWRT
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),EO(IZ,JZ)
EQUIVALENCE (Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
>           (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),EO(1,1))
DIMENSION ADD(4)
*****
ENTRY ADDX
*****
*
*      ADD SAI-DIRECTION 4TH ORDER ARTIFICIAL VISCOSITY
*
COEF=0.1250*OMEGAX
DO 70 J=1,JL
DO 70 I=1,IL
DO 70 I=2,IL
IF(I.EQ.1) GO TO 10
IF(I.EQ.2) GO TO 20
IF(I.EQ.IL1) GO TO 30

```

```

      IF(I.EQ.IL) GO TO 40
      DO 5 K=1,4
 5 ADD(K)=COEF*(Q(I+2,J,K)-4.*Q(I+1,J,K)
    >      +6.*Q(I,J,K)-4.*Q(I-1,J,K)
    >      +Q(I-2,J,K))
      GO TO 50
10 DO 15 K=1,4
      QM=2.*Q(1,J,K)-Q(2,J,K)
      QMM=2.*QM-Q(1,J,K)
15 ADD(K)=COEF*(Q(I+2,J,K)-4.*Q(I+1,J,K)
    >      +6.*Q(I,J,K)-4.*QM+QMM)
      GO TO 50
20 DO 25 K=1,4
      QMM=2.*Q(1,J,K)-Q(2,J,K)
25 ADD(K)=COEF*(Q(I+2,J,K)-4.*Q(I+1,J,K)
    >      +6.*Q(I,J,K)-4.*Q(I-1,J,K)
    >      +QMM)
      GO TO 50
30 DO 35 K=1,4
      QPP=2.*Q(I+1,J,K)-Q(I,J,K)
35 ADD(K)=COEF*(QPP-4.*Q(I+1,J,K)+6.*Q(I,J,K)
    >      -4.*Q(I-1,J,K)+Q(I-2,J,K)
    >      )
      GO TO 50
40 DO 45 K=1,4
      QP=2.*Q(I,J,K)-Q(I-1,J,K)
      QPP=2.*QP-Q(I,J,K)
45 ADD(K)=COEF*(QPP-4.*QP+6.*Q(I,J,K)-4.*
    >      Q(I-1,J,K)+Q(I-2,J,K))
50 CONTINUE
      DO 60 K=1,4
60 DQ(I,J,K)=DQ(I,J,K)-ADD(K)/RJ(I,J)*Y(I,J)
70 CONTINUE
      RETURN
*****
***** ENTRY ADDY *****
*****
*      ADD ETA-DIRECTION 4TH ORDER ARTIFICIAL VISCOSITY
*
      COEF=0.1250*OMEGAY
      DO 170 I=1,IL
      DO 170 I=2,IL
      DO 170 J=1,JL
      IF(J.EQ.1) GO TO 110
      IF(J.EQ.2) GO TO 120
      IF(J.EQ.JL1) GO TO 130
      IF(J.EQ.JL) GO TO 140
      DO 105 K=1,4
105 ADD(K)=COEF*(Q(I,J+2,K)-4.*Q(I,J+1,K)
    >      +6.*Q(I,J,K)-4.*Q(I,J-1,K)
    >      +Q(I,J-2,K))
      GO TO 150
110 DO 115 K=1,4
      QM=2.*Q(I,1,K)-Q(I,2,K)

```

```

QMM=2.*QM-Q(I,1,K)
115 ADD(K)=COEF*(Q(I,J+2,K)-4.*Q(I,J+1,K)
> +6.*Q(I,J,K)-4.*QM+QMM)
GO TO 150
120 DO 125 K=1,4
QMM=2.*Q(I,1,K)-Q(I,2,K)
125 ADD(K)=COEF*(Q(I,J+2,K)-4.*Q(I,J+1,K)
> +6.*Q(I,J,K)-4.*Q(I,J-1,K)
> +QMM)
GO TO 150
130 DO 135 K=1,4
QPP=2.*Q(I,J+1,K)-Q(I,J,K)
135 ADD(K)=COEF*(QPP-4.*Q(I,J+1,K)+6.*Q(I,J,K)
> -4.*Q(I,J-1,K)+Q(I,J-2,K)
> )
GO TO 150
140 DO 145 K=1,4
QP=2.*Q(I,J,K)-Q(I,J-1,K)
QPP=2.*QP-Q(I,J,K)
145 ADD(K)=COEF*(QPP-4.*QP+6.*Q(I,J,K)-4.*
> Q(I,J-1,K)+Q(I,J-2,K))
150 CONTINUE
DO 160 K=1,4
160 DQ(I,J,K)=DQ(I,J,K)-ADD(K)/RJ(I,J)*Y(I,J)
170 CONTINUE
RETURN
END
SUBROUTINE UGAS3(E,RHO,ZMU)
```

INPUTS FOR SUBROUTINE :

E = SPECIFIC INTERNAL ENERGY, IN (M/S)**2
RHO = DENSITY, IN KG/M**3

OUTPUT :

ZMU = DYNAMIC VISCOSITY, IN KG/M/S

```

DATA RHOO,E0/1.243,78408.4E00/
Z= ALOG10(E/E0)
Y= ALOG10(RHO/RHOO)
IF (Z.GT.0.67E00) GO TO 10
GAS1=4.84547E-01+4.67135E-01*Z
GAS2=(5.71205E-04-1.43629E-03*Z)*Y
GAS3=(2.55110E00-2.33472E-04*Y-1.44102E00*Z)*Z*Z
GAS4=(2.53416E-04-4.72375E-04*Z+1.86899E-05*Y)*Y*Y
F=GAS1+GAS2+GAS3+GAS4
GO TO 90
10 IF (Z.GT.1.75E00) GO TO 20
GAS1=-3.71666E01+6.67883E01*Z
GAS2=(-2.43998E00+2.12309E00*Z)*Y
GAS3=(-3.69259E01-3.08426E-01*Y+7.36486E00*Z)*Z*Z
GAS4=(-1.46446E-01+7.54423E-02*Z-2.91464E-03*Y)*Y*Y
GAS5=3.61757E01-6.11102E01*Z
GAS6=(2.40531E00-2.05914E00*Z)*Y
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GAS7=(3.23911E01+2.79149E-01*Y-5.07640E00*Z)*Z*Z
GAS8=(1.37916E-01-6.72041E-02*Z+2.61987E-03*Y)*Y*Y
GAS9=EXP(-3.433E01-1.823E00*Y+2.499E01*Z+6.503E-01*Z*Y)
GO TO 80
20 IF (Z.GT.2.50E00) GO TO 30
GAS1=-1.65147E02+2.11028E02*Z
GAS2=(-4.70948E00+2.78258E00*Z)*Y
GAS3=(-8.78308E01-1.28671E-01*Y+1.27639E01*Z)*Z*Z
GAS4=(-3.19867E-01+1.73179E-01*Z+3.86106E-03*Y)*Y*Y
GAS5=2.30407E02-2.98055E02*Z
GAS6=(-6.18307E00+8.44595E00*Z)*Y
GAS7=(1.26933E02-2.61671E00*Y-1.77257E01*Z)*Z*Z
GAS8=(-2.30229E-02+2.25458E-02*Z-4.41072E-03*Y)*Y*Y
GAS9=EXP(-6.882E01+8.824E00*Y+3.203E01*Z-5.359E00*Z*Y)
GO TO 80
30 IF (Z.GT.2.85E00) GO TO 40
GAS1=-7.09274E03+7.13648E03*Z
GAS2=(-2.46014E02+1.65826E02*Z)*Y
GAS3=(-2.37952E03-2.75487E01*Y+2.63465E02*Z)*Z*Z
GAS4=(-3.49744E00+1.28641E00*Z-3.13711E-03*Y)*Y*Y
GAS5=5.26158E03-4.96701E03*Z
GAS6=(2.03138E02-1.32984E02*Z)*Y
GAS7=(1.52424E03+2.15081E01*Y-1.50450E02*Z)*Z*Z
GAS8=(3.32432E00-1.15997E00*Z+1.14862E-02*Y)*Y*Y
GAS9=EXP(-3.594E02-3.763E01*Y+1.319E02*Z+1.348E01*Z*Y)
F=GAS1+GAS2+GAS3+GAS4
GO TO 80
40 IF (Z.GT.3.15E00) GO TO 50
GAS1=-1.27748E03+1.29400E03*Z
GAS2=(-3.60724E01+2.63194E01*Z)*Y
GAS3=(-4.22958E02-4.38228E00*Y+4.50571E01*Z)*Z*Z
GAS4=(-4.74425E-01+2.89684E-01*Z+1.64048E-02*Y)*Y*Y
F=GAS1+GAS2+GAS3+GAS4
GO TO 90
50 IF (Y.GT.-3.80E00) GO TO 70
IF (Z.GT.3.19E00) GO TO 60
GAS1=4.55919E03-4.21057E03*Z
GAS2=(1.03001E01-2.63478E01*Z)*Y
GAS3=(1.29069E03+6.59587E00*Y-1.31413E02*Z)*Z*Z
GAS4=(-8.28137E00+1.9827E00*Z-1.7287E-01*Y)*Y*Y
F=GAS1+GAS2+GAS3+GAS4
GO TO 90
60 Z=E/E0
GAS1=-4.41792E02+9.7986E-02*Z
GAS2=(-3.03148E02+7.6065E-03*Z)*Y
GAS3=(-5.5711E-05-3.52836E-06*Y+8.86148E-09*Z)*Z*Z
GAS4=(-7.561E01-4.76816E-04*Z-6.48859E00*Y)*Y*Y
GAS5=6.72387E04+3.28398E00*Z
GAS6=(3.55009E04+2.72616E00*Z)*Y
GAS7=(2.13714E-03+3.42377E-04*Y-6.84897E-08*Z)*Z*Z
GAS8=(6.50886E03+3.8056E-01*Z+4.14116E02*Y)*Y*Y
GAS9=EXP(2.978E01+5.415E00*Y+1.713E-03*Z+3.115E-04*Y*Z)
F=GAS1+GAS2+GAS3+GAS4+(GAS5+GAS6+GAS7+GAS8)/(1.0-GAS9)
GO TO 90
70 GAS1=-6.4029E03+6.24254E03*Z

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GAS2=(1.03279E02-8.73181E01*Z)*Y
GAS3=(-2.02865E03+1.71878E01*Y+2.19907E02*Z)*Z*Z
GAS4=(-1.22397E01+3.57830E00*Z-1.27953E-01*Y)*Y*Y
F=GAS1+GAS2+GAS3+GAS4
GO TO 90
80 F=GAS1+GAS2+GAS3+GAS4+(GAS5+GAS6+GAS7+GAS8)/(1.0+GAS9)
90 ZMU=1.748583E-05*F
RETURN
END
SUBROUTINE UGAS4(E,RHO,ZK)

```

INPUTS FOR SUBROUTINE :

E = SPECIFIC INTERNAL ENERGY, IN (M/S)**2
 RHO = DENSITY, IN KG/M**3

OUTPUT :

ZK = COEFFICIENT OF THERMAL CONDUCTIVITY, IN J/(KELVIN*M*S)

```

DATA RHOO,E0/1.243E00,78408E00/
Z=ALOG10(E/E0)
Y=ALOG10(RHO/RHOO)
IF (Z.GT.0.65E00) GO TO 10
GAS1=1.8100369E-01+4.8126802E00*Z
GAS2=(-2.7231116E-02+1.2691337E-01*Z)*Y
GAS3=(-8.9913034E00-1.2624085E-01*Y+8.9649105E00*Z)*Z*Z
GAS4=(-4.7198236E-03+9.2328079E-03*Z-2.9488327E-04*Y)*Y*Y
F=GAS1+GAS2+GAS3+GAS4
GO TO 200
10 IF (Y.GT.-1.00E00) GO TO 130
IF (Y.GT.-3.00E00) GO TO 70
IF (Z.GT.1.25E00) GO TO 20
GAS1=-1.05935E04+2.31470E04*Z
GAS2=(-7.41294E02+1.21724E03*Z)*Y
GAS3=(-1.67601E04-4.43184E02*Y+4.06631E03*Z)*Z*Z
GAS4=(1.35105E01+4.94914E00*Z+1.55386E00*Y)*Y*Y
GAS5=1.06032E04-2.31560E04*Z
GAS6=(7.46951E02-1.22465E03*Z)*Y
GAS7=(1.67604E04+4.45919E02*Y-4.06258E03*Z)*Z*Z
GAS8=(-1.28615E01-5.32398E00*Z-1.52956E00*Y)*Y*Y
GAS9=EXP(-4.219E01-4.687E00*Y+2.812E01*Z+3.125E00*Y*Z)
F=GAS1+GAS2+GAS3+GAS4+(GAS5+GAS6+GAS7+GAS8)/(1.0-GAS9)
GO TO 200
20 IF (Z.GT.1.775E00) GO TO 30
GAS1=3.79375E03-7.40351E03*Z
GAS2=(3.29698E02-3.55916E02*Z)*Y
GAS3=(4.77122E03+1.00241E02*Y-1.00740E03*Z)*Z*Z
GAS4=(1.97061E01-8.42554E00*Z+4.80494E-01*Y)*Y*Y
GAS5=-4.53603E03+9.05605E03*Z
GAS6=(-4.95870E02+6.33563E02*Z)*Y
GAS7=(-5.95317E03-2.05442E02*Y+1.28945E03*Z)*Z*Z
GAS8=(-2.00087E01+1.18851E01*Z-1.71735E-01*Y)*Y*Y
GAS9=EXP(-3.318E01+3.158E-01*Y+1.863E01*Z-1.035E00*Y*Z)
GO TO 190

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30 IF (Z.GT.1.93E00) GO TO 40
 GAS1=2.06651875E05-3.165645E05*Z
 GAS2=(-3.07322021E02+4.57036377E02*Z)*Y
 GAS3=(1.61824937E05-1.55508453E02*Y-2.7603957E04*Z)*Z*Z
 GAS4=(1.92260265E00-2.24788094E00*Z-3.06226015E-01*Y)*Y*Y
 GAS5=-2.06564312E05+3.18191312E05*Z
 GAS6=(2.17542285E03-2.46670776E03*Z)*Y
 GAS7=(-1.63597062E05+7.16753174E02*Y+2.80926367E04*Z)*Z*Z
 GAS8=(3.39526825E01-7.53815645E00*Z+1.91214371E00*Y)*Y*Y
 GAS9=EXP(-3.924E02-5.206E01*Y+2.054E02*Z+2.679E01*Y*Z)
 GO TO 190

40 IF (Z.GT.2.60E00) GO TO 50
 GAS1=7.1572625E04-9.2471625E04*Z
 GAS2=(1.9646323E03-2.0280527E03*Z)*Y
 GAS3=(3.9446105E04+4.5673853E02*Y-5.5728672E03*Z)*Z*Z
 GAS4=(-9.2131958E01+1.2724541E01*Z-5.0568476E00*Y)*Y*Y
 GAS5=-3.2910781E04+4.2551211E04*Z
 GAS6=(1.4566331E03-2.2653745E03*Z)*Y
 GAS7=(-1.9476277E04+8.4370288E02*Y+3.2389702E03*Z)*Z*Z
 GAS8=(-1.3324594E02+1.0591533E02*Z+5.8639469E00*Y)*Y*Y
 GAS9=EXP(4.917E01+2.415E01*Y-2.455E01*Z-1.181E01*Y*Z)
 GO TO 190

50 IF (Z.GT.2.69E00) GO TO 60
 GAS1=1.145683E06-1.237525E06*Z
 GAS2=(1.4024508E04-9.3467227E03*Z)*Y
 GAS3=(4.4593056E05+1.533074E03*Y-5.3608352E04*Z)*Z*Z
 GAS4=(2.8485107E02-1.0968916E02*Z-1.0955791E00*Y)*Y*Y
 GAS5=-1.752087E06+1.79675E06*Z
 GAS6=(-1.3278737E05+9.8215562E04*Z)*Y
 GAS7=(-6.0791744E05-1.811943E04*Y+6.7709875E04*Z)*Z*Z
 GAS8=(-1.3384084E03+5.2707324E02*Z+2.5904894E00*Y)*Y*Y
 GAS9=EXP(-1.798E02+7.371E00*Y+6.731E01*Z-3.205E00*Y*Z)
 GO TO 190

60 GAS1=-8.5499625E04+1.1739656E05*Z
 GAS2=(6.4563168E04-3.9551203E04*Z)*Y
 GAS3=(-4.8170254E04+6.0816055E03*Y+6.2052031E03*Z)*Z*Z
 GAS4=(2.3473167E-01+1.8871567E01*Z+4.0757723E00*Y)*Y*Y
 GAS5=5.8546883E04-9.4634875E04*Z
 GAS6=(-6.6513812E04+4.0899945E04*Z)*Y
 GAS7=(4.2127227E04-6.3717305E03*Y-5.7495195E03*Z)*Z*Z
 GAS8=(-1.0260344E00-5.343277E01*Z-1.1017392E01*Y)*Y*Y
 GAS9=EXP(5.411E00+1.162E01*Y-1.082E00*Z-3.391E00*Y*Z)
 F=GAS1+GAS2+GAS3+GAS4+(GAS5+GAS6+GAS7+GAS8)/(1.0-GAS9)
 GO TO 200

70 IF (Z.GT.1.29E00) GO TO 80
 GAS1=-1.22493E04+2.41071E04*Z
 GAS2=(-1.61829E03+2.22535E03*Z)*Y
 GAS3=(-1.59261E04-7.53213E02*Y+3.53376E03*Z)*Z*Z
 GAS4=(1.98026E00+5.18483E00*Z+1.47851E00*Y)*Y*Y
 GAS5=1.22486E04-2.41023E04*Z
 GAS6=(1.61810E03-2.22571E03*Z)*Y
 GAS7=(1.59235E04+7.53746E02*Y-3.53168E03*Z)*Z*Z
 GAS8=(-2.15482E00-5.05115E00*Z-1.48795E00*Y)*Y*Y
 GAS9=EXP(-3.111E01-4.444E00*Y+1.944E01*Z+2.778E00*Y*Z)
 F=GAS1+GAS2+GAS3+GAS4+(GAS5+GAS6+GAS7+GAS8)/(1.0-GAS9)

GO TO 200

80 IF (Z.GT.1.85E00) GO TO 90
 GAS1=3.18060E03-6.69664E03*Z
 GAS2=(4.33382E01-2.14649E02*Z)*Y
 GAS3=(4.41377E03+9.41359E01*Y-9.29758E02*Z)*Z*Z
 GAS4=(-3.62190E01+1.15538E01*Z-2.14621E00*Y)*Y*Y
 GAS5=-5.98764E03+1.29243E04*Z
 GAS6=(-2.72261E02+5.42378E02*Z)*Y
 GAS7=(-9.03293E03-2.11787E02*Y+2.07831E03*Z)*Z*Z
 GAS8=(2.74179E01-5.68578E00*Z+1.91217E00*Y)*Y*Y
 GAS9=EXP(-1.854E01+7.11E00*Y+1.068E01*Z-5.449E00*Y*Z)
 GO TO 190

90 IF (Z.GT.2.0E00) GO TO 100
 GAS1=5.14024E04-7.52733E04*Z
 GAS2=(-3.30889E02+3.11550E02*Z)*Y
 GAS3=(3.66539E04-7.41227E01*Y-5.93015E03*Z)*Z*Z
 GAS4=(-4.84164E01+2.23133E01*Z-9.19118E-01*Y)*Y*Y
 GAS5=-1.80898E05+2.82532E05*Z
 GAS6=(-1.01053E03+9.75576E02*Z)*Y
 GAS7=(-1.47220E05-2.33631E02*Y+2.55940E04*Z)*Z*Z
 GAS8=(3.28681E00-1.76588E00*Z-1.54962E-01*Y)*Y*Y
 GAS9=EXP(-4.104E01+6.507E01*Y+2.083E01*Z-3.472E01*Y*Z)
 GO TO 190

100 IF (Z.GT.2.58E00) GO TO 110
 GAS1=5.1131824E04-6.664875E04*Z
 GAS2=(2.02171E03-1.9306292E03*Z)*Y
 GAS3=(2.8762395E04+4.3353467E02*Y-4.1064609E03*Z)*Z*Z
 GAS4=(-8.4970047E01+1.7925919E01*Z-6.2576542E00*Y)*Y*Y
 GAS5=-6.2768156E04+8.6015875E04*Z
 GAS6=(-1.0002036E03+6.2537280E02*Z)*Y
 GAS7=(-3.957827E04-3.8467377E01*Y+6.12953E03*Z)*Z*Z
 GAS8=(-1.0591702E02+7.636142E01*Z+5.938859E00*Y)*Y*Y
 GAS9=EXP(-3.901E00+2.418E01*Y+1.374E00*Z-1.145E01*Y*Z)
 GO TO 190

110 IF (Z.GT.2.73E00) GO TO 120
 GAS1=1.0088046E06-1.086321E06*Z
 GAS2=(1.3844801E04-9.7268516E03*Z)*Y
 GAS3=(3.8985325E05+1.7091665E03*Y-4.6621066E04*Z)*Z*Z
 GAS4=(1.4840726E02-5.2645004E01*Z-1.5477133E-01*Y)*Y*Y
 GAS5=-1.073351E06+1.14571E06*Z
 GAS6=(-1.9343957E04+1.3366211E04*Z)*Y
 GAS7=(-4.0670987E05-2.2955198E03*Y+4.7999871E04*Z)*Z*Z
 GAS8=(-4.1016724E02+1.4994148E02*Z-1.9779787E00*Y)*Y*Y
 GAS9=EXP(-1.026E02+6.302E01*Y+3.819E01*Z-2.431E01*Y*Z)
 GO TO 190

120 GAS1=-9.6638500E04+1.3206488E04*Z
 GAS2=(-4.7458105E04+2.3596875E04*Z)*Y
 GAS3=(1.8602773E04-2.306802E03*Y-4.0413552E03*Z)*Z*Z
 GAS4=(-5.3564258E03+2.2433904E03*Z+2.5188145E02*Y)*Y*Y
 GAS5=1.0962581E05-2.990116E04*Z
 GAS6=(4.7883496E04-2.3785383E04*Z)*Y
 GAS7=(-1.1753969E04+2.2905522E03*Y+3.1304399E03*Z)*Z*Z
 GAS8=(5.473418E03-2.3208018E03*Z-2.6570068E02*Y)*Y*Y
 GAS9=EXP(-3.107E01+1.082E01*Y+1.047E01*Z-3.047E00*Y*Z)
 F=GAS1+GAS2+GAS3+GAS4+(GAS5+GAS6+GAS7+GAS8)/(1.0-GAS9)

GO TO 200

130 IF (Z.GT.1.40E00) GO TO 140
 GAS1=-1.58386E03+3.49223E03*Z
 GAS2=(-8.39834E02+1.09565E03*Z)*Y
 GAS3=(-2.56175E03-3.56197E02*Y+6.25145E02*Z)*Z*Z
 GAS4=(-1.22407E01+7.65634E00*Z+2.58235E-01*Y)*Y*Y
 GAS5=1.58025E03-3.47664E03*Z
 GAS6=(8.39588E02-1.09490E03*Z)*Y
 GAS7=(2.54682E03+3.55674E02*Y-6.18504E02*Z)*Z*Z
 GAS8=(1.20843E01-7.44857E00*Z-2.91202E-01*Y)*Y*Y
 GAS9=EXP(-2.171E01-4.342E00*Y+1.316E01*Z+2.632E00*Y*Z)
 F=GAS1+GAS2+GAS3+GAS4+(GAS5+GAS6+GAS7+GAS8)/(1.0-GAS9)
 GO TO 200

140 IF (Z.GT.1.91E00) GO TO 150
 GAS1=7.89255E02-1.91743E03*Z
 GAS2=(3.59227E02-4.44070E02*Z)*Y
 GAS3=(1.39463E03+1.34083E02*Y-3.13446E02*Z)*Z*Z
 GAS4=(1.90681E01-1.09285E01*Z+4.24933E-02*Y)*Y*Y
 GAS5=-1.31401E03+3.13134E03*Z
 GAS6=(-5.18755E02+6.80268E02*Z)*Y
 GAS7=(-2.32493E03-2.21393E02*Y+5.52563E02*Z)*Z*Z
 GAS8=(-3.32001E01+2.11819E01*Z-4.75163E-01*Y)*Y*Y
 GAS9=EXP(-5.025E01-8.412E00*Y+2.982E01*Z+3.509E00*Y*Z)
 GO TO 190

150 IF (Z.GT.2.05E00) GO TO 160
 GAS1=3.58691E04-5.16852E04*Z
 GAS2=(-6.30189E02+6.63314E02*Z)*Y
 GAS3=(2.47471E04-1.73538E02*Y-3.93167E03*Z)*Z*Z
 GAS4=(-4.23871E01+2.08048E01*Z-1.05512E00*Y)*Y*Y
 GAS5=-1.10522E05+1.67591E05*Z
 GAS6=(4.61877E03-4.94930E03*Z)*Y
 GAS7=(-8.46558E04+1.32441E03*Y+1.42438E04*Z)*Z*Z
 GAS8=(2.25065E01-1.10316E01*Z+9.62887E-01*Y)*Y*Y
 GAS9=EXP(-1.681E02+7.063E01*Y+8.75E01*Z-3.75E01*Y*Z)
 GO TO 190

160 IF (Z.GT.2.57E00) GO TO 170
 GAS1=3.1899562E04-4.2186664E04*Z
 GAS2=(2.3055603E03-1.9897017E03*Z)*Y
 GAS3=(1.849998E04+4.2561816E02*Y-2.6808696E03*Z)*Z*Z
 GAS4=(-1.6195114E01+5.8640623E00*Z-3.6172504E00*Y)*Y*Y
 GAS5=-5.7594039E04+7.9328437E04*Z
 GAS6=(-1.9275989E03+1.6730544E03*Z)*Y
 GAS7=(-3.6473008E04-3.6100732E02*Y+5.597543E03*Z)*Z*Z
 GAS8=(-7.920808E01+4.0542084E01*Z+2.1495867E00*Y)*Y*Y
 GAS9=EXP(-5.733E01+2.088E01*Y+2.592E01*Z-9.793E00*Y*Z)
 GO TO 190

170 IF (Z.GT.2.75E00) GO TO 180
 GAS1=7.0838087E05-7.5619919E05*Z
 GAS2=(3.9503091E03-2.7381802E03*Z)*Y
 GAS3=(2.6888181E05+4.7728687E02*Y-3.183816E04*Z)*Z*Z
 GAS4=(-1.2532251E02+4.7734787E01*Z-4.0148029E00*Y)*Y*Y
 GAS5=-2.5216325E05+2.1727769E05*Z
 GAS6=(9.2882383E03-7.780918E03*Z)*Y
 GAS7=(-5.6539297E04+1.6120212E03*Y+3.9419248E03*Z)*Z*Z
 GAS8=(1.8537296E02-7.1010757E01*Z+1.1307096E00*Y)*Y*Y

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GAS9=EXP(-1.786E02+2.18E-01*Y+6.714E01*Z-4.739E-01*Y*Z)
GO TO 190
180 GAS1=3.1855037E05-3.3041156E05*Z
GAS2=(2.2983352E04-1.6623461E04*Z)*Y
GAS3=(1.13848E05+3.0098223E03*Y-1.3020133E04*Z)*Z*Z
GAS4=(-1.8599039E02+6.9840683E01*Z-7.7371645E00*Y)*Y*Y
F=GAS1+GAS2+GAS3+GAS4
GO TO 200
190 F=GAS1+GAS2+GAS3+GAS4+(GAS5+GAS6+GAS7+GAS8)/(1.0+GAS9)
200 ZK=1.87915E-02*F
RETURN
END
FUNCTION FAMW(R,T)
COMMON /INPL/ X1(9),Y1(9),F1(9,9),X2(9),Y2(9),F2(9,9),
> X3(9),Y3(9),F3(9,9),X4(9),Y4(9),F4(9,9),
> X5(9),Y5(9),F5(9,9),X6(9),Y6(9),F6(9,9),
> X7(9),Y7(9),F7(9,9)
IF(R.LT.X1(1)) II=1
IF(R.GT.X1(9)) II=8
DO 1 I=1,8
IF(R.GE.X1(I).AND.R.LE.X1(I+1)) THEN
  II=I
  GO TO 2
ELSE
END IF
1 CONTINUE
2 CONTINUE
IF(II.EQ.0) THEN
  WRITE (6,500) R,X1(1),X1(9)
500  FORMAT(//2X,'R IS OUT OF BOUNDARIES, CALLED FROM FAMW'/
> 2X,'R=',E12.5,2X,'X1(1)=',E12.5,2X,'X1(9)=',E12.5)
  STOP
ELSE
END IF
IF(T.LT.Y1(1)) JJ=1
IF(T.GT.Y1(8)) JJ=8
DO 3 J=1,8
IF(T.GE.Y1(J).AND.T.LE.Y1(J+1)) THEN
  JJ=J
  GO TO 4
ELSE
END IF
3 CONTINUE
4 CONTINUE
IF(JJ.EQ.0) THEN
  WRITE (6,501) T,Y1(1),Y1(9)
501  FORMAT(//2X,'T IS OUT OF BOUNDARIES, CALLED FROM FAMW'/
> 2X,'T=',E12.5,2X,'Y1(1)=',E12.5,2X,'Y1(9)=',E12.5)
  STOP
ELSE
END IF
I=II
J=JJ
IF(II.EQ.0) I=II+1
IF(II.EQ.8) I=II-1

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IF(JJ.EQ.0) JJ=JJ+1
IF(JJ.EQ.8) JJ=JJ-1
AMW1=F1(I,J)
> +(F1(I+1,J)-F1(I,J))/(X1(I+1)-X1(I))*(R-X1(I))
AMW2=F1(I,J+1)
> +(F1(I+1,J+1)-F1(I,J+1))/(X1(I+1)-X1(I))*(R-X1(I))
AMW=AMW1+(AMW2-AMW1)/(Y1(J+1)-Y1(J))*(T-Y1(J))
FAMW=AMW
RETURN
END
FUNCTION FE(R,T)
COMMON /INPL/ X1(9),Y1(9),F1(9,9),X2(9),Y2(9),F2(9,9),
> X3(9),Y3(9),F3(9,9),X4(9),Y4(9),F4(9,9),
> X5(9),Y5(9),F5(9,9),X6(9),Y6(9),F6(9,9),
> X7(9),Y7(9),F7(9,9)
IF(R.LT.X4(1)) II=0
IF(R.GT.X4(9)) II=8
DO 1 I=1,8
IF(R.GE.X4(I).AND.R.LE.X4(I+1)) THEN
  II=I
  GO TO 2
ELSE
END IF
1 CONTINUE
2 CONTINUE
IF(II.EQ.0) THEN
  WRITE (6,500) R,X4(1),X4(9)
500  FORMAT(//2X,'R IS OUT OF BOUNDARIES, CALLED FROM FE'/
> 2X,'R=',E12.5,2X,'X4(1)=',E12.5,2X,'X4(9)=',E12.5)
  STOP
ELSE
END IF
IF(T.LT.Y4(1)) JJ=0
IF(T.GT.Y4(9)) JJ=8
DO 3 J=1,8
IF(T.GE.Y4(J).AND.T.LE.Y4(J+1)) THEN
  JJ=J
  GO TO 4
ELSE
END IF
3 CONTINUE
4 CONTINUE
IF(JJ.EQ.0) THEN
  WRITE (6,501) T,Y4(1),Y4(9)
501  FORMAT(//2X,'T IS OUT OF BOUNDARIES, CALLED FROM FE'/
> 2X,'T=',E12.5,2X,'Y4(1)=',E12.5,2X,'Y4(9)=',E12.5)
  STOP
ELSE
END IF
I=II
J=JJ
IF(II.EQ.0) I=II+1
IF(II.EQ.8) I=II-1
IF(JJ.EQ.0) J=JJ+1
IF(JJ.EQ.8) J=JJ-1

```

```

E1=F4(I,J)
> +(F4(I+1,J)-F4(I,J))/(X4(I+1)-X4(I))*(R-X4(I))
IF(E1.LT.F4(1,J)) E1=F4(1,J)
IF(E1.GT.F4(9,J)) E1=F4(9,J)
E2=F4(I,J+1)
> +(F4(I+1,J+1)-F4(I,J+1))/(X4(I+1)-X4(I))*(R-X4(I))
IF(E2.LT.F4(1,J+1)) E2=F4(1,J+1)
IF(E2.GT.F4(9,J+1)) E2=F4(9,J+1)
E=E1+(E2-E1)/(Y4(J+1)-Y4(J))*(T-Y4(J))
IF(E.LT.F4(I,1)) E=F4(I,1)
IF(E.GT.F4(I,9)) E=F4(I,9)
FE=E
RETURN
END
FUNCTION FT(R,E)
COMMON /INPL/ X1(9),Y1(9),F1(9,9),X2(9),Y2(9),F2(9,9),
> X3(9),Y3(9),F3(9,9),X4(9),Y4(9),F4(9,9),
> X5(9),Y5(9),F5(9,9),X6(9),Y6(9),F6(9,9),
> X7(9),Y7(9),F7(9,9)
IF(R.LT.X5(1)) II=0
IF(R.GT.X5(9)) II=8
DO 1 I=1,8
IF(R.GE.X5(I).AND.R.LE.X5(I+1)) THEN
  II=I
  GO TO 2
ELSE
END IF
1 CONTINUE
2 CONTINUE
IF(II.EQ.0) THEN
  WRITE (6,500) R,X5(1),X5(9)
500  FORMAT(//2X,'R IS OUT OF BOUNDARIES, CALLED FROM FT'/
> 2X,'R=',E12.5,2X,'X5(1)=',E12.5,2X,'X5(9)=',E12.5)
  STOP
ELSE
END IF
IF(E.LT.Y5(1)) JJ=0
IF(E.GT.Y5(9)) JJ=8
DO 3 J=1,8
IF(E.GE.Y5(J).AND.E.LE.Y5(J+1)) THEN
  JJ=J
  GO TO 4
ELSE
END IF
3 CONTINUE
4 CONTINUE
IF(JJ.EQ.0) THEN
  WRITE (6,501) E,Y5(1),Y5(9)
501  FORMAT(//2X,'E IS OUT OF BOUNDARIES, CALLED FROM FT'/
> 2X,'E=',E12.5,2X,'Y5(1)=',E12.5,2X,'Y5(9)=',E12.5)
  STOP
ELSE
END IF
I=II
J=JJ

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IF(II.EQ.0) II=II+1
IF(II.EQ.8) II=II-1
IF(JJ.EQ.0) JJ=JJ+1
IF(JJ.EQ.8) JJ=JJ-1
T1=F5(I,J)
> +(F5(I+1,J)-F5(I,J))/(X5(I+1)-X5(I))*(R-X5(I))
T2=F5(I,J+1)
> +(F5(I+1,J+1)-F5(I,J+1))/(X5(I+1)-X5(I))*(R-X5(I))
T=T1+(T2-T1)/(Y5(J+1)-Y5(J))*(E-Y5(J))
FT=T
RETURN
END
FUNCTION FZMU(R,E)
CALL UGAS3(E,R,ZMU)
FZMU=ZMU
RETURN
END
FUNCTION FZK(R,E)
CALL UGAS4(E,R,ZK)
FZK=ZK
RETURN
END
FUNCTION FDMDRT(R,T)
COMMON /INPL/ X1(9),Y1(9),F1(9,9),X2(9),Y2(9),F2(9,9),
> X3(9),Y3(9),F3(9,9),X4(9),Y4(9),F4(9,9),
> X5(9),Y5(9),F5(9,9),X6(9),Y6(9),F6(9,9),
> X7(9),Y7(9),F7(9,9)
IF(R.LT.X2(1)) II=0
IF(R.GT.X2(9)) II=8
DO 1 I=1,8
IF(R.GE.X2(I).AND.R.LE.X2(I+1)) THEN
  II=I
  GO TO 2
ELSE
END IF
1 CONTINUE
2 CONTINUE
IF(II.EQ.0) THEN
  WRITE (6,500) R,X2(1),X2(9)
500  FORMAT('//2X,'R IS OUT OF BOUNDARIES, CALLED FROM FDMDRT'/
> 2X,'R=' ,E12.5,2X,'X2(1)' ,E12.5,2X,'X2(9)' ,E12.5)
  STOP
ELSE
END IF
IF(T.LT.Y2(1)) JJ=0
IF(T.GT.Y2(9)) JJ=8
DO 3 J=1,8
IF(T.GE.Y2(J).AND.T.LE.Y2(J+1)) THEN
  JJ=J
  GO TO 4
ELSE
END IF
3 CONTINUE
4 CONTINUE
IF(JJ.EQ.0) THEN

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```

      WRITE (6,501) T,Y2(1),Y2(9)
501  FORMAT('//2X, 'T IS OUT OF BOUNDARIES, CALLED FROM FDMDRT'/
>   2X, 'T=',E12.5,2X,'Y2(1)=',E12.5,2X,'Y2(9)=',E12.5)
      STOP
      ELSE
      END IF
      I=II
      J=JJ
      IF(II.EQ.0) I=II+1
      IF(II.EQ.8) I=II-1
      IF(JJ.EQ.0) J=JJ+1
      IF(JJ.EQ.8) J=JJ-1
      DMDRT1=F2(I,J)
>   +(F2(I+1,J)-F2(I,J))/(X2(I+1)-X2(I))*(R-X2(I))
      DMDRT2=F2(I,J+1)
>   +(F2(I+1,J+1)-F2(I,J+1))/(X2(I+1)-X2(I))*(R-X2(I))
      DMDRT=DMDRT1+(DMDRT2-DMDRT1)/(Y2(J+1)-Y2(J))*(T-Y2(J))
      FDMDRT=DMDRT
      RETURN
      END
      FUNCTION FDMDTR(R,T)
      COMMON /INPL/ X1(9),Y1(9),F1(9,9),X2(9),Y2(9),F2(9,9),
>                  X3(9),Y3(9),F3(9,9),X4(9),Y4(9),F4(9,9),
>                  X5(9),Y5(9),F5(9,9),X6(9),Y6(9),F6(9,9),
>                  X7(9),Y7(9),F7(9,9)
      IF(R.LT.X3(1)) II=0
      IF(R.GT.X3(9)) II=8
      DO 1 I=1,8
      IF(R.GE.X3(I).AND.R.LE.X3(I+1)) THEN
          II=I
          GO TO 2
      ELSE
      END IF
1 CONTINUE
2 CONTINUE
      IF(II.EQ.0) THEN
          WRITE (6,500) R,X3(1),X3(9)
500  FORMAT('//2X, 'R IS OUT OF BOUNDARIES, CALLED FROM FDMDTR'/
>   2X, 'R=',E12.5,2X,'X3(1)=',E12.5,2X,'X3(9)=',E12.5)
          STOP
      ELSE
      END IF
      IF(T.LT.Y3(1)) JJ=0
      IF(T.GT.Y3(9)) JJ=8
      DO 3 J=1,8
      IF(T.GE.Y3(J).AND.T.LE.Y3(J+1)) THEN
          JJ=J
          GO TO 4
      ELSE
      END IF
3 CONTINUE
4 CONTINUE
      IF(JJ.EQ.0) THEN
          WRITE (6,501) T,Y3(1),Y3(9)
501  FORMAT('//2X, 'T IS OUT OF BOUNDARIES, CALLED FROM FDMDTR'/

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    > 2X, 'T-', E12.5, 2X, 'Y3(1)=', E12.5, 2X, 'Y3(9)=', E12.5)
      STOP
    ELSE
  END IF
  I=II
  J=JJ
  IF(II.EQ.0) I=II+1
  IF(II.EQ.8) I=II-1
  IF(JJ.EQ.0) J=JJ+1
  IF(JJ.EQ.8) J=JJ-1
  DMDTR1=F3(I,J)
  > +(F3(I+1,J)-F3(I,J))/(X3(I+1)-X3(I))*(R-X3(I))
  DMDTR2=F3(I,J+1)
  > +(F3(I+1,J+1)-F3(I,J+1))/(X3(I+1)-X3(I))*(R-X3(I))
  DMDTR=DMDTR1+(DMDTR2-DMDTR1)/(Y3(J+1)-Y3(J))*(T-Y3(J))
  FDMDTR=DMDTR
  RETURN
END
FUNCTION FDTDRE(R,E)
COMMON /INPL/ X1(9),Y1(9),F1(9,9),X2(9),Y2(9),F2(9,9),
>           X3(9),Y3(9),F3(9,9),X4(9),Y4(9),F4(9,9),
>           X5(9),Y5(9),F5(9,9),X6(9),Y6(9),F6(9,9),
>           X7(9),Y7(9),F7(9,9)
  IF(R.LT.X6(1)) II=0
  IF(R.GT.X6(9)) II=8
  DO 1 I=1,8
  IF(R.GE.X6(I).AND.R.LE.X6(I+1)) THEN
    II=I
    GO TO 2
  ELSE
  END IF
1 CONTINUE
2 CONTINUE
  IF(II.EQ.0) THEN
    WRITE (6,500) R,X6(1),X6(9)
500  FORMAT('//2X,'R IS OUT OF BOUNDARIES, CALLED FROM FDTDRE'/
> 2X,'R=',E12.5,2X,'X6(1)=',E12.5,2X,'X6(9)=',E12.5)
    STOP
  ELSE
  END IF
  IF(E.LT.Y6(1)) JJ=0
  IF(E.GT.Y6(9)) JJ=8
  DO 3 J=1,8
  IF(E.GE.Y6(J).AND.E.LE.Y6(J+1)) THEN
    JJ=J
    GO TO 4
  ELSE
  END IF
3 CONTINUE
4 CONTINUE
  IF(JJ.EQ.0) THEN
    WRITE (6,501) E,Y6(1),Y6(9)
501  FORMAT('//2X,'E IS OUT OF BOUNDARIES, CALLED FROM FDTDRE'/
> 2X,'E=',E12.5,2X,'Y6(1)=',E12.5,2X,'Y6(9)=',E12.5)
    STOP

```

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ELSE
END IF
I=II
J=JJ
IF(II.EQ.0) I=II+1
IF(II.EQ.8) I=II-1
IF(JJ.EQ.0) J=JJ+1
IF(JJ.EQ.8) J=JJ-1
DTDRE1=F6(I,J)
> +(F6(I+1,J)-F6(I,J))/(X6(I+1)-X6(I))*(R-X6(I))
DTDRE2=F6(I,J+1)
> +(F6(I+1,J+1)-F6(I,J+1))/(X6(I+1)-X6(I))*(R-X6(I))
DTDRE=DTDRE1+(DTDRE2-DTDRE1)/(Y6(J+1)-Y6(J))*(E-Y6(J))
FDTDRE=DTDRE
RETURN
END
FUNCTION FDTDER(R,E)
COMMON /INPL/ X1(9),Y1(9),F1(9,9),X2(9),Y2(9),F2(9,9),
> X3(9),Y3(9),F3(9,9),X4(9),Y4(9),F4(9,9),
> X5(9),Y5(9),F5(9,9),X6(9),Y6(9),F6(9,9),
> X7(9),Y7(9),F7(9,9)
IF(R.LT.X7(1)) II=0
IF(R.GT.X7(9)) II=8
DO 1 I=1,8
IF(R.GE.X7(I).AND.R.LE.X7(I+1)) THEN
  II=I
  GO TO 2
ELSE
END IF
1 CONTINUE
2 CONTINUE
IF(II.EQ.0) THEN
  WRITE (6,500) R,X7(1),X7(9)
500  FORMAT(//2X,'R IS OUT OF BOUNDARIES, CALLED FROM FDTDER'/
> 2X,'R=',E12.5,2X,'X7(1)=',E12.5,2X,'X7(9)=',E12.5)
  STOP
ELSE
END IF
IF(E.LT.Y7(1)) JJ=0
IF(E.GT.Y7(9)) JJ=8
DO 3 J=1,8
IF(E.GE.Y7(J).AND.E.LE.Y7(J+1)) THEN
  JJ=J
  GO TO 4
ELSE
END IF
3 CONTINUE
4 CONTINUE
IF(JJ.EQ.0) THEN
  WRITE (6,501) E,Y7(1),Y7(9)
501  FORMAT(//2X,'E IS OUT OF BOUNDARIES, CALLED FROM FDTDER'/
> 2X,'E=',E12.5,2X,'Y7(1)=',E12.5,2X,'Y7(9)=',E12.5)
  STOP
ELSE
END IF

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I=II
J=JJ
IF(II.EQ.0) I=II+1
IF(II.EQ.8) I=II-1
IF(JJ.EQ.0) J=JJ+1
IF(JJ.EQ.8) J=JJ-1
DTDER1=F7(I,J)
> +(F7(I+1,J)-F7(I,J))/(X7(I+1)-X7(I))*(R-X7(I))
DTDER2=F7(I,J+1)
> +(F7(I+1,J+1)-F7(I,J+1))/(X7(I+1)-X7(I))*(R-X7(I))
DTDER=DTDER1+(DTDER2-DTDER1)/(Y7(J+1)-Y7(J))*(E-Y7(J))
FDTDER=DTDER
RETURN
END
FUNCTION FDMUDRE(R,E)
DR=0.01*R
CALL UGAS3(E,R-DR/2.,ZMU1)
CALL UGAS3(E,R+DR/2.,ZMU2)
DMUDRE=(ZMU2-ZMU1)/DR
FDMUDRE=DMUDRE
RETURN
END
FUNCTION FDMUDER(R,E)
DE=0.01*E
CALL UGAS3(E-DE/2.,R,ZMU1)
CALL UGAS3(E+DE/2.,R,ZMU2)
DMUDER=(ZMU2-ZMU1)/DE
FDMUDER=DMUDER
RETURN
END
FUNCTION FDKDRE(R,E)
DR=0.01*R
CALL UGAS4(E,R-DR/2.,ZK1)
CALL UGAS4(E,R+DR/2.,ZK2)
DKDRE=(ZK2-ZK1)/DR
FDKDRE=DKDRE
RETURN
END
FUNCTION FDKDER(R,E)
DE=0.01*E
CALL UGAS4(E-DE/2.,R,ZK1)
CALL UGAS4(E+DE/2.,R,ZK2)
DKDER=(ZK2-ZK1)/DE
FDKDER=DKDER
RETURN
END
FUNCTION FAR(P,R,T,E,AMW)
DMDRT=FDMDRT(R,T)
DMDTR=FDMDTR(R,T)
DTDRE=FDTDRE(R,E)
BR=1.-R/AMW*DMDRT
BT=1.-T/AMW*DMDTR
FAR=P/R*BR+P/T*BT*DTDRE
RETURN
END

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FUNCTION FAE(P,R,T,E,AMW)
DMDRT=FDMDRT(R,T)
DMDTR=FDMDTR(R,T)
DTDER=FDTDER(R,E)
BR=1.-R/AMW*DMDRT
BT=1.-T/AMW*DMDTR
FAE=P/T*BT*DTDER
RETURN
END
FUNCTION FCO2(P,R,T,E,AMW)
COMPUTING OF SPEED OF SOUND - C**2
P - PRESSURE
R - DENSITY
T - TEMPERATURE
E - INTERNAL ENERGY
AMW - MOLECULAR WEIGHT
DMDRT=FDMDRT(R,T)
DMDTR=FDMDTR(R,T)
DTDRE=FDTDRE(R,E)
DTDER=FDTDER(R,E)
BR=1.-R/AMW*DMDRT
BT=1.-T/AMW*DMDTR
FCO2=P/R*BR+P/T*BT*(DTDRE+P/R**2*DTDER)
RETURN
END
SUBROUTINE SUPPLY
*****
*
* SERVICE SUBROUTINE
*
*****
PARAMETER (IZ=60,JZ=40)
COMMON /VECTOR/ DQ(IZ,JZ,4),Q(IZ,JZ,4),F(IZ,JZ,4),
>           G(IZ,JZ,4), P(IZ,JZ),T(IZ,JZ),E(IZ,JZ),AMW(IZ,JZ),
>           U(IZ,JZ),V(IZ,JZ),UN(IZ,JZ),VN(IZ,JZ),
>           ZMU(JZ),ZMUT(JZ),ZK(JZ)
COMMON /COORD/ SAI(X(IZ,JZ),SAI(Y(IZ,JZ),ETAX(IZ,JZ),
>           ETAY(IZ,JZ),RJ(IZ,JZ),X(IZ,JZ),Y(IZ,JZ),
>           DELTAU(IZ,JZ),A1(IZ,JZ),A2(IZ,JZ),A3(IZ,JZ),
>           A4(IZ,JZ)
COMMON /CONS/ EXI,EYI,THETA,CFL,CFL1,OMEGAX,OMEGAY,AIN,AEX,
>           RL,RG,AMWO,GAMMAO,REN,PRN,PRNT,TREF,ZMUO,OMEGA,
>           PO,TO,TWALL,PB,SUM(4)
COMMON /INTEG/ IL,JL,IL1,JL1,NBEG,NEND,NADV,NORD,ITIME,
>           IVISC,IWALL,IWRT
DIMENSION RHO(IZ,JZ),RHOU(IZ,JZ),RHOV(IZ,JZ),EO(IZ,JZ)
EQUIVALENCE (Q(1,1,1),RHO(1,1)),(Q(1,1,2),RHOU(1,1)),
>           (Q(1,1,3),RHOV(1,1)),(Q(1,1,4),EO(1,1))
DIMENSION SS(4),A(4,4)
*****
ENTRY CHECK
*****
DO 10 K=1,4
10 SS(K)=0.
DO 20 I=2,IL

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DO 20 J=2,JL
DO 20 K=1,4
QQ=Q(I,J,K)
IF(K.EQ.3) QQ=Q(I,J,2)
IF(QQ.EQ.0.0) GO TO 20
SS(K)=SS(K)+(DQ(I,J,K)*RJ(I,J)/Y(I,J)/QQ)**2
20 CONTINUE
DO 30 K=1,4
30 SS(K)=SQRT(SS(K))/(IL*JL)
WRITE (6,500) NADV,(SS(K),K=1,4)
500 FORMAT(2X,'NADV=',I4,4X,'SS(1)=' ,1X,E12.7,
>           2X,'SS(2)=' ,1X,E12.7,2X,'SS(3)=' ,1X,E12.7,
>           2X,'SS(4)=' ,1X,E12.7)
WRITE (10,501) NADV,(SS(K),K=1,4)
501 FORMAT(I5,3X,4(1X,E14.7))
RETURN
*****
ENTRY MASS
*****
PI=ACOS(-1.0)
I=1
FLRT=0.
DO 41 J=1,JL1
DR=SQRT((X(I,J+1)-X(I,J))**2+(Y(I,J+1)-Y(I,J))**2)
CXCY1=SQRT(SAIX(I,J)**2+SAIY(I,J)**2)
CXCY2=SQRT(SAIX(I,J+1)**2+SAIY(I,J+1)**2)
FLRT=FLRT+0.5*PI*(Y(I,J)+Y(I,J+1))*DR*
>           (RHO(I,J)*UN(I,J)/CXCY1+RHO(I,J+1)*UN(I,J+1)/CXCY2)
41 CONTINUE
WRITE (6,502) I,FLRT
WRITE (4,503) I,FLRT
DO 40 I=1,IL1
FLRT=0.
DO 50 J=1,JL1
DR1=SQRT((X(I,J+1)-X(I,J))**2+(Y(I,J+1)-Y(I,J))**2)
DR2=SQRT((X(I+1,J+1)-X(I+1,J))**2+(Y(I+1,J+1)-Y(I+1,J))**2)
DR=0.5*(DR1+DR2)
*
* 1ST ORDER
*
CXCY11=SQRT(SAIX(I,J)**2+SAIY(I,J)**2)
CXCY12=SQRT(SAIX(I+1,J)**2+SAIY(I+1,J)**2)
CXCY1=0.5*(CXCY11+CXCY12)
CXCY21=SQRT(SAIX(I,J+1)**2+SAIY(I,J+1)**2)
CXCY22=SQRT(SAIX(I+1,J+1)**2+SAIY(I+1,J+1)**2)
CXCY2=0.5*(CXCY21+CXCY22)
RHOUN1=0.5*(RHO(I,J)*UN(I,J)/CXCY11
>           +RHO(I+1,J)*UN(I+1,J)/CXCY12)
RHOUN2=0.5*(RHO(I,J+1)*UN(I,J+1)/CXCY21
>           +RHO(I+1,J+1)*UN(I+1,J+1)/CXCY22)
IF(I.EQ.IL1) GO TO 59
CALL JCBABPM(1,1,1,A,I,J)
AQ1=0.
DO 51 JJ=1,4
51 AQ1=AQ1+A(1,JJ)*(Q(I+1,J,JJ)-Q(I,J,JJ))

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CALL JCBABPM(1,1,1,A,I,J+1)
AQ2=0.
DO 52 JJ=1,4
52 AQ2=AQ2+A(1,JJ)*(Q(I+1,J+1,JJ)-Q(I,J+1,JJ))
RHOUN1=RHOUN1-0.5*AQ1/CXCY1
RHOUN2=RHOUN2-0.5*AQ2/CXCY2
CALL JCBABPM(1,2,1,A,I,J)
AQ1=0.
DO 53 JJ=1,4
53 AQ1=AQ1+A(1,JJ)*(Q(I+1,J,JJ)-Q(I,J,JJ))
CALL JCBABPM(1,2,1,A,I,J+1)
AQ2=0.
DO 54 JJ=1,4
54 AQ2=AQ2+A(1,JJ)*(Q(I+1,J+1,JJ)-Q(I,J+1,JJ))
RHOUN1=RHOUN1+0.5*AQ1/CXCY1
RHOUN2=RHOUN2+0.5*AQ2/CXCY2
*
* 2ND ORDER
*
IF(I.GT.1.AND.I.LT.IL1) THEN
CXCY11=SQRT(SAIX(I-1,J)**2+SAIY(I-1,J)**2)
CXCY12=SQRT(SAIX(I,J)**2+SAIY(I,J)**2)
CXCY1=0.5*(CXCY11+CXCY12)
CXCY21=SQRT(SAIX(I-1,J+1)**2+SAIY(I-1,J+1)**2)
CXCY22=SQRT(SAIX(I,J+1)**2+SAIY(I,J+1)**2)
CXCY2=0.5*(CXCY21+CXCY22)
CALL JCBABPM(1,1,1,A,I-1,J)
AQ1=0.
DO 55 JJ=1,4
55 AQ1=AQ1+A(1,JJ)*(Q(I,J,JJ)-Q(I-1,J,JJ))
CALL JCBABPM(1,1,1,A,I-1,J+1)
AQ2=0.
DO 56 JJ=1,4
56 AQ2=AQ2+A(1,JJ)*(Q(I,J+1,JJ)-Q(I-1,J+1,JJ))
RHOUN1=RHOUN1+0.5*AQ1/CXCY1
RHOUN2=RHOUN2+0.5*AQ2/CXCY2
CXCY11=SQRT(SAIX(I+1,J)**2+SAIY(I+1,J)**2)
CXCY12=SQRT(SAIX(I+2,J)**2+SAIY(I+2,J)**2)
CXCY1=0.5*(CXCY11+CXCY12)
CXCY21=SQRT(SAIX(I+1,J+1)**2+SAIY(I+1,J+1)**2)
CXCY22=SQRT(SAIX(I+2,J+1)**2+SAIY(I+2,J+1)**2)
CXCY2=0.5*(CXCY21+CXCY22)
CALL JCBABPM(1,2,1,A,I+1,J)
AQ1=0.
DO 57 JJ=1,4
57 AQ1=AQ1+A(1,JJ)*(Q(I+2,J,JJ)-Q(I+1,J,JJ))
CALL JCBABPM(1,2,1,A,I+1,J+1)
AQ2=0.
DO 58 JJ=1,4
58 AQ2=AQ2+A(1,JJ)*(Q(I+2,J+1,JJ)-Q(I+1,J+1,JJ))
RHOUN1=RHOUN1-0.5*AQ1/CXCY1
RHOUN2=RHOUN2-0.5*AQ2/CXCY2
END IF
59 CONTINUE
Y1=0.5*(Y(I,J)+Y(I+1,J))

```

```

      Y2=0.5*(Y(I,J+1)+Y(I+1,J+1))
      FLRT=FLRT+0.5*PI*(Y1+Y2)*DR*(RHOUN1+RHOUN2)
50  CONTINUE
     II=I+1
     WRITE (6,502) II,FLRT
502 FORMAT(1X,'I=',I4,2X,'FLRT=',E14.7)
     WRITE (4,503) II,FLRT
503 FORMAT(1X,I8,E14.7)
40  CONTINUE
     RETURN
*****
***** ENTRY OUTPUT *****
*****
      IF(IWRT.EQ.0) GO TO 60
      WRITE (6,504) NEND
504 FORMAT(//4X,'NEND=',I5//)
      DO 70 I=1,IL
      WRITE (6,505) I
505 FORMAT(//2X,2HI=,I2,4X,1HX,11X,1HY,11X,1HU,11X,1HV,11X,
>           1HP,11X,1HR,11X,1HT,11X,1HE,11X,1HS,11X,1HM/)
      DO 70 J=1,JL
      RA=RHO(I,J)
      UA=RHOU(I,J)/RHO(I,J)
      VA=RHOV(I,J)/RHO(I,J)
      EOA=EO(I,J)
      EA=EOA/RA-0.5*(UA**2+VA**2)
      TA=FT(RA,EA)
      AMWA=FAMW(RA,TA)
      PA=RA*(RG/AMWA)*TA
      GAMMA=1.+((RG/AMWA)/(EA/TA))
      SA=ALOG(PA)/GAMMA-ALOG(RA)
      CO=SQRT(FC02(PA,RA,TA,EA,AMWA))
      AMACH=SQRT(UA**2+VA**2)/CO
      WRITE (6,506) J,X(I,J),Y(I,J),UA,VA,PA,TA,EOA,SA,AMACH
506 FORMAT(2X,2HJ=,I2,10(1X,E11.4))
70  CONTINUE
60  CONTINUE
*
*      WRITING COMPUTED DATA ON TAPE
*
      WRITE (8) ((DELTAU(I,J),I=1,IL),J=1,JL)
      WRITE (8) ((RHO(I,J),RHOU(I,J),RHOV(I,J),EO(I,J),
>           I=1,IL),J=1,JL)
      RETURN
      END
      SUBROUTINE EEL(J,MM,JMAX,E,EL,AM,BM,CM,DM,IN,AL,BE)
*****
*
*      LIBRARY SUBROUTINES
*
*****
      DIMENSION IN(MM),E(MM,MM,JMAX),EL(MM,JMAX)
      DIMENSION AM(MM,MM),BM(MM,MM),CM(MM,MM),DM(MM)
      DIMENSION AL(MM,MM),BE(MM)
      DO 1 M=1,MM

```

```

TP=0.00
DO 2 N=1,MM
T1=0.00
IF(J.EQ.1) GO TO 3
TP=TP+AM(M,N)*EL(N,J-1)
DO 4 K=1,MM
T1=T1+AM(M,K)*E(K,N,J-1)
4 CONTINUE
3 CONTINUE
AL(M,N)=BM(M,N)-T1
2 CONTINUE
EL(M,J)=DM(M)+TP
1 CONTINUE
DO 5 M=1,MM
DO 6 N=1,MM
E(M,N,J)=CM(M,N)
6 CONTINUE
5 CONTINUE
CALL AXB(MM,MM,AL,E(1,1,J),BE,O,IN)
CALL AXB(MM,1,AL,EL(1,J),BE,1,IN)
RETURN
END
SUBROUTINE SOLU(W,JMAX,MM,E,EL)
*****
```

```

* LIBRARY SUBROUTINES
*
```

```

*****
```

DIMENSION W(MM,JMAX),E(MM,MM,JMAX),EL(MM,JMAX)

DO 1 M=1,MM

W(M,JMAX)=EL(M,JMAX)

1 CONTINUE

DO 2 J1=2,JMAX

J=JMAX+1-J1

DO 3 M=1,MM

SUM=0.00

DO 4 K=1,MM

SUM=SUM+E(N,K,J)*W(K,J+1)

4 CONTINUE

W(M,J)=SUM+EL(M,J)

3 CONTINUE

2 CONTINUE

RETURN

END

SUBROUTINE AXB(N,M,A,B,X,INIT,IPS)

```

* LIBRARY SUBROUTINES
*
```

```

*****
```

DIMENSION A(N,N),B(N,M),IPS(N),X(N)

IF(INIT.EQ.0) CALL DECOMP(N,A,IPS)

DO 1 I=1,M

CALL SOLV(N,A,B(1,I),X,IPS)

1 CONTINUE

```

RETURN
END
SUBROUTINE DECOMP(N,UL,IPS)
*****
*
* LIBRARY SUBROUTINES
*
*****
DIMENSION UL(N,N), IPS(N)
DO 1 I=1,N
IPS(I)=I
1 CONTINUE
NM1=N-1
DO 2 K=1,NM1
BIG=0.00
DO 3 I=K,N
IP=IPS(I)
SIZE=ABS(UL(IP,K))
IF(SIZE-BIG) 3,3,4
4 BIG=SIZE
IDXPIV=I
3 CONTINUE
IF(IDXPIV-K) 5,6,5
5 J=IPS(K)
IPS(K)=IPS(IDXPIV)
IPS(IDXPIV)=J
6 KP=IPS(K)
PIVOT=UL(KP,K)
KP1=K+1
DO 7 I=KP1,N
IP=IPS(I)
EM=-UL(IP,K)/PIVOT
UL(IP,K)=-EM
DO 7 J=KP1,N
UL(IP,J)=UL(IP,J)+EM*UL(KP,J)
7 CONTINUE
2 CONTINUE
RETURN
END
SUBROUTINE SOLV(N,UL,B,X,IPS)
*****
*
* LIBRARY SUBROUTINES
*
*****
DIMENSION UL(N,N),B(N),X(N),IPS(N)
NP1=N+1
IP=IPS(1)
X(1)=B(IP)
DO 1 I=2,N
IP=IPS(I)
IM1=I-1
SUM=0.00
DO 2 J=1,IM1
SUM=SUM+UL(IP,J)*X(J)
2 CONTINUE
1 CONTINUE

```

```

2 CONTINUE
X(I)=B(IP)-SUM
1 CONTINUE
IP=IPS(N)
B(N)=X(N)/UL(IP,N)
DO 3 IBACK=2,N
I=NP1-IBACK
IP=IPS(I)
IP1=I+1
SUM=0.00
DO 4 J=IP1,N
SUM=SUM+UL(IP,J)*B(J)
4 CONTINUE
B(I)=(X(I)-SUM)/UL(IP,I)
3 CONTINUE
RETURN
END
SUBROUTINE SZERO(M,A)
*****
*
* LIBRARY SUBROUTINES
*
*****
SET ZERO FOR MATRIC (M,M)
DIMENSION A(M,M)
DO 1 I=1,M
DO 1 J=1,M
A(I,J)=0.00
1 CONTINUE
RETURN
END
SUBROUTINE SMM(M,C,A,B)
*****
*
* LIBRARY SUBROUTINES
*
*****
SCALAR*METRIC (M,M)
DIMENSION A(M,M),B(M,M)
DO 1 I=1,M
DO 1 J=1,M
B(I,J)=C*A(I,J)
1 CONTINUE
RETURN
END
SUBROUTINE MMM(M,A,B,C)
*****
*
* LIBRARY SUBROUTINES
*
*****
METRIX*METRIX (M*M)
DIMENSION A(M,M),B(M,M),C(M,M)
DO 1 I=1,M
DO 1 J=1,M

```

FILE: NPROG11 FOR A1 VM/SP CMS 4-8602 (02/02/88) -- THE PENNSYLVANIA STAT

C(I,J)=0.00